FHWA/IN-JHRP-84/20

Purdue University



JOINT HIGHWAY RESEARCH PROJECT

INDIANA HIGHWAY COST ALLOCATION STUDY: FINAL REPORT

K. C. Sinha

T. F. Fwa

E. A. Sharaf

A. B. Tee

H. L. Michael

TOTAL DESCRIPTION OF THE PROJECT

STREET, PLANT SERVED WITCOMAN

Marie A

|  |  | 3. Recipient's Catalog No.                             |
|--|--|--|
| 1. Report No.  | ?. Government Accession No.            | S. Accipient Course                                    |
| FHWA/IN/JHRP-84/20   |  |  |
| 4. Title and Subtitle  |  | 5. Report Date October 31, 1984<br>Revised March, 1985 |
| INDIANA HIGHWAY COST-ALLO<br>REPORT  | OCATION STUDY: FINAL                   | 6. Performing Organization Code                        |
| 7. Author(s) Kumares C. Sinha, Tien-Fa Ah-Beng Tee and Harold L              | ang Fwa, Essam A. Sharaf,<br>. Michael | 8. Performing Organization Report No.  JHRP-84-20      |
| 9. Performing Organization Name and Addre                                    |  | 10. Work Unit No.                                      |
| Joint Highway Research Pr<br>Civil Engineering Buildin                       | 11. Contract or Grant No. HPR-Part I   |  |
| Purdue University<br>West Lafayette, Indiana                                 | 47907                                  | 13. Type of Report and Period Covered                  |
| 12. Sponsoring Agency Name and Address Indiana Department of Hig             | ghways                                 | Final Report   |
| State Office Building<br>100 North Senate Avenue<br>Indianapolis, Indiana 40 | 6204                                   | 14. Sponsoring Agency Code                             |
| 15. Supplementary Notes  | with the U.S. Department o             | f Transportation, Federal                              |

Highway Administration.

This final report presents the findings of the highway cost-allocation study in Indiana. The cost responsibilities and revenue contributions of various vehicle classes were determined for FY 1983 and the biennial period of 1985-86. The findings indicate that passenger cars and single-unit trucks are overpaying their cost responsibility, while buses and heavy combination trucks are underpaying. The report also includes a summary of the procedures used. A thickness incremental approach was used to allocate new highway construction cost and an integrated approach was followed to allocate highway rehabilitation and routine maintenance costs. The structure-related costs were allocated by an incremental analysis. An explicit consideration was given to the effects of age, weather, salt and other chemicals on highways.

| highway cost allocation; revenue attribution; cost responsibility. |                  | available to<br>National Te | No restrictions. This document is available to the public through the National Technical Information Service, Springfield, VA 22161 |           |  |  |  |  |
|--|------------------|-----------------------------|---|-----------|--|--|--|--|
| 19. Security Classif. (of this report)                             | 20. Security Cla | self. (of this page)        | 21. No. of Poges  | 22. Price |  |  |  |  |
| Unclassified Unclass   |                  | ified                       | 259   |           |  |  |  |  |

# INDIANA HIGHWAY COST-ALLOCATION STUDY: FINAL REPORT

To: H.L. Michael, Director

October 31, 1984

Joint Highway Research Project

Revised March, 1985

From: K.C. Sinha, Research Engineer

Project: C-36-54PP

Joint Highway Research Project

File: 3-3-42

Attached is the Final Report on the HPR Part I Study titled, "Indiana Highway Cost-Allocation Study." This report presents the findings of the cost-allocation study for Indiana and it has been prepared under the direction of Professor K. C. Sinha.

The methodology conforms to the mandate of the H.E.A. 1006 of the 103rd General Assembly. The findings indicate that the passenger cars and single-unit trucks are overpaying their cost responsibility, while the buses and heavy combination trucks are underpaying their cost responsibility.

This report is forwarded for review, comment and acceptance by the IDOH and FHWA as fulfillment of the objectives of the study.

Respectfully submitted,

K.C. Sinha

Research Engineer

KCS/rrp

cc: A.G. Altschaeffl

J.M. Bell

W.F. Chen W.L. Dolch

R.L. Eskew

J.D. Fricker

J.R. Skinner

W.H. Goetz

G.K. Hallock

J.F. McLaughlin

R.D. Miles

P.L. Owens

B.K. Partridge

b.k. Partinge

G.T. Satterly

C.F. Scholer

R.M. Shanteau

K.C. Sinha

C.A. Venable

L.E. Wood

r.r. Mood

S.R. Yoder

# THE THE RESTAURANT THE PARTY AND THE PARTY A

TARBORIS STREET, STREET, STREET,

Trees 1.0. times terrary business

THE PERSON NAMED IN

STALL STALL STALL

And the state of the second se

and the contract of the contra

the to contract our to respect that asker on an average and the

and the same of th

challes.

THE VALUE OF

AND THE PARTY OF T

# INDIANA HIGHWAY COST-ALLOCATION STUDY: FINAL REPORT

by

Kumares C. Sinha
Professor of Transportation Engineering

Tien-Fang Fwa Graduate Research Assistant

Essam A. Sharaf
Post-Doctoral Research Fellow

Ah-Beng Tee Graduate Research Assistant

Harold L. Michael Professor of Civil Engineering

Joint Highway Research Project

Project No: C-36-54PP

File No: 3-3-42

Prepared as Part of an Investigation

Conducted by

Joint Highway Research Project Engineering Experiment Station Purdue University

in cooperation with the

Indiana Department of Highways

and the

U.S. Department of Transportation Federal Highway Administration

The contents of this report reflect the views of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

Purdue University West Lafayette, Indiana October 31, 1984

Revised March, 1985

Digitized by the Internet Archive in 2011 with funding from LYRASIS members and Sloan Foundation; Indiana Department of Transportation

#### ACKNOWLEDGMENTS

The preparation of the report was financially supported by the Federal Highway Administration and Indiana Department of Highways. The guidance and counsel of Mr. Gene K. Hallock, Director of the Indiana Department of Highways is greatly appreciated. The assistance of Messrs. Charles Basner and Gary Dalporto of the Federal Highway Administration and Messrs. Daniel Novreske, Deputy Director of Administration and Larry Scott and Don Houterloot of the Planning Division of the Indiana Department of Highways has made the study possible. In addition, many individuals at the Indiana Department of Highways have provided data and necessary information, including Messrs. Richard A. Payne of the Accounting Division, Stanley R. Yoder and Steven J. Hull of the Design Division, David L. Tolbert of the Computer Services Division, William J. Rittman of the Construction Division, William T. May of the Contracts and Legal Division, Robert E. Woods of the Local Assistance Division, Kenneth M. Mellinger and R. Clay Whitmire of the Maintenance Division, Barry Partridge and Keith J. Kercher of the Research and Training Division, and Clinton A. Venable of the Traffic Division. Many students and faculty members at Purdue University contributed to the study, including Messrs. Mark Henderson, Paul Satterly, John D. N. Riverson, Greg Turk, Mitsuru Saito and Khaled Ksaibati, and Profs. Virgil L. Anderson, Robert H. Lee, Robert M. Shanteau and Edward C. Ting. The assistance of Mr. Fred Ross of the Wisconsin Department of Transportation in the early phase of the study is acknowledged. Acknowledgment is also extended to Mrs. Rita Pritchett and Mrs. Julia Jordan who typed the report.



#### TABLE OF CONTENTS

|          |   | Page         |
|----------|---|--------------|
| LIST OF  | TABLES  | v            |
| LIST OF  | FIGURES   | хí           |
| EXECUTIV | VE SUMMARYx   | <b>i i i</b> |
| CHAPTER  | 1. INTRODUCTION   | 1            |
|          | Purpose of the Study                                    | 2            |
|          | Highway Classification                                  | 2            |
|          | Definition of Costs                                     | 5            |
|          | Time Frame of Study                                     | 9            |
|          | Allocated Costs   | 9            |
|          | Attributed Revenues                                     | 1 4          |
| CHAPTER  | 2. COST ALLOCATION METHODOLOGY                          | 18           |
|          | Guiding Principles                                      | 18           |
|          | Overview of the Study Approach                          | 19           |
|          | Summary of Cost-Allocation and Revenue-Attribution      |              |
|          | Procedures  | 22           |
| CHAPTER  | 3. RESULTS OF COST-ALLOCATION AND REVENUE-ATTRIBUTION   |              |
|          | ANALYSIS  | 27           |
|          |   |              |
|          | Cost-Responsibility Factors for Highway and Structure   |              |
|          | Expenditure Items                                       | 27           |
|          | Cost-Responsibility Factors for Major Expenditure Areas | 29           |
|          | Overall Statewide Vehicle Class Cost-                   | 29           |
|          | Responsibilities  | 35           |
|          | Proportions of Attributable and Non-Attributable        |              |
|          | Costs   | 38           |
|          | Revenue Contribution by Vehicle Class                   | 42           |
|          | Comparison of Cost Responsibility with Revenue          | 4. 2         |
|          | Contribution  | 42           |
| •        | Base Period (1983) Findings                             | 42           |
|          | Biennial Budget Period (1985-86) Findings               | 44           |
|          |   |              |
|          | Comparison of Indiana's Findings to Findings in         | / -          |
|          | Other Studies   | 45           |
| CHAPTER  | 4. CONCLUSIONS  | 47           |
| APPENDIX | A. DATA BASE  | 50           |
|          | Traffic Data  | 50           |



|          | Cost  | Dat                                    | а  | • • • •                        |                                    | • • • •                      |                              |   |                   | • • •            | • • •      |        |              | • • •                    |                     |       | • •   | • | 50  |
|----------|---|--|--|--------------------------------|------------------------------------|------------------------------|------------------------------|---|-------------------|------------------|------------|--------|--------------|--------------------------|---------------------|-------|-------|---|---|
|          |   |  | Stat   |                                |                                    |                              |                              |   |                   |                  |            |        |              |                          |                     |       |       |   | 5 1<br>5 2  |
|          | Reve  | nue                                    | Data   |                                |                                    | • • •                        |                              | • • •                                       |                   | • • •            |            |        | • • •        |                          |                     |       | • •   |   | 53  |
| APPENDIX | В.  | PROC                                   | EDUR   | E F                            | OR T                               | RAF                          | FIC                          | DAT   | ГΑ                | COL              | LEC        | TIC    | N.           |                          | • • •               |       | • •   |   | 54  |
|          | Fiel<br>Data<br>Esti<br>VMT                 | cle<br>d Da<br>Red<br>mati<br>Corr     | ta (<br>lucti<br>on o  | olle<br>on a<br>of Ve          | ecti<br>and<br>ehic<br>nce         | on l<br>Anai<br>le-l<br>Mat  | Prod<br>lysi<br>Mile<br>rice | edu<br>ls d<br>es d                         | of<br>for         | s .<br>Tra<br>Re | vel        | ter    | ed           | an                       | • • •<br>• • •<br>d | • • • | • • • | • | <ul><li>54</li><li>55</li><li>55</li><li>60</li></ul> |
| APPENDIX | C.  | HIGH                                   | IWAY   | CON                            | STRU                               | CTI                          | ON (                         | 00 S 1                                      | ΓΑ                | LLO              | CAT        | ION    | 1 .          | • • •                    | • • •               | • • • | • • • | • | 87  |
|          | Righ<br>Grad<br>Drai<br>New<br>Shou<br>Reco | eral nt-of ling lnage Pave nlder onstr | -Way and and ment Cos  | Ear<br>Ear<br>Ear<br>Cos<br>ts | sts thwo osio sts Cost             | rk<br>n C                    | Cost                         | rol   | Co                | sts              |            |        |              |                          |                     | • • • |       | • | 87<br>87<br>91<br>94<br>97<br>105<br>107              |
| APPENDIX | D.  | HIGH                                   | IWAY   | REH                            | ABIL                               | ITA                          | TION                         | 1 C   | OST               | AL               | LOC        | CATI   | ON           | • •                      |                     | • •   |       | • | 109   |
|          | Prev  | eral<br>vious<br>ocati                 | Stu<br>Ion I   | die                            | s<br>edur                          | e f                          | • • • • or 1                 | Pav   | eme               | nt               | Reh        | abi    | 111          | ···<br>tat               | ion                 | • • • |       | • |   |
| APPENDIX | к Е.  |  | CTUE<br>BIL1   |                                |                                    |                              |                              |   |                   |                  |            |        |              |                          |                     |       |       |   | 117   |
|          | Adop<br>Dest<br>Corr<br>Sele<br>Vari        | eral oted ign I celat ectic iatio      | Increading ion of on of other or of the other or of the other or o | emendings Between British      | ntal ween idge ruct twee           | Me<br>AA<br>Sa<br>ure<br>n H | thod<br>SHT(<br>mplo<br>Wid  | d ) and | nd<br>wi          | Act<br>th        | ual<br>Liv | Tive l | rucl<br>Load | <br>ks<br><br>din<br>Cro | e<br>gs<br>ssi      | ng    |       | • | 118<br>118<br>119<br>121                              |
|          |   |  | Subs<br>Exca<br>Drai<br>Rail   | stru<br>avat<br>inag<br>ling   | ruct<br>ctur<br>ion<br>e Pi<br>Fac | e C<br>and<br>pe<br>tor      | ost<br>Ba<br>Fact            | Fa<br>ckf<br>tor                            | cto<br>ill<br>s . | rs<br>Fa         | cto        | ors    | • • •        | • • •                    | • • •               | • • • | • • • |   | 148<br>148  |



| Bridge Replacement   | 152<br>152<br>154<br>154 |
|--|--------------------------|
| APPENDIX F. MAINTENANCE COST ALLOCATION  | 159                      |
| General Previous Studies Allocation Methodology Data Base for Analysis Procedure for Allocating Pavement Routine Maintenance Costs                               | 159<br>160<br>162        |
| APPENDIX G. REVENUE ATTRIBUTION  | 165                      |
| State Highway Revenues   | 167                      |
| State Fuel Taxes   | 169<br>170               |
| APPENDIX H. DETERMINATION OF COST-RESPONSIBILITY FACTORS OF LOAD-RELATED AND NON-LOAD-RELATED FACTORS IN PAVEMENT REHABILITATION AND MAINTENANCE COST ALLOCATION | 172                      |
| APPENDIX I. TABLES OF COST-RESPONSIBILITY FACTORS USED FOR COST-ALLOCATION COMPUTATION   | 183                      |
| APPENDIX J. PROBLEMS OF USING CENTS PER VEHICLE-MILES OF TRAVEL AS AN INDEX FOR EXPRESSING COST-ALLOCATION RESULTS   | 234                      |
| REFERENCES   | 239                      |



## LIST OF TABLES

| Table |  | Page |
|-------|--|------|
| 1     | Adopted Vehicle Classification   | 6    |
| 2     | Vehicle Class Weight Group Classification                                | 7    |
| 3     | Expenditure Items by Expenditure Area                                    | 10   |
| 4     | Highway User Revenues  | 17   |
| 5     | Overall Statewide Cost-Responsibility for Year 1983                      | 36   |
| 6     | Overall Statewide Cost-Responsibility for Year 1985-86                   | 37   |
| 7     | Cost Allocation Criteria for Expenditure Items                           | 39   |
| 8     | Revenue Contribution by Vehicle Class (1983)                             | 40   |
| 9     | Revenue Contribution by Vehicle Class (1985-86)                          | 41   |
| 10    | Cost-Allocation and Revenue Attribution Summary                          | 43   |
| 11    | Comparison of Findings of the Indiana Study to Findings of Other Studies | 46   |
| B • 1 | Number of Traffic Count Sites  | 56   |
| B • 2 | Volume Count Station Locations   | 57   |
| В•3   | Percent VMT of Vehicle Classes on Rural Interstate (1983)                | 6 1  |
| B • 4 | Percent VMT of Vehicle Classes on Urban Interstate (1983)                | 62   |
| B • 5 | Percent VMT of Vehicle Classes on State Primary (1983)                   | 63   |
| B • 6 | Percent VMT of Vehicle Classes on State Secondary (1983)                 | 6 4  |
| B • 7 | Percent VMT of Vehicle Classes on County Roads (1983)                    | 6.5  |
| B • 8 | Percent VMT of Vehicle Classes on City Streets (1983)                    | 66   |
| B.9   | Percent VMT of Vehicle Classes on Rural Interstate                       |      |



|         | (1985-86)  | 69  |
|---------|--|-----|
| B • 1 0 | Percent VMT of Vehicle Classes on Urban Interstate (1985-86)   | 70  |
| B • 11  | Percent VMT of Vehicle Classes on State Primary Routes (1985-86)   | 7 1 |
| B • 12  | Percent VMT of Vehicle Classes on State Secondary Routes (1985-86)                                       | 7 2 |
| B • 13  | Percent VMT of Vehicle Classes on County Roads (1985-86)   | 7 3 |
| B • 14  | Percent VMT of Vehicle Classes on City Streets (1985-86)   | 74  |
| B • 15  | VMT Values by Highway Functional Class   | 7 5 |
| B.16    | Indiana Bureau of Motor Vehicles Registered Vehicle Classification                                       | 76  |
| B • 17  | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Single-Unit Trucks Class 3        | 7 7 |
| B.18    | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Single-Unit Trucks Class 6        | 78  |
| B.19    | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Combination Trucks Class 7        | 7 9 |
| B • 20  | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Single-Unit Trucks Class 9        | 80  |
| B • 21  | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Combination Trucks Class 10       | 8 1 |
| B • 22  | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Combination Trucks Class 11       | 8 2 |
| B.23    | Vehicle Registration Weight-Operating Weight<br>Correspondence Matrix for Combination Trucks<br>Class 12 | 8 3 |
| B • 24  | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Combination Trucks                | 8 5 |



| B.25   | Vehicle Registration Weight-Operating Weight Correspondence Matrix for Combination Trucks |       |
|--------|---|-------|
|        | Class 14  | 8 6   |
| C • 1  | Right-of-Way Width Requirements   | 89    |
| C.2    | Traveled-Way Width Requirements   | 93    |
| E • 1  | Study Vehicle Classification and Equivalent AASHTO Designation                            | 122   |
| E . 2  | Vehicular Classification and Responsibility Summary for Bridge Superstructure             | 1 2 3 |
| E.3    | Characteristics of Typical Bridges Constructed in the Base Period                         | 127   |
| E . 4  | Bridge Width Under Different Loadings   | 129   |
| E • 5  | Distribution Between Highway and Waterway   | 120   |
|        | Crossings   | 130   |
| E.6    | Bridge Superstructure Unit Costs  | 134   |
| E • 7  | Bridge Deck Area  | 135   |
| E . 8  | Superstructure Cost Factors for Interstate Rural Bridges                                  | 136   |
| E.9    | Superstructure Cost Factors for Interstate Urban Bridges                                  | 137   |
| E.10   | Superstructure Cost Factors for State Primary Highway Bridges                             | 138   |
| E • 11 | Superstructure Cost Factors for Secondary Highway Bridges                                 | 139   |
| E.12   | Superstructure Cost Factors for Local Road Bridges  | 140   |
| E.13   | Piling Cost Factors   | 147   |
| E • 14 | Piers and Abutment Cost Factors   | 149   |
| E.15   | Railing Cost Factors  | 151   |
| E • 16 | Percent Distribution of New Bridge Construction Cost by Cost Item and by Highway Class    | 153   |
| E . 17 | Percent Distribution of Bridge Replacement Cost by Cost Item and by Highway Class         | 155   |



| E.18   | Percent Distribution of Bridge Rehabilitation Cost  |     |
|--------|---|-----|
| E • 10 | by Cost Item and by Highway Class   | 156 |
| F • 1  | Pavement Routine Maintenance Activities   | 163 |
| H.1    | Relationship Between Present Serviceability Index (PSI) and Roughness Number (RN)   | 176 |
| H • 2  | Proportional Responsibilities of Load-Related and Non-Load-Related Factors in Indiana Pavement Rehabilitation and Maintenance Cost Allocation | 181 |
| I.1    | Pavement Construction Cost-Responsibility Factors   | 184 |
| I.2    | Shoulder Construction Cost-Responsibility Factors   | 185 |
| 1.3    | Right-of-way Construction Cost-Responsibility Factors   | 186 |
| I • 4  | Drainage & Erosion Control Cost-Responsibility Factors  | 187 |
| I.5    | Grading & Earthwork Cost-Responsibility Factors   | 188 |
| I.6    | Common Costs Cost-Responsbility Factors   | 189 |
| I.7    | Truck-Only Common Costs Cost-Responsibility Factors   | 190 |
| I.8    | Pavement Construction Cost-Responsibility of Vehicle Classes on Rural Interstate (1983)   | 191 |
| I.9    | Pavement Rehabilitation Cost-Responsibility Factors for Rural Interstate  | 192 |
| I.10   | Pavement Rehabilitation Cost-Responsibility Factors for Urban Interstate  | 193 |
| I.11   | Pavement Rehabilitation Cost-Responsibility Factors for State Routes Primary  | 194 |
| I.Î2   | Pavement Rehabilitation Cost-Responsibility Factors for State Routes Secondary  | 195 |
| I.13   | Pavement Rehabilitation Cost-Responsibility Factors for County Roads  | 196 |
| I.14   | Pavement Rehabilitation Cost-Responsibility   | 197 |



| 1.15    | Pavement Maintenance Cost-Responsibility Factors for Rural Interstate       | 198 |
|---------|---|-----|
| I.16    | Pavement Maintenance Cost-Responsibility Factors for Urban Interstate       | 199 |
| I.17    | Pavement Maintenance Cost-Responsibility Factors for State Routes Primary   | 200 |
| I.18    | Pavement Maintenance Cost-Responsibility Factors for State Routes Secondary | 201 |
| I.19    | Pavement Maintenance Cost-Responsibility Factors for County Roads           | 202 |
| I.20    | Pavement Maintenance Cost-Responsibility Factors for City Streets           | 203 |
| I.21    | Bridge Superstructure Cost-Responsibility Factors                           | 204 |
| I . 22  | Bridge Pier Cost-Responsibility Factors                                     | 205 |
| I • 23  | Bridge Excavation Backfill Cost-Responsibility Factors                      | 206 |
| I.24    | Bridge Drainage Cost-Responsibility Factors                                 | 207 |
| I.25    | Bridge Pile Cost-Responsibility Factors                                     | 208 |
| I.26    | Bridge Railing Cost-Responsibility Factors                                  | 209 |
| I.27    | Cost-Responsibility for State Highways (1983)                               | 210 |
| I.28    | Cost-Responsibility for County Roads (1983)                                 | 211 |
| I.29    | Cost-Responsibility for City Streets (1983)                                 | 212 |
| 1.30    | Cost-Responsibility for Bridges on State Highways (1983)                    | 213 |
| I.31    | Cost-Responsibility for Bridges on County Roads (1983)                      | 214 |
| I • 3·2 | Cost-Responsibility for Bridges on City Streets (1983)                      | 215 |
| 1.33    | Cost-Responsibility for Sign Bridges (1983)                                 | 216 |
| I.34    | Cost-Responsibility for Police Enforcement (1983)                           | 217 |
| 1.35    | Weigh Station Inspection Cost-Responsibility for                            |     |



|      | Trucks (1983)   | 218 |
|------|---|-----|
| 1.36 | Cost-Responsibility for State Highways (1985-86)                  | 219 |
| I.37 | Cost-Responsibility for County Roads (1985-86)                    | 220 |
| I.38 | Cost-Responsibility for City Streets (1985-86)                    | 221 |
| 1.39 | Cost-Responsibility for Bridges on State Highways (1985-86)       | 222 |
| I.40 | Cost-Responsibility for Bridges on County Roads (1985-86)         | 223 |
| I.41 | Cost-Responsibility for Bridges on City Roads (1985-86)           | 224 |
| I.42 | Cost-Responsibility for Sign Bridges (1985-86)                    | 225 |
| I.43 | Cost-Responsibility for Police Enforcement (1985-86)              | 226 |
| I.44 | Weigh Station Inspection Cost-Responsibility for Trucks (1985-86) | 227 |
| I.45 | Overall Cost-Responsibility for State Highway System (1983)       | 228 |
| I.46 | Overall Cost-Responsibility for County Road System (1983)         | 229 |
| I.47 | Overall Cost-Responsibility for City Street System (1983)         | 230 |
| I.48 | Overall Cost-Responsibility for State Highway System (1985-86)    | 231 |
| I.49 | Overall Cost-Responsibility for County Road System (1985-86)      | 232 |
| I.50 | Overall Cost-Responsibility for City Street System (1985-86)      | 233 |
| J.1  | Cost-Allocaion Analysis of Example Problem                        | 234 |
| J.2  | Cost-Allocation of Example Problem Expressed in Cents/VMT         | 238 |



## LIST OF FIGURES

| Figure |   | Page |
|--------|---|------|
| 1      | Expenditure Distribution for Fiscal Year 1983   | 12   |
| 2      | Expenditure Distribution for Budget Year 1985-86  | 13   |
| 3      | Cost-Allocation Study Flow Chart  | 23   |
| 4      | Computation of Overall Statewide Vehicle Class Cost-Responsibilities                                      | 30   |
| 5      | Computation of Statewide Vehicle Class Cost-<br>Responsibilities for State Highways                       | 3 1  |
| 6      | Computation of Statewide Cost-Responsibilities for County Roads and City Streets                          | 3 2  |
| 7      | Derivation of Statewide Cost-Responsibilities for State Highway Bridges                                   | 3 3  |
| 8      | Derivation of Statewide Cost-Responsibilities for Bridges on County Roads and City Streets                | 34   |
| D.1    | Schematic Diagram Showing Pavement Performance<br>Considered in Highway Rehabilitation Cost<br>Allocation | 114  |
| E • 1  | Modified AASHTO Live Loading Configurations for Bridge Incremental Designs                                | 120  |
| E.2    | HS and H Trucks Correlation   | 124  |
| E • 3  | Flow Chart Illustrating the Data Generation for the Correlation Process                                   | 123  |
| E • 4  | Percent of Total Superstructure Cost vs. AASHTO HS Loading for Interstate Urban Bridges                   | 141  |
| E • 5  | Percent of Total Superstructure Cost vs. AASHTO HS Loading for Interstate Rural Bridges                   | 142  |
| E • 6  | Percent of Total Superstructure Cost vs. AASHTO HS Loading for State Primary Bridges                      | 143  |
| E.7    | Percent of Total Superstructure Cost vs. AASHTO HS Loading for State Secondary Bridges                    | 144  |
| E . 8  | Percent of Total Superstructure Cost vs. AASHTO HS Loading for Bridges on Local Roads                     | 145  |



| G.1   | Organization of the Motor Vehicle Highway Account (MVHA)   | 166 |
|-------|--|-----|
| H • 1 | Total Pavement Damage as Defined by Zero-<br>Maintenance Pavement Performance Curve                        | 173 |
| H • 2 | Schematic Diagram Showing Pavement Performance Curves with their Associated Routine Expenditures           | 174 |
| н.3   | Schematic Diagram Showing Load-Related and Non-<br>Load-Related Effects Responsible for Pavement<br>Damage | 178 |
| н.4.  | Northern and Southern Regions for Pavement Cost-Allocation   | 182 |



#### **EXECUTIVE SUMMARY**

This study was mandated by the House Enrolled Act 1006 of the 103rd Indiana General Assembly and it was conducted by the Joint Highway Research Project of Purdue University in cooperation with the Indiana Department of Highways.

The study documented the full cost of building and maintaining the state's highway system including that portion of the Federal Interstate system within Indiana. An equitable methodology based on an incremental approach was developed for allocating such costs to all the users of the system. An explicit consideration was given to the effects of age, weather, salt and other chemicals on highways.

The study findings indicated a significant imbalance between cost responsibility of and revenue payment by different vehicle classes. In FY 1983 passenger cars including panels and pickups as well as single-unit trucks overpaid their cost responsibility, while heavy combination trucks and buses underpaid their cost responsibility. The same pattern is expected in the biennial period of 1985-86. However, the underpayment by heavy trucks would be more pronounced in 1985-86. During this biennial period, passenger cars as a group would be overpaying about 25% of their cost responsibility while single-unit trucks as a group would be overpaying about 24% of their cost responsibility. At the same time buses would pay about 2% less than their cost responsibility and combination trucks as a group would pay about 46% less than their cost responsibility.



Although the passenger cars as a group would overpay, there is a significant inequity within this group. This inequity primarily involves underpayment by small cars and overpayment by large cars. In 1985-86, small cars would underpay about 24%, while large cars would overpay about 38% of their cost responsibility. Also, among single-unit trucks, 2-axle and 4-axle trucks would overpay by 45% and 3% respectively, while 3-axle trucks would underpay by 18%. At the same time, almost all vehicle classes in heavy combination group would underpay by about 50% except vehicle class 13 (other 5-axle) which would overpay by about 20%.

In the two-year period of 1985-86 the passenger cars as a group would overpay \$197,960,000 and single-unit trucks as a group would overpay \$31,283,000. On the other hand, combination trucks would underpay \$229,130,000 and buses would underpay only \$113,000. The subsidization of heavy vehicles by passenger cars and single-unit trucks would thus continue if the tax structure remains the same.



#### INTRODUCTION

The Indiana highway system consists of 11,294 miles of State Roads,
66,564 miles of County Roads and 13,818 miles of City Streets. The FederalAid portion of the Indiana highway system is comprised of 1144 miles of Interstates, 5064 miles of Primary, 8980 miles of Secondary and 4828 miles of
Federal-Aid Urban highways. For all governmental units combined, annual
expenditures for highway purposes in Indiana are about 3/4 billion dollars.

As a part of the House Enrolled Act 1006, the 103rd Indiana General Assembly required the Indiana Department of Highways (IDOH) "to undertake a highway cost-allocation study to (a) document the full cost of building and maintaining the state's highway system, including that portion of the Federal Interstate system within Indiana; and (b) develop an equitable methodology for allocating such costs to all the users of the system".

This study, entitled Indiana Highway Cost-Allocation Study, was initiated by the Advisory Board of the Joint Highway Project of Purdue University in cooperation with the IDOH on May 4, 1983. It was carried out in two phases. The major tasks undertaken in Phase I are literature review, study design, data collection and data analysis. Those included in Phase II are development of the methodological framework, preparation of an interim report, determination of travel functions and current cost responsibility, sensitivity analysis, future cost responsibility and preparation of a final report.

An interim report was issued during Phase II of this study. It examined the methodology and procedures adopted by previous studies of other states to determine cost responsibilities of various highway user groups. A procedure for use in Indiana was discussed in the report [39]. This final report



presents the results, findings and conclusions of the entire study. A summary description of the cost-allocation procedures adopted is included in the Appendices to this report.

### Purpose of the Study

The main objective of this study was to fulfill the requirement of the legislative directive mentioned earlier by determining the responsibility of individual vehicle classes in occasioning highway costs. The total highway costs and traffic distribution must first be determined in the highway system concerned. Subsequently, an equitable cost-allocation procedure is to be devised to derive the cost responsibilities of various vehicle classes.

Although determination of the revenue contributed by each vehicle class was not within the initial scope of the present cost-allocation study, the study would not be complete without such information. The results of the cost-allocation study would be meaningful only if it is compared to the user revenue contribution. It was therefore decided to include determination of revenue contribution of individual highway user classes as a task in the Phase II of this study. The revenue contribution of each user class could then be compared with its cost responsibility. This comparison would enable one to determine if the contribution of each user class matches its cost responsibility for the highway costs.

#### Highway Classification

The House Enrolled Act 1006 indicated that the highways to be considered in the cost-allocation study include the State's entire highway system, including that portion of the Federal Interstate system within Indiana. Fol-



lowing this directive, all public roads in Indiana are considered in this study. Toll roads, however, are not included. Exclusion of toll roads is justified because the construction and maintenance of these roads are paid directly by the toll road users and are not part of the state highway expenditures.

The main concern is to select a classification which would lead to an accurate allocation of highway cost. Two important criteria are (i) the data availability by type, and (ii) the accuracy of the cost-allocation figures. Often traffic data are available according to functional classification, while cost data are given in terms of jurisdictional classification. A classification must be sought such that matching and transferring of the two sets of data would not introduce unnecessary inaccuracy in the study results.

The most logical set of criteria for highway classification are:

- a classification which best satisfies the needs of cost allocation;
- a classification which covers all the road systems specified in the scope of the present study; and
- c. a classification which is compatible to the available data from the IDOH and other highway agencies in Indiana.

Following these criteria, the following highway classification was adopted:

- 1. Interstate Urban
- 2. Interstate Rural



- 3. State Routes Primary
- 4. State Routes Secondary
- 5. County Roads
- 6. City Streets

The adopted highway classification conforms well to the functional classification used by the FHWA in recording HPMS data. At the same time, this classification allows identification of the highway system by jurisdiction.

# Vehicle Classification

The basic idea of vehicle classification is to group vehicles having similar characteristics with respect to highway use and highway damage. Ideally, each group must be small enough so that the cost responsibility calculated would represent accurately the cost responsibility of the individual user within the group. On the other hand, the number of groups cannot be so large as to make data sets too formidable to handle. The classification used must reflect the range of highway users in Indiana. It also must be such that the existing data at the IDOH can be used and any new data collected can in turn be employed by the IDOH for other purposes.

Most classification systems used in cost-allocation study follow a two-step procedure: (i) major classes according to function type of vehicles, e.g., passenger cars, buses and trucks; (ii) subdivision of these major classes into smaller grouping based on vehicle weights and/or axle configuration.



A point to note regarding the weight classification is that different types of weights have been used for this purpose. For instance, the 1983 Maryland study [42] used gross registered weight, the 1982 Wisconsin study [48] and 1980 Oregon study [33] used gross operating weight, and the 1981 Wyoming study [45] used empty vehicle weight. Use of gross registered weight facilitates computation of revenue contribution, but transformation to operating weight is needed for assessing cost responsibilities. The reverse is true of classification using gross operating weight.

In the present study vehicles were grouped into fourteen classes as defined in Table 1. The data collected from truck weighing stations were used to subdivide nine of the fourteen classes in terms of gross operating weights. The nine classes are Class 3, 6, 7, 9, 10, 11, 12, 13 and 14. For these nine classes, all cost-allocation analyses were carried out in weight divisions of 2500 pounds. In Table 2 are listed the weight subgroups used for each of the vehicle classes. For the purpose of attributing appropriate revenues correspondence matrices were developed to relate registered vehicle weight classes to gross vehicle weight classes.

## Definition of Costs

Most cost-allocation studies have chosen to use actual expenditure instead of needed expenditure as the allocated costs. The primary reason for not using needed expenditure is that there are no fixed criteria as to what level of highway needs have to be satisfied. Rather than making more assumptions in order to derive a needed expenditure, the actual expenditure was used in the present study because it represents the amount spent in a given year and can be directly related to the revenue contribution of the same year.



Table 1. Adopted Vehicle Classification.

| Class | Description   |
|-------|---|
| 1     | small passenger cars                                  |
| 2     | standard and compact passenger cars, panel and pickup |
| 3     | 2-axle truck (2S and 2D)                              |
| 4     | bus   |
| 5     | car with 1-axle trailer                               |
| 6     | 3-axle single unit truck                              |
| 7     | 2S1 tractor-trailer                                   |
| 8     | car with 2-axle trailer                               |
| 9     | 4-axle single unit truck                              |
| 10    | 3S1 tractor-trailer                                   |
| 11    | 2S2 tractor-trailer                                   |
| 12    | 3S2 tractor-trailer                                   |
| 13    | other 5-axle  |
| 14    | 6 or more axle  |



Table 2. Vehicle Class Weight Group Classification

| 1         A11         B1         A11         B1         C-22,500         12         22,500-87,500         12         25,500-87,500         12         25,500-87,500         12         25,500-87,500         12         25,500-87,500         12         25,500-87,500         12         25,500-87,500         13         25,500-87,500         13         26,51,500-87,500         13         26,51,500-87,500         13         27,500-47,500         13<   | Vehicle<br>Class | Weight<br>Group | Weight in<br>Pounds                     | Vehicle<br>Class | Weight | Weight in<br>Pounds | Vehicle<br>Class | Weight   | Weight in<br>Pounds |
|---|------------------|-----------------|---|------------------|--------|---------------------|------------------|----------|---------------------|
| 1   | 1                | 1               | A11                                     | 9                | -      | <27,500             | 12               | 23       | 75,000-77,500       |
| 10  | 2                | 7               | A11                                     | 10               | CI (   | 27,500-30,000       | 12               | 24<br>25 | 80,000-82,500       |
| 1         7,500         10         2,25,00         13         1           2         7,500         11         2,25,00         13         2         1 <td>ı</td> <td></td> <td></td> <td>10</td> <td>n v</td> <td>&gt;32,500</td> <td>12</td> <td>26</td> <td>82,500 &amp; Above</td>   | ı                |                 |   | 10               | n v    | >32,500             | 12               | 26       | 82,500 & Above      |
| 3         10,000-12,000         11         2         22,500-27,000         13         1           4         12,500-15,000         11         2         22,500-27,000         13         2           5         15,000-15,000         11         4         22,500-27,000         13         2           6         17,500-15,000         11         6         22,500-30,000         13         4           9         22,500-25,000         11         6         32,500-30,000         13         6           9         22,500-25,000         11         6         32,500-30,000         13         6           1         A11         11         1         6         32,500-40,000         13         6           1         A11         11         1         6         32,500-40,000         13         10           1         A11         11         1         4         5,500-40,000         13         10           1         A11         11         1         4         5,500-40,000         13         10           1         A11         11         1         4         5,500-40,000         13         13         11         11 <t< td=""><td>£ .</td><td>٦,</td><td>&lt;7500</td><td>10</td><td>•</td><td></td><td></td><td></td><td></td></t<>   | £ .              | ٦,              | <7500                                   | 10               | •      |                     |                  |          |                     |
| 10,000-27,500   11   2   22,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   25,500-25,000   13   2   2   25,500-25,000   13   2   2   2   2   2   2   2   2   2  | e                | 2               | 000'II-000'                             | 1.1              | -      | <22.500             | 13               | 1        | <42,500             |
| \$ 15,000-17,500 11   | Ć,               | - In            | 10,000-12,500                           | 17               | 2      | 22,500-25,000       | 13               | 2 1      | 42,500-45,000       |
| 6         17,500-20,000         11         4         27,500-30,000         13         4           7         20,000-22,500         11         5         30,000-31,500         13         6           8         22,500-25,000         11         7         35,000-37,500         13         6           9         225,000-25,000         11         8         37,500-45,000         13         8           1         A11         11         11         40,500-42,500         13         10           1         A11         11         14         45,000-42,500         13         11           1         A11         11         11         45,000-42,500         13         11           1         A11         11         11         45,000-42,500         13         11           2         17,500-20,000         11         45,000-42,500         14         13         11           2         20,000-22,500         11         12         47,500-50,000         14         13         11           4         27,500-23,000         12         27,500-25,000         14         13         14         1           5         27,000-22,500         1   | m                | 3 (             | 12,000-11,000                           | 1.               | . ~    | 25,000-27,500       | 13               | (1       | 45,000-47,500       |
| 7         20,000-22,500         11         5         30,000-32,500         13         5           8         22,500-25,000         11         6         32,000-30,500         13         6           9         22,500-25,000         11         7         35,000-40,000         13         6           1         A11         11         11         40,000-42,500         13         10           1         A11         11         11         45,000-45,000         13         10           1         A11         11         11         45,000-45,000         13         11           1         A11         11         47,500-45,000         13         11         12         11         45,000-45,000         13         11         12         20,000-45,000         13         11         12         20,000-45,000         14         13         11         14         45,000-45,000         14         13         11         14         45,000-45,000         14         13         11         14         45,000-45,000         14         14         14         11         14         45,000-45,000         14         14         14         14         14         14         14  | <u>س</u>         | ^ \             | 15,000-17,500                           | 11               | 1 4    | 27,500-30,000       | 13               | 7        | 47.500-50,000       |
| 8         22,500-25,000         11         6         31,500-45,000         13         6           9         22,500-25,000         11         7         35,000-45,000         13         7           1         A11         11         10         42,500-45,000         13         10           1         A11         11         11         42,500-45,000         13         11           1         A12         11         11         42,500-45,000         13         11           1         A12         11         11         42,500-45,000         13         11           2         17,500-20,000         11         12         47,500-47,000         13         11           2         17,500-20,000         12         2,500-27,000         14         3         11         11         12         47,500-47,000         13         11         11         47,500-47,000         13         11         11         47,500-47,000         13         11         11         47,500-47,000         11         11         47,500-47,000         14         11         11         47,500-47,000         14         11         11         47,500-47,000         14         11         41   | ٣                | 01              | 17, 500-20,000                          | 1.               | ۰ ،    | 30,000-32,500       |                  | 2        | 50,000-52,500       |
| 8         22,500-25,000         11         7         35,000-37,500         13         7           1         A11         11         8         37,500-46,000         13         8           1         A11         11         10         42,500-45,000         13         10           1         A11         11         11         10         42,500-45,000         13         10           1         1,7,500         11         11         12         42,500-45,000         13         11           2         1,7,500         11         13         50,000-22,500         13         11           4         22,500-22,000         12         22,500-25,000         14         3           5         25,000-22,500         12         22,500-27,500         14         3           6         27,500-32,000         12         22,500-27,500         14         3           6         27,500-32,000         12         22,500-32,500         14         3           7         27,500-30         12         42,500-32,500         14         3           8         27,500-30         12         42,500-42,500         14         3           9 </td <td>٣</td> <td>_ `</td> <td>20,000-22,500</td> <td>11.</td> <td>) «</td> <td>32,500-35,000</td> <td>13</td> <td>9</td> <td>52,500-55,000</td>  | ٣                | _ `             | 20,000-22,500                           | 11.              | ) «    | 32,500-35,000       | 13               | 9        | 52,500-55,000       |
| 1         A11         11         8         37,500-40,000         13         8           1         A11         11         10         42,500-45,500         13         9         60,000-47,500         13         11         10         42,500-45,500         13         11         10         42,500-45,500         13         11         11         42,500-45,500         13         11         11         42,500-47,500         13         11         11         12         47,500-47,500         13         11         11         12         47,500-47,500         13         11         11         12         47,500-47,500         13         11         12         47,500-47,500         14         12         47,500-45,000         14         12         47,500-45,000         14         12         12         12,500-45,000         14         12         12         12,500-45,000         14         12         12         12,500-45,000         14         12         12         12,500-45,000         14         12         12         12         12         12         12         12         12         12         12         12         12         12         12         12         12         12         12  | m                | ж «             | 22,500-25,000                           | 11.              | ۰ د    | 35,000-37,500       | 13               | 7        | 55,000-57,500       |
| 1 A11 111 9 40,000-42,500 133 10 40,000-42,500 133 11 10 42,500-42,500 133 11 11 45,000-42,500 133 11 11 45,000-42,500 133 11 11 45,000-42,500 133 11 11 45,000-42,500 133 11 11 12 47,500-50,000 133 12 47,500-52,000 11 12 47,500-52,000 14 13 13 12 47,500-52,000 11 12 47,500-52,000 14 13 13 12 47,500-52,000 11 12 47,500-52,000 14 13 13 13 13 13 13 13 13 13 13 13 13 13  | 0                | D.              | 000,625                                 | 1 :              | . oc   | 37, 500-40,000      | 7 -              | - 00     | 57, 500-60,000      |
| A11   |                  | ,               | # P P P P P P P P P P P P P P P P P P P | 1 [              | 0 0    | 40,000-42,500       |                  | ) or     | 60,000-62,500       |
| 1         A11         11         45,000-47,500         13         11           1         <17,500  | . 7              | 7               | All                                     | 1 =              | 10     | 42,500-45,000       | 13               | 01       | 000 59-005 69       |
| 11  |                  |                 |   | 11               | 2 -    | 45,000-47,500       |                  | 10       | 25,000-00,000       |
| 1         <17,500   | 5                | 7               | AII                                     | 1:               | 12     | 47,500-50,000       | 5                | 11       | 62 500-20 000       |
| 1         7,500-22,500         11         1         1,500-22,500         14         1         1         1         2,500-25,000         14         1         2         1         2,500-25,000         14         2         1         2         2,500-25,000         14         2         1         2         2         2,500-25,000         14         2         2         2         2,500-25,000         14         2         2         2         2         2,500-27,500         14         2         2         2         2         2         2         2         3   |                  |                 |   | 11               | 4 -    | SO 000 & Above      | 3 :              | 1.6      | 000,000,000         |
| 2         11,300-22,500         12         1         20,000-22,500         14         1           4         22,500-25,500         12         2         25,000-25,000         14         2           5         25,000-27,500         12         3         25,000-27,500         14         3           6         27,500-37,500         12         4         27,500-37,500         14         3           7         30,000-32,500         12         4         27,500-37,500         14         3           8         32,500-36,000         12         6         32,500-37,500         14         3           9         2,500-36,000         12         7         35,000-37,500         14         3           1         <20,000-22,500   | 9                | _               | <17,500                                 | 11               | 7      |                     | 1.1              | 1.3      | /0,000 & Above      |
| 3       20,000-22,500       12       22,500-25,000       14       1         5       22,500-25,000       12       22,500-25,000       14       2         6       27,500-30,000       12       4       27,500-30,000       14       3         7       30,000-32,500       12       4       27,500-36,000       14       3         8       32,500-35,000       12       7       35,000-37,500       14       3         9       25,000-35,000       12       8       37,500-40,000       12       4       40,000-42,500         1       22,500-25,000       12       14       45,000-47,300       12       47,500-40,000         1       22,500-25,000       12       12       47,500-50,000       12       47,500-50,000         1       22,500-25,000       12       12       47,500-50,000       12       47,500-50,000         1       22,500-30,000       12       14       55,000-57,500       12       14       55,000-57,500         1       10,000-37,500       12       14       52,500-57,500       12       14       52,500-57,500         1       10,000-37,500       12       12       14,500-50,000       12 </td <td>9</td> <td>7</td> <td>17,500-20,000</td> <td></td> <td>-</td> <td>20 000-22 500</td> <td>:</td> <td></td> <td>0000</td>  | 9                | 7               | 17,500-20,000                           |                  | -      | 20 000-22 500       | :                |          | 0000                |
| 4       22,500-25,000       12       2,500-25,500       14       2         5       25,000-27,500       12       4       25,000-27,500       14       3         6       27,500-30,000       12       4       27,500-30,000       14       3         7       30,000-32,500       12       6       32,500-35,000       12       4       27,500-37,000         9       7,500-35,000       12       7       37,500-45,000       12       8       37,500-40,000         1       22,500-22,500       12       11       45,000-42,500       12       40,000-42,500         2       20,000-22,500       12       11       45,000-45,000       12       11       45,000-45,000         3       22,500-25,000       12       12       47,500-50,000       12       13       50,000-52,500         4       25,000-27,500       12       14       52,500-52,000       12       14       52,500-53,000         5       5,000-32,500       12       13       50,000-52,500       12       14       52,500-53,000         6       30,000-37,500       12       14       52,500-53,000       12       14       53,500-53,000         7 <td>9</td> <td></td> <td>20,000-22,500</td> <td>12</td> <td>٦ ،</td> <td>22 500-25 000</td> <td>14</td> <td>4</td> <td>000,04&gt;</td>  | 9                |                 | 20,000-22,500                           | 12               | ٦ ،    | 22 500-25 000       | 14               | 4        | 000,04>             |
| 5     25,000-27,500     12     3     25,000-27,500     14     3       6     27,500-30,000     12     4     27,500-30,000     12     4     27,500-30,000       8     32,500-32,500     12     5     32,500-30,000       9     25,000-32,500     12     8     37,500-40,000       1     22,000-22,500     12     9     40,000-42,500       2     20,000-22,500     12     11     42,500-47,500       4     25,000-27,500     12     11     47,500-50,000       6     30,000-32,500     12     14     52,500-50,000       6     30,000-32,500     12     14     52,500-50,000       7     32,500-30,000     12     14     52,500-50,000       8     15,000-31,500     12     14     52,500-50,000       9     40,000-32,500     12     14     52,500-50,000       10     12     14     52,500-50,500     12     15     51,500-50,000       10     12     12     14     52,500-50,000     12     14     52,500-50,000       10     12     12     14     52,500-50,000     12     12     14     52,500-50,000       10     12     13     14  | 9                | 7               | 22,500-25,000                           | , 12             | 7      | 000, 12, 000, 27    | 14               | 2        | 000,09-000,04       |
| 6 27,500-30,000 12 4 27,500-30,000  7 30,000-32,500 12 5 30,000-32,500  8 32,500-35,000 12 7 35,000-37,500  1   | . 4              | 5               | 25.000-27.500                           | 12               | ~      | 25,000-27,500       | 14               | ~        | >60,000             |
| 7 30,000-32,500 12 5 30 8 32,500-35,000 12 6 3 12 20,000-22,500 12 8 3 12 22,500-22,500 12 10 4 22,500-27,500 12 11 4 25,000-27,500 12 11 4 25,000-37,500 12 11 4 12,500-35,000 12 11 14 12,500-35,000 12 11 14 12,500-37,500 12 11 15 14 55 15,500-37,500 12 11 15 16 5 17 71,500-37,500 12 11 11 17 71,500 12 11 11 18 6 19 7,72,500 12 12 14 10 7,72,500 12 12 14 11 7 11 12 14 12 7,71 13 7,71 14 5,71 15 7,71 16 7,71 17 7,71 18 | o 4              | . 4             | 27, 500-30,000                          | 12               | 4      | 27,500-30,000       |                  |          | 1                   |
| 12   6   3   32,500–35,000  | 0 4              | ۰ ۲             | 30 000-32 500                           | 1.2              | 2      | 30,000-32,500       |                  |          |                     |
| 9 52,500 12 7 3<br>-235,000 12 8 3<br>1   | 0 \              | ~ 0             | 22,500-25,000                           | 12               | 9      | 32,500-35,000       |                  |          |                     |
| 12  | ٩                | 0               | 32,000-30,000                           | 1 0              | 7      | 35,000-37,500       |                  |          |                     |
| 12  | 9                | 6               | 232,000                                 | 12               | . α    | 37,500-40,000       |                  |          |                     |
| 1   |                  |                 | 4                                       | 71,              | 0 0    | 40 000-42 500       |                  |          |                     |
| 2 20,000-22,500 12 10 4<br>3 22,500-25,000 12 11 4<br>4 22,500-27,500 12 12 13 5<br>5 27,500-30,000 12 13 5<br>6 30,000-32,500 12 14 5<br>7 32,500-37,500 12 14 5<br>9 5,000-37,500 12 16 5<br>11 All All 12 19 19 10 11 12 19 10 11 12 19 10 10 10 10 10 10 10 10 10 10 10 10 10   | ./               | _               | < 20,000                                | 7 7              | 9      | 7.2 500-65 000      |                  |          |                     |
| 3 22,500-25,000 112 11 4<br>4 25,000-27,500 112 112 113 5<br>5 27,500-30,000 112 113 114 5<br>6 30,000-35,000 112 114 5<br>11 12 114 5<br>12 114 5<br>13 5,000-37,500 112 116 117 117 117 117 117 117 117 117 117   | 7                | 2               | 20,000-22,500                           | 1.2              | 0 .    | 000 73 800          |                  |          |                     |
| 4 25,000-27,500 12 12 4 5 27,500-30,000 12 13 5 6 30,000-32,500 12 14 5 7 32,500-35,000 12 15 5 8 45,000-37,500 12 15 5 9 -5-17,500 12 18 6 1 -72,500 12 19 6 2 -72,500 12 19 6 2 -72,500 12 29   | 1                |                 | 22,500-25,000                           | 1.2              | 11     | 42,000-47,500       |                  |          |                     |
| 5 27,500-30,000 12 13 5<br>6 30,000-32,500 12 14 5<br>7 32,500-35,000 12 15 5<br>8 35,000-37,500 12 16 5<br>9 5,17,500 12 17 10 11 12 18 11 11 11 11 11 11 11 11 11 11 11 11  |                  | 47              | 25,000-27,500                           | 1.2              | 1.2    | 47,500-50,000       |                  |          |                     |
| 6 30,000-32,500 12 14 5 12 14 5 12 15 15 15 15 15 15 15 15 15 15 15 15 15   | , '              |                 | 27,500-30,000                           | 12               | 13     | 50,000-52,500       |                  |          |                     |
| 7 12,500–35,000 12 15 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6   |                  | n 4             | 005 25 -000 01.                         | 1.2              | 14     | 52,500-55,000       |                  |          |                     |
| 12   13   13   14   15   16   17   18   18   18   18   18   18   18   |                  | 0 -             | 000 31 000 07                           | 12               | 1.5    | 55,000-57,500       |                  |          |                     |
| 8 55,000-57,500<br>12 17<br>1 A11<br>1 A11<br>1 -72,500<br>12 21<br>20 6<br>20 6<br>21 20 6<br>21 20 6<br>21 20 6   | _                | , :             | 000,000,000                             | 4.0              | 91     | 57,500-60,000       |                  |          |                     |
| 1 A11 12 18 6 19 10 10 10 10 10 10 10 10 10 10 10 10 10   | 1                | æ :             | 000 11 -000 CS                          | 24 -             | 1.2    | 60,000-62,500       |                  |          |                     |
| 1 A11 12 19 19 19 19 19 19 19 19 19 19 19 19 19   | /                | C C             | 000,785                                 | 77               | - X    | 62,500-65,000       |                  |          |                     |
| 1   |                  |                 | •                                       |                  |        | 65 000-67 500       |                  |          |                     |
| 12 < 22,500 12 24<br>2 > 22,500 12 24   | \$2              | -               | V   1                                   |                  | 5      | 000,000,000         |                  |          |                     |
| 2 > 22,500 12 21 21 22 21 22 22 22 22 22 22 22 22   |                  |                 |   | *                | 2 =    | 005 77 -000 02      |                  |          |                     |
| 2 22,500  | 6                | _               | 1.72,500                                |                  |        | 22 500 35 000       |                  |          |                     |
|   | 2                | 04              | 272,500                                 | 15               |        | 000,01-000,11       |                  |          |                     |



The HEA 1006 requires that the study consider the full cost of building and maintaining the state's highway system. Full costs are really what we have been spending and an estimate of these estimates can be made by examining actual expenditures for a period of time. Actual expenditure may change from year to year. This change may be brought about by changes in area of emphasis in expenditure program or availability of fund. However, if actual expenditures for a number of years are considered, a great part of the yearly variation can be discounted.

The definition of "full costs" used in the study is valid as confirmed by other state studies. Although "full costs" in one sense of meaning might be defined as what should have been spent to maintain the highway system at a "reasonable level," the fact remains that disagreement with users as to the "reasonable level" will result and determination of that cost will also be subject to question. On the other hand, what was spent is fact and was what the users provided.

The fact that actual expenditures are used in most cost-allocation studies explains why such a study has to be carried out from time to time to check that each user group is paying its fair share of responsibility.

In cost-allocation study, expenditure is commonly divided into distinct categories such as construction, rehabilitation and maintenance. The present study followed the general categories used in the State cost data. The exact categories are as follows:

Highway Construction
Highway Rehabilitation
Structure Construction



Structure Rehabilitation

Maintenance and Operation

Other Costs

Each expenditure category was further subdivided into a number of expenditure items. These subdivisions enabled more accurate cost-allocation to be carried out. This is mainly because each expenditure item is likely to have different responsible attributes (or cost-allocators). The detailed division of each expenditure category into smaller items depends largely upon the degree of breakdown available in the cost data. The expenditure items listed in Table 3 were adopted after careful examination of the cost data files.

### Time Frame of Study

The basic input data used in the study were compiled from a period of four years, 1980 to 1983. Cost and other data were analyzed for this period to determine the appropriate allocation factors. The base period cost responsibility and revenue contribution figures were computed for the fiscal year of 1983. The allocation factors from base period were applied to the study period (1985-86) budgeted expenditure to arrive at the cost responsibility of each vehicle class for the study period. These cost responsibility figures were then compared to the appropriate revenue contribution figures.

#### Allocated Costs

A detailed analysis of expenditure records by cost item for the four year period, 1980-83, was conducted for the state highway system. All expenditures by contract type, by object code and by cost account were analyzed and grouped in terms of the cost categories used in the present study. No such detailed



Table 3. Expenditure Items by Expenditure Area

| Other Costs                                  | Enforcement (policing)          | Weight<br>Inspection            | Special                  | Railroad<br>Crossings  |                  |                                 |                        |
|--|---------------------------------|---------------------------------|--------------------------|------------------------|------------------|---------------------------------|------------------------|
| Routine<br>Maintenance                       | Drainage and<br>Erosion Control | Pavement and<br>Shoulder        | Bridge                   | Miscellaneous<br>Items |                  |                                 |                        |
| Structure<br>Rehabilitation                  | Concrete                        | forcements                      | Steel                    | Miscellaneous<br>Items |                  |                                 |                        |
| Highway<br>Rehabilitation                    | Grading and<br>Earthwork        | Drainage and<br>Erosion Control | Pavement and<br>Shoulder | Miscellaneous          | T CAMES          |                                 |                        |
| Structure<br>Construction and<br>Replacement | Excavation and<br>Backfill      | Concrete<br>Steel Rein-         | forcements               | Structural<br>Steel    | Piers and Piling | Culverts and<br>Sign Structures | Miscellaneous<br>Items |
| Highway<br>Construction                      | Right-of-Way<br>Grading and     | Earthwork<br>Drainage and       | Erosion Control          | Shoulder               | Miscellaneous    | Items                           |                        |



data for the local highway system were available and information from various sources was used to compile the local data. The highway expenditure data from the county annual reports, data from the Bureau of the Census and data collected directly from a number of selected counties and cities were used. In addition, information from the Office of Local Assistance of the Indiana Department of Highways was also available.

For the purpose of cost allocation, expenditures by cost category, by high-way type, by pavement type and by geographic location were necessary. This detailed information for the state highway system was generated by analyzing several data files including road life record files, construction reports, itemized cost estimates, monthly expenditure files, and routine maintenance files. For the local highway system, the corresponding data were collected directly from a number of counties and cities including the counties of Tippecanoe, Monroe, Marion and cities of Lafayette, Fort Wayne, and West Lafayette. The local road inventory file maintained by the IDOH was also used. In addition, the pavement type information was supplemented by an analysis of the records of the local assistance projects supported by the IDOH. The data from the HPMS records were also used in this effort.

A breakdown of the total expenditure supported by user revenue in terms of major cost categories for the fiscal year 1983 is presented in Figure 1. The corresponding expenditure data for the two year period of 1985-86 are presented in Figure 2. The 1985-86 data were estimated from the available revenue information and the adopted program levels. The costs shown in Figures 1 and 2 were subsequently allocated among vehicle classes.

It should be pointed out that the total highway expenditure in Indiana is



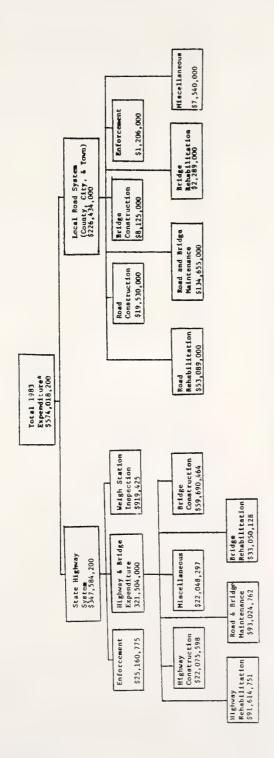
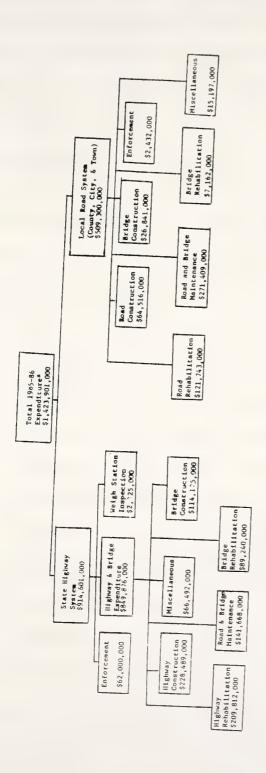


Figure 1. Expenditure Distribution for Piscal Year 1983

\*includes only the expenditure supported by user revenues





\*includes only the expenditure supported by user revenues

Figure 2. Expenditure Distribution for Budget Period 1985/86



expenditure in the state highway system is greatly dependent on user revenues with about 90 percent of the expenditure derived from user revenue in 1983, the portion of expenditure supported by user revenue at the local level was about 52 percent in 1983.

#### Attributed Revenues

Revenues considered in the present study were defined as those revenues contributed by Indiana highway users which were used to support highway activities. The following sources of revenue support these activities in Indiana:

- 1. State gasoline and special fuel taxes
- 2. State motor carrier fuel use tax
- 3. State vehicle license fees including specific periodic permit fees
- 4. State motor carrier fees including vehicle identification stamp fees
- 5. Reciprocity identification stamp fees
- 6. Oversize and overweight permit fees
- 7. Federal gasoline and special fuel taxes
- 8. Federal taxes on tires, tread rubber, inner tubes, lubricating oil, and truck parts (effective in 1983 but not included in 1985-86)
- 9. Federal tax on truck sales
- 10. Federal heavy vehicle use fee
- 11. Local option user taxes

In 1983 the State gasoline and special fuel taxes were equivalent to 11.1 cents per gallon. State motor carrier fuel use tax is collected for the fuel not purchased in Indiana but consumed on Indiana roads from all commercial



vehicles with more than 2 axles including passenger vehicles that seat more than nine passengers. Information on motor fuel taxes was obtained from the Motor Fuel Tax Division of the Department of Revenue.

State vehicle registration fees include such items as license fees on passenger cars, commercial vehicles, personal license plate fees and short term permit fees. The data on registration fees were collected from the Bureau of Motor Vehicles.

Motor carrier vehicle identification stamp fees are for transporting regulated goods over Indiana highways and they include tractor fees, truck or bus fees, 30-day temporary tractor and truck or bus fees. Reciprocity identification stamp fees are collected from interstate carriers from those states with which Indiana has a reciprocity agreement. Information on these fees was obtained from the Public Service Commission.

State revenue sources excluded from revenue attribution were those fees which were charges related to specific services, such as vehicle title fee, various dealer fees, transfer fees, amateur radio fees, driver license fees, driver court fees and reinstatement fees. It should be pointed out that the costs of administering these services were also excluded so as not to affect the revenue/cost comparisons.

Federal revenue sources include motor fuel taxes and other taxes and fees. In 1983 other taxes and fees consisted of tax on tires, tread rubber, inner tubes, lubricating oil and truck parts, tax on truck sales, and heavy vehicle use fee. The STAA of 1982 and subsequent amendment made several changes in the federal tax structure. Schedules of motor fuel taxes, tax on truck sales and heavy vehicle use fee have been changed significantly and the



rest of the taxes have been eliminated. Proper consideration was given to these changes for revenue attribution in 1985-86. A detailed discussion on revenue sources and related tax structures is given in Appendix G.

It should be noted that as Indiana is a donor state, only that part of the Indiana highway user payments to the Highway Trust Fund that was returned to Indiana was included in the analysis.

Table 4 shows the revenue sources and the amounts for the FY 1983 and the biennial period of FY 1985-86 included in the user revenue attribution analysis. It may be noted that the major portion of user revenues includes state and federal motor fuel taxes and state registration fees. For example, in 1985-86 out of the total attributed revenue of \$1,422,910,000, these two sources comprised \$1,251,170,000 or about 80 percent of the total amount.



Table 4. Highway User Revenues

|                                 | Amount in Millions |         |         |                  |  |  |
|---------------------------------|--------------------|---------|---------|------------------|--|--|
| Revenue Source                  | FY 1983            | FY 1985 | FY 1986 | 1985-86<br>Total |  |  |
| State Motor Fuel Taxes          | 305.18             | 308.00  | 306.00  | 614.00           |  |  |
| State Vehicle Registration Fees | 109.70             | 113.80  | 112.00  | 225.80           |  |  |
| Other State and Local Fees      | 3.56               | 5.35    | 5.50    | 10.85            |  |  |
| Subtotal (State and Local)      | 418.44             | 427.15  | 423.50  | 850.65           |  |  |
| Federal Motor Fuel Taxes        | 111.03             | 196.44  | 214.93  | 411.37           |  |  |
| Other Federal Taxes             | 44.53              | 76.39   | 85.50   | 161.89           |  |  |
| Subtotal (Federal)              | 155.56             | 272.83  | 299.43  | 572.26           |  |  |
| Total                           | 574.00             | 699.98  | 722.93  | 1,423.91         |  |  |



#### COST-ALLOCATION METHODOLOGY

# Guiding Principles

There are two broad approaches to highway cost-allocation studies, namely the equity approach and the efficiency approach. Ideally, highway cost-allocation study should result in an equitable and efficient highway user financing system so that each user group would be paying its fair share of cost responsibility in terms of revenue contribution.

To be fully efficient, economic theory requires that the price of a trip be equal to the extra or marginal costs caused by that trip. Under this approach, highway users during peak hours would be charged at a higher rate than other users who use highways during off-peak periods. Similarly, highway users in heavily developed area have to pay higher charges than other users in less congested areas. Understandably, much more detailed information than ordinarily available traffic and transportation data is required before such a study can be carried out. There are other difficulties in following this approach even if all the required data were available. Firstly, it cannot be applied directly in a highway cost-allocation analysis because it is extremely difficult to relate marginal costs to levels of expenditures. Most importantly, user charge instruments cannot be easily developed and implemented that vary geographically and by time of day - a requirement for efficient pricing. As a result, the efficiency has not been adopted as the main criterion in other cost-allocation studies although the approach has a sound economic concept of market pricing.

Virtually all cost-allocation studies follow the equity approach. Equity itself is a subjective concept and a clear definition is needed for



application. Equity can be judged by one of the following three criteria [47]:

- a. Costs should be assigned to users in proportion to the benefits they receive.
- b. Costs should be assigned to users in proportion to the costs they cause (occasion).
- c. Costs should be assigned to users in proportion to their ability to pay.

The definition of equity appropriate for highway cost-allocation studies is that related to cost-responsibility or the cost occasioned by various vehicle groups. The present cost-allocation study, based on the equity approach, followed a procedure which is both practical and theoretically sound.

## Overview of the Study Approach

The major steps in the present cost-allocation study are identified in this section, and these are:

- a. Collection of data: An extensive data collection effort was made to obtain information on highway traffic, highway expenditures and user revenues. Relevant information on highway pavement and structure characteristics was also compiled. Information on the data base is given in Appendix A.
- b. Establishing Input Data: The collected data were processed to provide input information to the cost-allocation and revenue attribution analyses.

  The 1983 traffic data included vehicle classification by highway class, gross



operating weight distribution by vehicle class, distribution of gross vehicle weights for each registered weight class, and an estimate of vehicle-miles of travel by vehicle class, by weight group, and by highway class. Appropriate adjustments were made to project traffic information to the study period of 1985-86. A more detailed discussion of the traffic data collection and analysis is presented in Appendix B.

The state highway expenditure data were compiled from the computerized records of the IDOH Accounting Division for the fiscal years of 1980 through 1983. The local highway expenditure data were compiled from various sources as mentioned earlier. The input information on expenditure included expenses by detailed cost category, by highway class, by pavement type and by geographic location. For certain cost items, such as maintenance, historical record of expenses was processed to provide appropriate input information. The 1985-86 expenditure for the State highway system was based on the expected level of revenues and proposed budgets, while the corresponding amounts for the local highway system was estimated according to the expected level of user revenues and past expenditure records.

The input for user revenue attribution analysis included information on total amounts by revenue source for state highway system, county ads and city streets. In order to attribute revenues among vehicle classes, appropriate tax structures were also provided as input.

c. Identifying Attributable and Non-attributable Costs: One of the major issues in cost-allocation study is to determine the proportions of attributable and non-attributable costs in each expenditure item. Attributable costs are costs which can be attributed to specific vehicle classes, whereas non-



attributable costs are those which are not related to vehicular characteristics and vehicle use. A large part of the non-attributable costs results from the effects of age, weather, salt and other chemicals on highways. In the present study, non-attributable costs were considered as common costs to all highway users.

- d. Selection of Cost-Allocators for Expenditure Items: After identifying attributable and non-attributable costs, the next step was to select suitable cost-allocators to distribute these costs among vehicle classes. Due to the differing nature and causes of various expenditure items, it is not possible to use a single cost-allocator that is satisfactory for all expenditure items. In order to distribute equitably highway costs among vehicle classes in proportion to their responsibility for occasioning these costs, an appropriate cost-allocator was selected for each expenditure item so as to reflect as closely as possible the relationships between particular expenditure items and the specific vehicle classes. A separate set of allocators also was selected for distributing the non-attributable or common costs among user groups.
- e. Determination of Cost-Responsibility Factors: The direct consequence of using different expenditure items is obvious the proportion of cost responsibility (i.e. the cost-responsibility factor) of a specific vehicle class for different expenditure items would be different. As mentioned earlier, cost-responsibility factors were determined using the base period data. These factors were then applied to the 1985-86 biennial budgeted expenditure to arrive at the cost-responsibility for each vehicle class in the study period.
  - f. Determination of Revenue Attribution: Once the cost-responsibilities



by each vehicle class. This was accomplished by examining the separate
sources of revenues paid by Indiana highway users and then apportioning the
revenue amounts by vehicle class.

A flow chart is shown in Figure 3 to present the various steps of the cost-allocation and revenue attribution procedures. The interdependence of these steps is also indicated in the flow chart.

### Summary of Cost-Allocation and Revenue Attribution Procedures

The various cost-allocation procedures developed in this study for individual expenditure items may be grouped into two major areas, namely the roadway related area and the structure-related area. In the first area, the main concern was to develop a rational unified allocation procedure for highway construction, routine maintenance and rehabilitation costs. In the second area, the main emphasis was to allocate equitably structure-related costs.

A new incremental approach was developed for allocation of pavement construction costs to highway users. It considers increments of pavement thickness rather than increments or decrements of traffic volume commonly employed in previous cost-allocation studies. The thickness incremental approach eliminates the need for an iterative process to compute vehicle ESAL which is required for cost-responsibility calculation. The procedure also eliminates the economy-of-scale problem present in the classical incremental cost-allocation method.

The allocation of shoulder construction costs followed a procedure similar to that used for new pavement costs. Other highway construction



Collect Base Period Determine Highway Expenditure Data Classification, Vehicle Classification & Expenditure Categories Establish Input Data to Collect Base Period Cost-Allocation Analysis Traffic Data Collect Base Period Revenue Data Identify Attributable & Non-attributable Costs for Each Expenditure Item Determine Base Period Revenue Contribution by Vehicle Class Select Cost-Allocators of Vehicle Classes for Each Expenditure Item Determine Base Period Compare Cost-Responsibility Cost-Responsibility with Revenue Contribution by Vehicle Class in Base Period Estimate Study Period Identify Study Period Traffic Data Highway Program and Budget Determine Study Period Cost-Responsibility by Vehicle Class Estimate Study Period Revenue Compare Cost-Responsibility Determine Study Period with Revenue Contribution Revenue Contribution in Study Period by Vehicle Class

Figure 3. Cost-Allocation Study Flow Chart



expenditure items, such as grading and earthwork, drainage and erosion control, and right-of-way costs, were allocated essentially on the basis of vehicle-miles of travel (VMT). A common feature of the allocation procedures for the five major highway construction items mentioned was that a minimum width was specified for each. The costs incurred within this specified width are attributable to all vehicle classes on the basis of a suitable allocator (such as ESAL, or VMT). Those costs that are associated with width beyond the specified limit were allocated using appropriate allocator weighted by PCE.

For the allocation of highway rehabilitation and routine maintenance costs, a performance-based methodology was developed for determining the cost-responsibilities of load-related and non-load-related factors. The procedure does not require an extensive amount of data collection effort. It relies entirely on recorded pavement performance data which are available in the records of IDOH, and hence eliminates the undesired element of subjective judgment commonly involved in most cost-allocation studies. For the load-related portion of the costs, the basis of allocation was ESAL. The non-load-related portion of the costs was allocated to vehicle classes in proportion to their VMT.

Police enforcement expenditures and other common costs such as traffic signal installation costs, pavement striping costs and roadside mowing costs were distributed to all vehicle classes on the basis of VMT. Such common costs do not include the costs of construction, maintenance, and rehabilitation of facilties like climbing lane and weigh station. These facilties serve only trucks and the associated costs were considered as truck-related common costs. These costs were allocated to trucks only based on their respective VMT.



Structure-related costs included expenditure for bridge construction, bridge rehabilitation, bridge replacement, culvert construction and sign structure construction. Bridge construction refers to bridges built on new alignment, while bridge replacement indicates bridges built on essentially the same alignment. Bridge rehabilitation includes such activities as partial replacement, widening and deck repair. Culvert construction involves box culverts, corrugented metal and structural plate pipes. Sign structurs are overhead sign bridges.

An incremental method that involvoes repetitive designing of a given bridge structure under different vehicle loadings was used in this study. Five types of bridge were used: reinforced concrete slab, prestressed box beam, prestressed I-beam, steel beam and steel girder. Ten AASHTO design loadings were used to approximate various observed vehicle loadings on the highway. The present study developed different cost-allocation procedures for superstructure, substructure, railing, drainage items, excavation and backfill, and miscellaneous elements. The procedures involved in the allocation of structure- related costs followed three specific steps: (1) the correlation of the adopted vehicle classes to the AASHTO design loads, (2) the incremental design of structures with specified increments of AASHTO design loads, and (3) the allocation of individual cost items among various vehicle classes.

The revenue attribution procedure used in the study included the identification of the amount of user revenues from various federal, state and local sources and appropriate attribution of these revenues among the vehicle classes. The applicable tax rates of various revenue sources were also identified. Fuel efficiency rates and other related factors were obtained from the FHWA study [9] and other available sources.



A detailed discussion of the cost-allocation and revenue attribution procedures used in this study is given in the Appendices.



#### CHAPTER THREE

## RESULTS OF COST-ALLOCATION AND REVENUE ATTRIBUTION ANALYSIS

Detailed descriptions of cost-allocation procedures for the expenditure items listed in Table 3 are presented in Appendices C through H. These procedures were employed to determine the cost-responsibility of each vehicle class for individual expenditure item. The cost-allocators employed in the analysis were developed on the basis of information on the actual amount of each expenditure and physical features of the associated facilities obtained from records of the 4-year base period (1980-1983).

# Cost-Responsibility Factors for Highway and Structure Expenditure Items

Presented in Tables I.1 through I.7 of Appendix I are the computed costresponsibility factors (in percentages) by fourteen vehicle classes and six
highway classes for the following highway construction expenditure items:
pavement, shoulder, right-of-way, drainage and erosion control, grading and
earthwork, common costs, and truck-related-only common costs, respectively.
Although only vehicle class cost-responsibilities are shown in these tables,
all cost-allocation analyses were without exception performed with the complete range of weight groups listed in Table 2. For the purpose of illustration, Table I.8 is included in Appendix I to show the breakdown of costresponsibility factors in terms of weight groups for all the fourteen vehicle
classes for pavement construction costs on Interstate Rural.

Pavement rehabilitation cost-responsibility for each vehicle class differs for different regions (northern vs southern Indiana), pavement types



(rigid, overlay and flexible) and highway functional classes (Interstate Rural, Interstate Urban, State Primary, State Secondary, County Roads and City Streets). The effects of region, pavement type and highway class on vehicle class cost-responsibilities are represented by the cost-responsibility factors given in Tables I.9 through I.14 of Appendix I.

Vehicle class cost-responsibilities for pavement maintenance also vary in a similar manner with regions, pavement types and highway functional classes. The cost-responsibility factors of vehicle classes for all region-pavement type-highway class combinations are given in Tables I.15 through I.20 of Appendix I.

The cost-responsibility factors presented in Tables I.1 through I.20 form the basic expenditure item cost-responsibility values which were used to derive the resultant cost-responsibility of each vehicle class for each high-way expenditure area defined in Table 3. The magnitude of this resultant cost-responsibility is a function of the basic cost-responsibility factor values of relevant items and the relative expenditure amounts of the corresponding expenditure items.

An incremental methodology for allocating structure costs was used to arrive at structure cost responsibilities. Vehicle classes were assigned costs in proportion to the effect of their size and weight characteristics. An incremental bridge design process was applied to allocate the following structure cost items:

- 1. superstructure:
- 2. substructure (Pier, Abutment, spread footing):
- 3. piling;
- excavation and backfill;
- 5. railing;



- 6. drainage pipes; and
- 7. miscellaneous items.

The cost-responsibility factors for the first six items are shown in Table I.21 through I.26 in Appendix I. Miscellaneous items have the same cost-responsibility factors as those of common costs presented in Table I.6.

## Cost-Responsibility Factors for Major Expenditure Areas

To determine the overall cost-responsibility of each vehicle class for a desired analysis year, the expenditure item cost-responsibility factors developed in the preceding sections were applied to the corresponding expenditures (budgeted or actual) for the analysis year. In the present study, cost-allocation analysis was performed for FY 1983 (July 1982 to June 1983), and then for the biennial budget period covering FY 1985 and FY 1986. For FY 1983, expenditure actually spent was used for analysis. For FY 1985 and FY 1986, the analysis was performed with budgeted expenditures.

Figures 4 through 8 present a complete flow diagram of the step-by-step cost-responsibility computation involved in the cost-allocation analysis. Expenditure item cost-responsibility factors were first applied to their corresponding expenditure amounts to obtain aggregated expenditure area cost-responsibility factors, as shown in Figures 5 through 8. These factors were then used to compute the overall cost-responsibilities of vehicle classes as explained in Figure 4.

Two sets of cost-responsibility factors for major expenditure areas are given in Appendix I. The first set, presented in Tables I.27 through I.35, pertains to vehicle class cost-responsibilities for Fiscal Year 1983. The second set, shown in Tables I.36 through I.44, is computed for the biennial period 1985 - 1986.



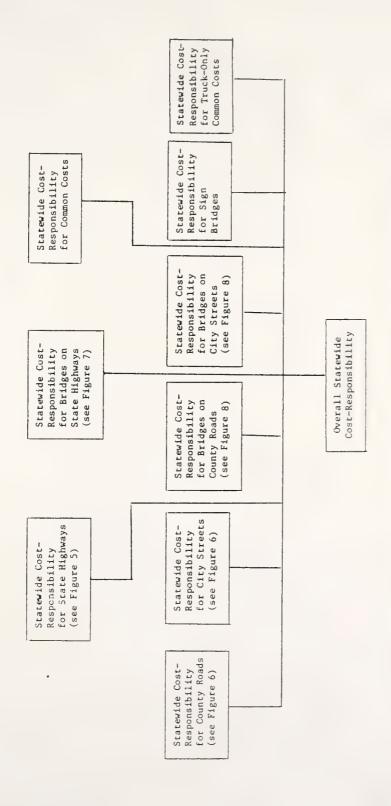


Figure 4. Computation of Overall Statewide Vehicle Class Cost-Responsibilities.



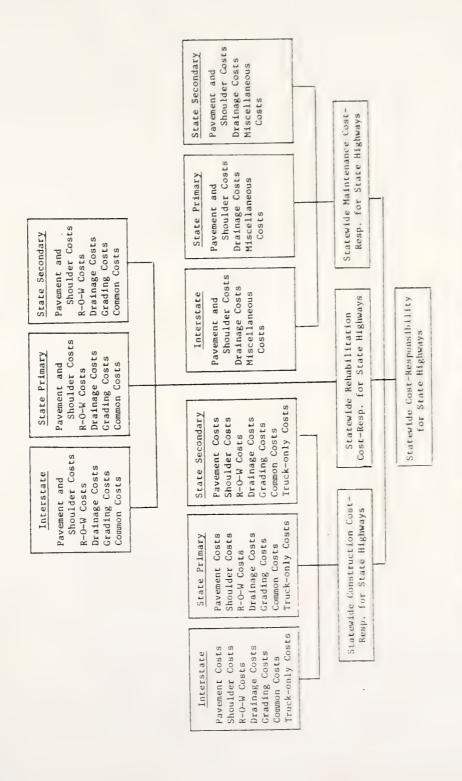


Figure 5. Computation of Statewide Vehicle Class Cost-Responsibilities for State Highways



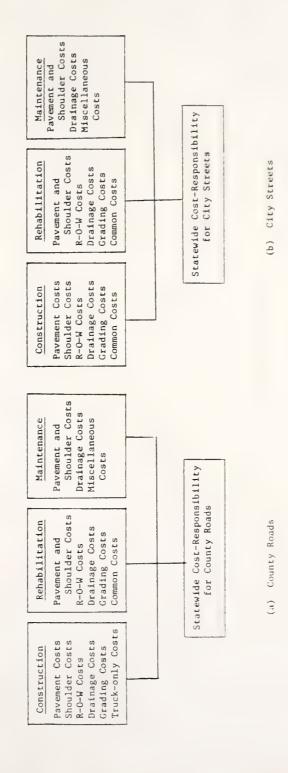


Figure 6. Computation of Statewide Cost-Responsibilities for (a) County Roads, and (b) City Streete



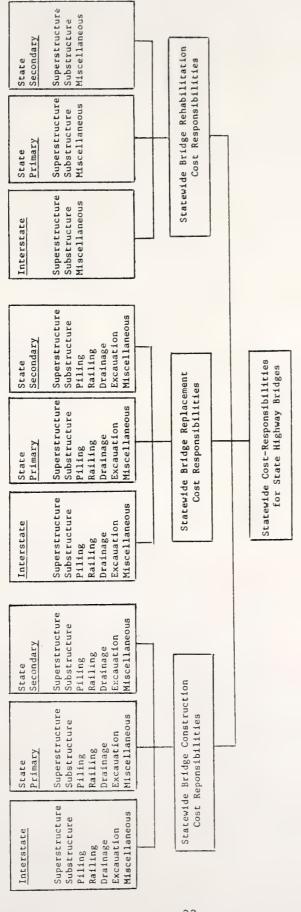
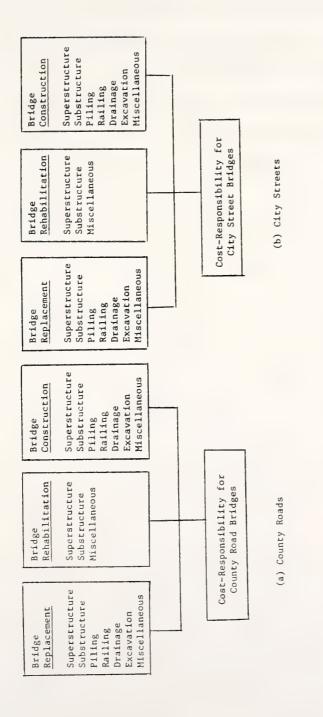


Figure 7. Derivation of Statewide Cost-Responsibilities for State Highway Bridges





Derivation of Statewide Cost-Responsibilities for Bridges on County Roads and City Streets Figure 8.



## Overall Statewide Vehicle Cost-Responsibilities

The overall statewide vehicle class cost-responsibilities for Fiscal Year 1983 and 1985-86 are presented in Tables 5 and 6, respectively. This is the most common form for expressing cost-allocation analysis results. It offers a direct and easily understood comparison with vehicle revenue contribution. This is equivalent to comparing the cost-responsibility per unit vehicle of a given vehicle class against its revenue contribution.

It is noted from the flow diagrams in Figures 4 through 8 that vehicle class cost-responsibilities for state highways, county roads and city streets are kept separate up to the final step. This is desired because these highways are constructed and maintained by different jurisdictional agencies which keep their respective cost accounts and records independently. While the ultimate goal of the present study is to determine the overall statewide cost-responsibility of each vehicle class, it is also meaningful to analyze vehicle class cost-responsibilities in terms of jurisdictional system. Vehicle class cost-responsibilities by jurisdictional system are given in Tables I.45 through I.47 for Fiscal Year 1983 and Tables I.48 through I.50 for biennial period 1985-86.

A number of previous cost-allocation studies had expressed cost-allocation results in terms of cents per vehicle-mile of travel. Unfortunately, this index does not have a clear physical meaning in cost-allocation analysis. It is also not practical to assess equity based on cents/VMT because revenues are not collected on the basis of vehicle-miles of travel.



Table 5. Overall Statewide Cost-Responsibility for Year 1983

| Veh<br>Class | Sub-<br>s Group |         | nsibility<br>Sub-Group | Veh<br>Class | Sub-<br>Group |     |     | sibility<br>Sub-Group |
|--------------|-----------------|---------|------------------------|--------------|---------------|-----|-----|-----------------------|
| 1            | 1               | 10.869  | 10.869                 | 11           | 6             |     |     | 0.410                 |
|              |                 |         |                        | 11           | 7             |     |     | 0.142                 |
| 2            | 1               | 41.510  | 41.510                 | 11           | 8             |     |     | 0.183                 |
| _            | •               | 72.6510 | 411310                 | 11           | 9             |     |     | 0.133                 |
| 3            | 1               | 6.766   | 0.440                  | 11           | 10            |     |     |                       |
| 3            | 2               | 0.700   | 0.403                  | 11           |               |     |     | 0.161                 |
| 3            | 3               |         |                        |              | 11            |     |     | 0.197                 |
| 3            | 4               |         | 0.866                  | 11           | 12            |     |     | 0.213                 |
| 3            |                 |         | 0.873                  | 11           | 13            |     |     | 0.463                 |
| 3            | 5<br>6          |         | 0.450                  |              |               | 2.0 |     |                       |
|              |                 |         | 1.587                  | 12           | 1             | 30. | 253 | 0.020                 |
| 3            | 7               |         | 1.179                  | 12           | 2             |     |     | 0.072                 |
| 3            | В               |         | 0.388                  | 12           | 3             |     |     | 0.263                 |
| 3            | 9               |         | 0.580                  | 12           | 4             |     |     | 0.994                 |
|              |                 |         |                        | 12           | 5             |     |     | 0.455                 |
| 4            | 1               | 0.448   | 0.448                  | 12           | 6             |     |     | 0.526                 |
|              |                 |         |                        | 12           | 7             |     |     | 0.187                 |
| 5            | 1               | 0.387   | 0.387                  | 12           | 8             |     |     | 0.308                 |
|              |                 |         |                        | 12           | 9             |     |     | 0.581                 |
| 6            | 1               | 2.605   | 0.362                  | 12           | 10            |     |     | 0.612                 |
| 6            | 2               |         | 0.266                  | 12           | 11            |     |     | 0.286                 |
| 6            | 3               |         | 0.174                  | 12           | 12            |     |     | 0.388                 |
| 6            | 4               |         | 0.234                  | 12           | 13            |     |     | 0.551                 |
| 6            | 5               |         | 0.092                  | 12           | 14            |     |     | 0.544                 |
| 6            | 6               |         | 0.117                  | 12           | 15            |     |     | 0.629                 |
| 6            | 7               |         | 0.144                  | 12           | 16            |     |     | 0.675                 |
| 6            | 8               |         | 0.220                  | 12           | 17            |     |     | 0.955                 |
| 6            | 9               |         | 0.995                  | 12           | 18            |     |     | 3.051                 |
|              |                 |         |                        | 12           | 19            |     |     | 1.817                 |
| 7            | 1               | 0.974   | 0.029                  | 12           | 20            |     |     | 3.499                 |
| 7            | 2               |         | 0.035                  | 12           | 21            |     |     | 5.320                 |
| 7            | 3               |         | 0.049                  | 12           | 22            |     |     | 3.808                 |
| 7            | 4               |         | 0.072                  | 12           | 23            |     |     | 3.737                 |
| 7            | 5               |         | 0.077                  | 12           | 24            |     |     | 0.672                 |
| 7            | 6               |         | 0.137                  | 12           | 25            |     |     | 0.136                 |
| 7            | 7               |         | 0.156                  | 12           | 26            |     |     | 0.171                 |
| 7            | 8               |         | 0.191                  |              |               |     |     |                       |
| 7            | 9               |         | 0.228                  | 13           | 1             | 1.  | 285 | 0.259                 |
|              |                 |         |                        | 13           | 2             |     |     | 0.317                 |
| 8            | 1               | 0.081   | 0.081                  | 13           | 3             |     |     | 0.249                 |
|              |                 |         |                        | 13           | 4             |     |     | 0.158                 |
| 9            | 1               | 1.087   | 0.018                  | 13           | 5             |     |     | 0.182                 |
| 9            | 2               |         | 1.069                  | 13           | 6             |     |     | 0.008                 |
|              |                 |         |                        | 13           | 7             |     |     | 0.017                 |
| 10           | 1               | 0.107   | 0.021                  | 13           | 8             |     |     | 0.009                 |
| 10           | 2               |         | 0.025                  | 13           | 9             |     |     | 0.009                 |
| 10           | 3               |         | 0.027                  | 13           | 10            |     |     | 0.016                 |
| 10           | 4               |         | 0.033                  | 13           | 11            |     |     | 0.009                 |
|              |                 |         |                        | 13           | 12            |     |     | 0.025                 |
| 11           | 1               | 2.525   | 0.060                  | 13           | 13            |     |     | 0.028                 |
| 11           | 2               |         | 0.106                  |              |               |     |     |                       |
| 11           | 3               |         | 0.224                  | 14           | 1             | I.  | 110 | 0.095                 |
| 11           | 4               |         | 0.128                  | 14           | 2             |     |     | 0.249                 |
| 11           | 5               |         | 0.105                  | 14           | 3             |     |     | 0.765                 |



Table 6. Overall Statewide Cost-Responsibility for Years 1985-86

|       |       | * Page      | nsibility | Veh   | Sub-  | Z   | Respo | nsibility |
|-------|-------|-------------|-----------|-------|-------|-----|-------|-----------|
| Veh   | Sub-  | Veh Class   | Sub-Group | Class | Group | Veh | Class | Sub-Group |
| Class | Group | Ven Class   | 3db-Group |       | ,     |     |       |           |
| 1     | 1     | 11.707      | 11.707    | 11    | 6     |     |       | 0.340     |
| •     | •     |             |           | 11    | 7     |     |       | 0.122     |
| 2     | 1     | 43.610      | 43.610    | 11    | 8     |     |       | 0.153     |
| -     | •     |             |           | 11    | 9     |     |       | 0.123     |
| 3     | 1     | 5.746       | 0.409     | 11    | 10    |     |       | 0.147     |
| 3     | 2     | 3 . 7 . 4 0 | 0.240     | 11    | 11    |     |       | 0.174     |
| 3     | 3     |             | 0.783     | 11    | 12    |     |       | 0.201     |
| 3     | 4     |             | 0.793     | 11    | 13    |     |       | 0.413     |
| 3     | 5     |             | 0.435     |       |       |     |       |           |
| 3     | 6     |             | 1.302     | 12    | 1     | 29  | .281  | 0.021     |
| 3     | 7     |             | 0.960     | 12    | 2     |     |       | 0.084     |
| 3     | 8     |             | 0.342     | 12    | 3     |     |       | 0.323     |
| 3     | 9     |             | 0.484     | 12    | 4     |     |       | 1.042     |
| ,     |       |             |           | 12    | 5     |     |       | 0.544     |
| 4     | 1     | 0.344       | 0.344     | 12    | 6     |     |       | 0.536     |
| -     | -     |             |           | 12    | 7     |     |       | 0.241     |
| 5     | 1     | 0.427       | 0.427     | 12    | 8     |     |       | 0.337     |
|       | •     |             |           | 12    | 9     |     |       | 0.539     |
| 6     | 1     | 2.224       | 0.325     | 12    | 10    |     |       | 0.571     |
| 6     | 2     | 2122        | 0.238     | 12    | 11    |     |       | 0.324     |
| 6     | 3     |             | 0.164     | 12    | 12    |     |       | 0.401     |
| 6     | 4     |             | 0.206     | 12    | 13    |     |       | 0.519     |
| 6     | 5     |             | 0.083     | 12    | 14    |     |       | 0.569     |
| 6     | 6     |             | 0.101     | 12    | 15    |     |       | 0.620     |
| 6     | 7     |             | 0.124     | 12    | 16    |     |       | 0.799     |
| 6     | 8     |             | 0.186     | 12    | 17    |     |       | 0.999     |
| 6     | 9     |             | 0.799     | 12    | 18    |     |       | 2.670     |
| ·     | -     |             |           | 12    | 19    |     |       | 1.718     |
| 7     | 1     | 0.804       | 0.031     | 12    | 20    |     |       | 3.155     |
| 7     | 2     |             | 0.032     | 12    | 21    |     |       | 4.910     |
| 7     | 3     |             | 0.044     | 12    | 22    |     |       | 3.851     |
| 7     | 4     |             | 0.062     | 12    | 23    |     |       | 3.453     |
| 7     | 5     |             | 0.066     | 12    | 24    |     |       | 0.736     |
| 7     | 6     |             | 0.109     | 12    | 25    |     |       | 0.130     |
| 7     | 7     |             | 0.132     | 12    | 26    |     |       | 0.190     |
| 7     | 8     |             | 0.152     |       |       |     |       |           |
| 7     | 9     |             | 0.176     | 13    | 1     | 1   | .218  | 0.222     |
|       |       |             |           | 13    | 2     |     |       | 0.274     |
| 8     | 1     | 0.090       | 0.090     | 13    | 3     |     |       | 0.226     |
|       |       |             |           | 13    | 4     |     |       | 0.148     |
| 9     | 1     | 1.146       | 0.020     | 13    | 5     |     |       | 0.161     |
| 9     | 2     |             | 1.126     | 13    | 6     |     |       | 0.016     |
|       |       |             |           | 13    | 7     |     |       | 0.027     |
| 10    | 1     | 0.093       | 0.018     | 13    | 8     |     |       | 0.012     |
| 10    | 2     |             | 0.021     | 13    | 9     |     |       | 0.013     |
| 10    | 3     |             | 0.025     | 13    | 10    |     |       | 0.024     |
| 10    | 4     |             | 0.029     | 13    | 11    |     |       | 0.015     |
|       |       |             |           | 13    | 12    |     |       | 0.037     |
| 11    | 1     | 2.287       | 0.059     | 13    | 13    |     |       | 0.044     |
| 11    | 2     |             | 0.104     |       |       |     |       | 0.000     |
| 11    | 3     |             | 0.218     | 14    | 1     |     | 1.030 | 0.089     |
| 11    | 4     |             | 0.124     | 14    | 2     |     |       | 0.217     |
| 11    | 5     |             | 0.111     | 14    | 3     |     |       | 0.724     |
|       |       |             |           |       |       |     |       |           |



Appendix J to this report offers a detailed account of the reasons why the index of cents/VMT was not used to present the final results in this study.

## Proportions of Attributable and Non-Attributable Costs

Non-attributable costs refer to expenditures which are resulted by non-traffic causes such as action of environmental forces, including age, weather, salt and other chemical agents, and expend times that are incurred based upon safety or aesthetic considerations. These costs cannot be attributed to any particular user class or group of user classes. In the present study, these costs were distributed on the basis of VMT. The main reason for using this cost-allocator was simply that it has been used widely and is easily understood and accepted.

Attributable costs include (a) costs which are entirely attributable to a single vehicle class, (b) costs which are attributable to a group of vehicle classes, and (c) costs which are occasioned by the entire traffic as a whole. Table 7 classifies all expenditure items into attributable and non-attributable category as defined above. It also presents a summary of cost-allocation criteria adopted for each of these items.

Based on the classification in Table 7, it was computed that for FY 1983, attributable and non-attributable costs constituted 44.59% and 55.41% of the total expenditure, respectively. For biennial period 1985-86, the corresponding numbers are 49.15% and 50.85%.



Table 7. (cont'd)

|    | Expenditure Items |                           | At               | tributable Costs           | Non-Attributable Costs  |                |         |  |
|----|-------------------|---------------------------|------------------|----------------------------|-------------------------|----------------|---------|--|
|    |                   | 1                         | Proportion       | Allocation Procedure       | Proportion              | Allocation Pro | ocedure |  |
|    | 5.                | Miscellaneous             |                  |                            |                         |                |         |  |
|    |                   | (Traffic Service)         |                  |                            | 1002                    | Proportional   | VHT     |  |
|    |                   | (Administration)          |                  |                            | 100%                    | Proportional   |         |  |
|    |                   | (Truck-Related Facilitie  | es)100%          | Proporational truck VMT    |                         |                |         |  |
|    |                   | (Others)                  |                  |                            | 100 <b>z</b>            | Proportional   | VMT     |  |
| c. | Hij               | ghway Maintenance         |                  |                            |                         |                |         |  |
|    | 1.                | Pavement & Shoulder       | Varies<br>66-98% | Proportional $\Sigma$ ESAL | Varies<br>2-34%         | Proportional   | Z ESAL  |  |
|    | 2.                | Right-of-Way              |                  |                            | 100%                    | Proportional   | VMI     |  |
|    | 3.                | Drainage                  |                  |                            | 100%                    | Proportional   | VMT     |  |
|    | 4.                | Roadside Maintenance      | •                |                            | 100%                    | Proportional   | VMI     |  |
|    | 5.                | Miscellaneous             |                  |                            |                         |                |         |  |
|    |                   | (Traffic Service)         |                  |                            | 100%                    | Proportional   | VMT     |  |
|    |                   | (Administration)          |                  |                            | 100%                    | Proportional   | VMI     |  |
|    |                   | (Winter Emergency)        |                  |                            | 100%                    | Proportional   | VMI     |  |
|    |                   | (Truck-Related Maintenanc | e)100%           | Proportional Truck VMT     |                         |                |         |  |
|    |                   | (Others)                  |                  |                            | 100 <b>%</b>            | Proportional   | VXI     |  |
| D. | Bri               | idge Maintenance          |                  |                            |                         |                |         |  |
|    | 1.                | Roadway Maintenance       | Varies<br>66-98% | Proportional $\Sigma$ ESAL | Varies<br>2-34 <b>%</b> | Proportional   | VMT     |  |
|    | 2.                | Structural Members        |                  |                            | 100%                    | Proportional   | VMI     |  |
|    | 3.                | Miscellaneous             |                  |                            | 100%                    | Proportional   | VMI     |  |
| E. |                   | dge Construction, Replace | ement            |                            |                         |                |         |  |
|    | 1.                | Superstructures           | 100%             | Incremental Analysis       |                         |                |         |  |
|    | 2.                | Substructures             | 25-35            | Incremental Analysis       | 65-75                   | Proportional   | VMI     |  |
|    | 3.                | Drainage                  |                  |                            | 100%                    | Proportional   | 77.     |  |
|    | 4.                | Excavation                |                  |                            | 100%                    | Proportional   | WI      |  |
|    | 5.                | Miscellaneous             |                  |                            | 100%                    | Proportional   | 777     |  |



Table 7. Cost Allocation Criteria for Expenditure Item

|    |     | Expenditure Items                       | A                | ttributable Costs                              | Non-Attributable Costs |                      |  |  |
|----|-----|---|------------------|--|------------------------|----------------------|--|--|
|    |     | :                                       | Proportio        | n Allocation Procedure                         | Proportion             | Allocation Procedure |  |  |
| Α. | Hig | hway Construction                       |                  |  |                        |                      |  |  |
|    | 1.  | Pavement (minimum width)                | 100%             | Thickness Incremental method based on ESAL     |                        |                      |  |  |
|    |     | (Additional width)                      | 100%             | Thickness Incremental method based on PCE-ESAL |                        |                      |  |  |
|    | 2.  | Shoulder<br>(minimum width)             | 100%             |  |                        |                      |  |  |
|    |     | (Additional width)                      | 100%             | same as item A.l                               |                        |                      |  |  |
|    | 3.  | Right-of-Way<br>(minimum width)         | 100%             | Proportional VMT                               |                        |                      |  |  |
|    |     | (Additional width)                      | 100%             | Proportional PCE-VMT                           |                        |                      |  |  |
|    | 4.  | Grading & Earthwork<br>(minimum width)  | 100%             | Proportional VMT                               |                        |                      |  |  |
|    |     | (Additional width)                      | 100%             | Proportional PCE-VMT                           |                        |                      |  |  |
|    | 5.  | Drainage & Erosion Cont (minimum width) | rol<br>100%      | Proportional VMT                               |                        |                      |  |  |
|    |     | (Additional width)                      | 100%             | Proportional PCE-VMT                           |                        |                      |  |  |
|    | 6.  | Miscellaneous<br>(Traffic Service)      |                  |  | 100%                   | Proportional VMT     |  |  |
|    |     | (Administration)                        |                  |  | 100%                   | Proportional VMT     |  |  |
|    |     | (Truck-Related Facilitie                | s)100%           | Proportional truck VMT                         | 100*                   | Descriptional IMT    |  |  |
|    |     | (Others)                                |                  |  | 100%                   | Proportional VMT     |  |  |
| В. | Hig | hway Rehabilitation                     |                  |  |                        |                      |  |  |
|    |     | Pavement & Shoulder                     | Varies<br>66-98% |  | Varies I<br>2-34%      | Proportional VMT     |  |  |
|    | 2.  |   | 100%             | same as item A.3                               |                        |                      |  |  |
|    | 3.  | Grading & Earthwork                     | 100%             | same as item A.4                               |                        |                      |  |  |
|    | 4.  | Drainage & Erosion control              | 100%             | same as item A.5                               |                        |                      |  |  |



Table 8. Revenue Contribution by Vehicle Class (1983)

|       |       |           | dhund on  | Veh   | Sub-  | % Contr    | (button   |
|-------|-------|-----------|-----------|-------|-------|------------|-----------|
| Veh   | Sub-  | % Contr   |           |       |       | Veh Class  |           |
| CIASS | Group | ven class | Sub-Group | Class | Group | VEII CLASS | 340-31049 |
|       |       |           |           |       |       |            |           |
| 1     | 1     | 8.080     | 8.080     | 11    | 6     |            | 0.150     |
| •     | •     |           |           | 11    | 7     |            | 0.070     |
| 2     | 1     | 56.670    | 56.670    | 11    | 8     |            | 0.073     |
| 4     | 1     | 30.070    | 30.070    | 11    | 9     |            | 0.073     |
|       |       |           |           |       | -     |            | 0.063     |
| 3     | 1     | 8.020     | 3.240     | 11    | 10    |            |           |
| 3     | 2     |           | 0.450     | 11    | 11    |            | 0.062     |
| 3     | 3     |           | 0.900     | 11    | 12    |            | 0.058     |
| 3     | 4     |           | 0.940     | 11    | 13    |            | 0.066     |
| 3     | 5     |           | 0.710     |       |       |            |           |
| 3     | 6     |           | 0.580     | 12    | 1     | 18.900     | 0.043     |
| 3     | 7     |           | 0.330     | 12    | 2     |            | 0.166     |
| 3     | 8     |           | 0.400     | 12    | 3     |            | 0.563     |
| 3     | 9     |           | 0.460     | 12    | 4     |            | 1.370     |
| ,     | ,     |           | 0.400     | 12    | 5     |            | 0.847     |
| 4     | 1     | 0.372     | 0.372     | 12    | 6     |            | 0.631     |
| 4     |       | 0.3/2     | 0.3/2     | 12    | 7     |            | 0.400     |
| 5     | 1     | 0.453     | 0.453     | 12    | 8     |            | 0.419     |
| ,     |       | 0.455     | 0.433     | 12    | 9     |            | 0.457     |
| ,     |       | 2 210     | 0.390     | 12    | 10    |            | 0.416     |
| 6     | I     | 2.210     | 0.390     | 12    | 11    |            | 1.120     |
| 6     | 2     |           |           |       |       |            | 0.329     |
| 6     | 3     |           | 0.160     | 12    | 12    |            |           |
| 6     | 4     |           | 0.250     | 12    | 13    |            | 0.397     |
| 6     | 5     |           | 0.160     | 12    | 14    |            | 0.468     |
| 6     | 6     |           | 0.210     | 12    | 15    |            | 0.487     |
| 6     | 7     |           | 0.210     | 12    | 16    |            | 0.718     |
| 6     | 8     |           | 0.160     | 12    | 17    |            | 0.606     |
| 6     | 9     |           | 0.450     | 12    | 18    |            | 0.730     |
| •     | -     |           |           | 12    | 19    |            | 0.614     |
| 7     | 1     | 0.540     | 0.037     | 12    | 20    |            | 0.782     |
| 7     | 2     | 0.540     | 0.046     | 12    | 21    |            | 1.442     |
| 7     | 3     |           | 0.036     | 12    | 22    |            | 1.799     |
| 7     | 4     |           | 0.030     | 12    | 23    |            | 0.952     |
|       |       |           |           | 12    | 24    |            | 0.454     |
| 7     | 5     |           | 0.038     | 12    | 25    |            | 1.337     |
| 7     | 6     |           | 0.031     |       |       |            | 1.355     |
| 7     | 7     |           | 0.180     | 12    | 26    |            | 1.333     |
| 7     | 8     |           | 0.040     |       |       |            |           |
| 7     | 9     |           | 0.039     | 13    | 1     | 1.260      | 0.461     |
|       |       |           |           | 13    | 2     |            | 0.128     |
| 8     | 1     | 0.078     | 0.078     | 13    | 3     |            | 0.080     |
|       |       |           |           | 13    | 4     |            | 0.073     |
| 9     | 1     | 1.620     | 0.630     | 13    | 5     |            | 0.056     |
| 9     | 2     |           | 0.990     | 13    | 6     |            | 0.032     |
|       |       |           |           | 13    | 7     |            | 0.046     |
| 10    | 1     | 0.069     | 0.017     | 13    | 8     |            | 0.037     |
| 10    | 2     |           | 0.016     | 13    | 9     |            | 0.037     |
| 10    | 3     |           | 0.020     | 13    | 10    |            | 0.049     |
| 10    | 4     |           | 0.016     | 13    | 11    |            | 0.038     |
|       | •     |           |           | 13    | 12    |            | 0.057     |
| 11    | 1     | 1.211     | 0.074     | 13    | 13    |            | 0.163     |
| 11    | 2     | 1 *** 1   | 0.110     | 1.5   |       |            |           |
| 11    |       |           | 0.110     | 14    | 1     | 0.520      | 0.189     |
|       | 3     |           |           | 14    | 2     | 0.520      | 0.068     |
| 11    | 4     |           | 0.106     |       |       |            | 0.264     |
| 11    | 5     |           | 0.110     | 14    | 3     |            | 0.204     |



Table 9. Revenue Contribution by Vehicle Class (1985-86)

| Veh   | Sub-  |           | ribution  | Veh   | Sub-  |     |              | Lbution   |
|-------|-------|-----------|-----------|-------|-------|-----|--------------|-----------|
| 01495 | Group | ven class | Sub-Group | Class | Group | ven | Class        | Sub-Group |
|       |       |           |           |       |       |     |              |           |
| 1     | I     | 8.946     | 8.946     | 11    | 6     |     |              | 0.131     |
|       |       |           |           | 11    | 7     |     |              | 0.062     |
| 2     | 1     | 60.250    | 60.250    | 11    | 8     |     |              | 0.065     |
| -     | -     |           | ******    | 11    | 9     |     |              | 0.064     |
| 3     | 1     | 8.306     | 3.563     | 11    | 10    |     |              | 0.055     |
| 3     | 2     | 0.300     | 0.450     | -     |       |     |              |           |
| 3     | 3     |           |           | 11    | 11    |     |              | 0.055     |
| 3     | 4     |           | 0.833     | 11    | 12    |     |              | 0.051     |
| 3     | 5     |           | 0.897     | 11    | 13    |     |              | 0.058     |
| 3     | 6     |           | 0.977     |       |       |     |              |           |
| 3     |       |           | 0.556     | 12    | 1     | 15. | 029          | 0.038     |
| 3     | 7     |           | 0.306     | 12    | 2     |     |              | 0.148     |
|       | 8     |           | 0.350     | 12    | 3     |     |              | 0.490     |
| 3     | 9     |           | 0.375     | 12    | 4     |     |              | 1.195     |
|       | _     |           |           | 12    | 5     |     |              | 0.733     |
| 4     | 1     | 0.336     | 0.336     | 12    | 6     |     |              | 0.547     |
| _     |       |           |           | 12    | 7     |     |              | 0.344     |
| 5     | 1     | 0.459     | 0.459     | 12    | 8     |     |              | 0.362     |
|       |       |           |           | 12    | 9     |     |              | 0.391     |
| 6     | 1     | 1.824     | 0.369     | 12    | 10    |     |              | 0.358     |
| 6     | 2     |           | 0.204     | 12    | 11    |     |              | 0.490     |
| 6     | 3     |           | 0.138     | 12    | 12    |     |              | 0.279     |
| 6     | 4     |           | 0.212     | 12    | 13    |     |              | 0.307     |
| 6     | 5     |           | 0.130     | 12    | 14    |     |              | 0.353     |
| 6     | 6     |           | 0.173     | 12    | 15    |     |              | 0.357     |
| 6     | 7     |           | 0.170     | 12    | 16    |     |              | 0.546     |
| 6     | 8     |           | 0.129     | 12    | 17    |     |              | 0.476     |
| 6     | 9     |           | 0.300     | 12    | 18    |     |              | 0.573     |
| •     | -     |           | 0.300     | 12    | 19    |     |              | 0.467     |
| 7     | 1     | 0.420     | 0.034     | 12    | 20    |     |              | 0.612     |
| 7     | 2     | 0.420     | 0.064     | 12    | 21    |     |              | 1.159     |
| 7     | 3     |           | 0.032     | 12    | 22    |     |              | 1.427     |
| 7     | 4     |           | 0.058     | 12    | 23    |     |              |           |
| 7     | 5     |           |           |       |       |     |              | 0.814     |
| 7     | 6     |           | 0.035     | 12    | 24    |     |              | 0.383     |
|       |       |           | 0.028     | 12    | 25    |     |              | 1.083     |
| 7     | 7     |           | 0.097     | 12    | 26    |     |              | 1.099     |
| 7     | 8     |           | 0.036     |       |       |     |              |           |
| 7     | 9     |           | 0.035     | 13    | 1     | 1.  | 457          | 0.813     |
| _     |       |           |           | 13    | 2     |     |              | 0.108     |
| 8     | 1     | 0.079     | 0.079     | 13    | 3     |     |              | 0.067     |
|       |       |           |           | 13    | 4     |     |              | 0.061     |
| 9     | 1     | 1.179     | 0.515     | 13    | 5     |     |              | 0.041     |
| 9     | 2     |           | 0.664     | 13    | 6     |     |              | 0.027     |
|       |       |           |           | 13    | 7     |     |              | 0.036     |
| 10    | 1     | 0.062     | 0.016     | 13    | 8     |     |              | 0.029     |
| 10    | 2     |           | 0.015     | 13    | 9     |     |              | 0.029     |
| 10    | 3     |           | 0.018     | 13    | 10    |     |              | 0.038     |
| 10    | 4     |           | 0.014     | 13    | 11    |     |              | 0.030     |
|       |       |           |           | 13    | 12    |     |              | 0.045     |
| 11    | 1     | 1.087     | 0.066     | 13    | 13    |     |              | 0.134     |
| 11    | 2     |           | 0.113     |       |       |     |              |           |
| 11    | 3     |           | 0.175     | 14    | 1     | 0   | 5 <b>6</b> 6 | 0.304     |
| 11    | 4     |           | 0.094     | 14    | 2     | 0.  | 200          | 0.051     |
| 11    | 5     |           | 0.098     | 14    | 3     |     |              | 0.031     |
|       |       |           | 0.070     | T.4   | )     |     |              | V = 4.4   |



# Revenue Contribution by Vehicle Class

The result of the revenue attribution analysis provided percentage of revenues contributed by individual vehicle classes. The revenue contribution figures for FY 1983 and the biennial period of 1985-86 are given in Tables 8 and 9, respectively. For example, in 1983 the percentage revenue contributed by vehicle class 2 (large cars) was 56.6%, while the corresponding percentage for vehicle class 12 (3S2 or 5-axle combination truck) was 18.90%. In 1985-86 these percentages were 60.25% and 15.03%, respectively.

## Comparison of Cost-Responsibility with Revenue Contribution

The information on cost-responsibility and revenue contribution of vehicle classes was combined to provide a revenue/cost comparison for each vehicle class. Such a comparison would indicate the equity in revenue contribution. The revenue/cost ratios for FY 1983 and the biennial period of 1985-86 are summarized in terms of fourteen vehicle classes in Table 10.

The study findings for FY 1983 show that passenger cars, including panels and pickups, and single-unit trucks are overpaying, while heavy combination trucks are consistently underpaying their cost responsibility. The same pattern is evident in the 1985-86 results. However, the underpayment by heavy combination trucks is more pronounced in 1985-86.

#### Base Period (1983) Findings

While the passenger cars including panels and pick-ups as a group overpaid their cost-responsibility in 1983, there was a significant imbalance



Table 10. Cost-Allocation and Revenue Attribution Summary

| 1985/86                             | Revenue/Cost          | 0.764<br>1.382<br>1.075<br>0.878   | 0.977 | 1.446<br>0.820<br>1.029<br>1.241     | 0.522<br>0.667<br>0.475<br>0.513<br>1.196<br>0.550            |
|-------------------------------------|-----------------------|------------------------------------|-------|--------------------------------------|---|
| 1 Period                            | Percent<br>Revenue    | 8.946<br>60.250<br>0.459<br>0.079  | 0.336 | 8.306<br>1.824<br>1.179<br>11.309    | 0.420<br>0.062<br>1.087<br>15.029<br>1.457<br>0.566           |
| Summary for Biennial Period 1985/86 | Percent<br>Cost-Resp. | 11.707<br>43.610<br>0.427<br>0.090 | 0.344 | 5.746<br>2.224<br>1.146<br><br>9.116 | 0.804<br>0.093<br>2.287<br>29.281<br>1.218<br>1.030<br>34.713 |
| Summary                             | Percent               | 19.176<br>68.001<br>0.641<br>0.127 | 0.162 | 2.604<br>0.646<br>0.092<br>          | 0.219<br>0.043<br>0.752<br>7.211<br>0.245<br>0.081            |
| 33                                  | Revenue/Cost          | 0.743<br>1.365<br>1.171<br>0.963   | 0.830 | 1.185<br>0.848<br>1.490<br>1.133     | 0.554<br>0.645<br>0.480<br>0.625<br>0.981<br>0.468            |
| 1 Year 198                          | Percent<br>Revenue    | 8.080<br>56.670<br>0.453<br>0.078  | 0.372 | 8.020<br>2.210<br>1.620<br>          | 0.540<br>0.069<br>1.211<br>18.900<br>1.260<br>0.520           |
| Summary for Fiscal Year 1983        | Percent<br>Cost-Resp. | 10.869<br>41.510<br>0.387<br>0.081 | 0.448 | 6.766<br>2.605<br>1.087              | 0.974<br>0.107<br>2.525<br>30.253<br>1.285<br>1.110           |
| Summa                               | Percent<br>VMT        | 19.124<br>68.921<br>0.623<br>0.107 | 0.164 | 2.666<br>0.692<br>0.091              | 0.196<br>0.040<br>0.688<br>6.385<br>0.224<br>0.078            |
|                                     | Vehicle<br>Class      | 8 2 5 1                            | 7     | 6 6 9                                | 7<br>10<br>11<br>12<br>13                                     |
|                                     | Vehicle<br>Type       | Passenger<br>Car                   | Bus   | Single-Unit<br>Truck                 | Combination<br>Truck  |



hetween costs and revenues within the group. In particular, small cars underpaid their cost responsibility, while large cars considerably overpaid.

Single-unit trucks as a group also overpaid their cost responsibility in 1983, although not to the same extent as the passenger cars. In addition, there was a considerable inequity within the group. While 2-axle and 4-axle single-unit trucks overpaid, 3-axle single-unit trucks underpaid their cost-responsibility.

Buses and combination trucks significantly underpaid their costresponsibility. The underpayment was consistent among all combination trucks. However, the extent of this underpayment varied within the group.

Considering the four major vehicle groups, all passenger cars together made an overpayment of \$71,288,000 in excess of their cost responsibility in 1983. Single-unit trucks as a group contributed \$8,004,000 in excess of their cost responsibility. However, buses underpaid \$438,000 and combination trucks as a group paid \$78,854,000 less than their cost responsibility. The net result was that passenger cars and single-unit trucks subsidized the buses and combination trucks.

## Biennial Budget Period (1985-86) Findings

It can be noted in Table 10 that the same general pattern of overpayments and underpayments as in 1983 is present in 1985-86. Passenger cars would be overpaying about 25% of their cost responsibility while single-unit trucks would be overpaying about 24% of their cost responsibility. At the same time buses would pay about 2% less then their cost responsibility and combination trucks would pay about 46% less than their cost-responsibility.



The within-group imbalance of costs and revenue payments in 1985-86 shows the same general pattern as in 1983 with the exception that in 1985-86 vehicle class 13 (other 5-axle) would pay about 20% more than its cost responsibility.

In the two-year period of 1985-86 the passenger cars as a group would overpay \$197,960,000 and single-unit trucks as a group would overpay \$31,283,000. On the other hand, combination trucks would underpay \$229,130,000 and buses would underpay only \$113,000. The subsidization of heavy vehicles by passenger cars and single-unit trucks would thus continue if the tax structure remains the same.

# Comparison of Indiana's Findings to Findings in Other Studies

In Table 11 are shown the revenue/cost ratios for the four generalized vehicle classes determined in Indiana study along with the corresponding figures from other cost-allocation studies. This table is presented for the purpose of comparison. The studies included here covered a wide range of procedures and geographic variations. In addition, the definition of generalized vehicle classes was not the same in all studies. Furthermore, the cost-responsibility and revenue attribution figures depend on the specific expenditure patterns and revenue structures included in a study. Consequently, the results cannot be precisely compared. Nevertheless, the ratios presented in Table 11 give a broad indication of the reasonableness of the results of the Indiana study. It can be noted that the findings of the Indiana study are consistent with those of other studies.



Table 11. Comparison of Findings of the Indiana Study to Findings of Other Studies.

User Revenue Contribution/Cost-Responsibility

|                       | Passenger Car | SU Truck | Combination |
|-----------------------|---------------|----------|-------------|
| Florida (1979)        | 1.04          | 0.91     | 0.51*       |
| Georgia (1979)        | 1.03          | 0.66     | 0.44*       |
| Oregon (1980)         | 1.00          | 1.25     | 0.92        |
| Colorado (1981)       | 1.22          | 1.24     | 0.56        |
| Kentucky (1982)       | 1.57          |          | 0.57**      |
| Maryland (1982)       | 1.17          | 0.83     | 0.56        |
| Connecticut (1982)    | 1.11          | 1.61     | 0.63        |
| Ohio (1982)           | 0.90          | 2.25     | 0.35        |
| Wisconsin (1982)      | 0.94          | 1.40     | 0.89        |
| Maine (1982)          | 1.02          | 1.16     | 0.97        |
| North Carolina (1983) | 0.96          | 2.14     | 0.78        |
| Federal (1982)        | 1.10          | 1.50     | 0.60        |
| Indiana (Base period) | 1.24          | 1.13     | 0.62        |
| (Budget period)       | 1.25          | 1.24     | 0.54        |

<sup>\*5</sup> or more axles

<sup>\*\*</sup> for all trucks



#### CONCLUSIONS

This report has presented the findings and the procedures used in the Indiana highway cost-allocation study. On the basis of a detailed review of the existing cost-allocation studies, an integrated set of methodologies was developed for application in Indiana. An incremental approach was followed for allocation of costs for new highway and structure construction, highway and structure rehabilitation and routine maintenance. This approach is consistent with the state-of-the-art pavement and structure design and maintenance procedures and at the same time the procedures achieved a higher degree of equity in establishing cost responsibilities among highway users than what is provided by the existing cost-allocation methodologies. In particular, the consideration of such non-attributable costs as those caused by age, weather, salt and other chemicals on highways was explicit and the allocation of these costs was achieved through an objective procedure.

The findings of the study indicated that there is a definite imbalance in cost-responsibility and revenue contribution of vehicle classes. In particular, passenger cars as a group and single-unit trucks as a group contribute more revenue than their cost responsibility, while buses and heavy combination trucks contribute less revenue than their cost responsibility. Although passenger cars as a group contribute more revenue, small cars do not pay their fair share and large cars pay more than their fair share. This general trend was determined both in 1983 as well as in the analysis for the biennial period of 1985-86.

There are several issues related to the study that need to be pointed out. First, the study did not treat out-of-state vehicles as a separate



Heavy vehicles are statutorily required to pay fuel tax in proportion to the miles they travel in the state, so the issue would seem to be whether or not out-of-state vehicles pay their proportionate share of registration fees. Currently there are various forms of reciprocity agreements between Indiana and other states as to the travel of out-of-state commercial vehicles. These agreements allow out-of-state commercial vehicles to travel on Indiana highways practically free of any registration fees. However, Indiana based carriers also have the benefit of traveling in other reciprocity states in the same manner. A recent study examined the feasibility of Indiana's participation in the International Registration Plan (IRP) whereby registration fees of interstate vehicles can be shared among participating states in proportion to the miles traveled in a state [38]. While this arrangement would make the revenue contribution of out-of-state travel more close to their cost responsibility, Indiana's participation in the IRP under the current registration fee structure may not be financially beneficial. Furthermore, as Indiana's current registration fees are relatively low and the registration revenue from all interstate trucks of 26,000 lb. or more GVW is only about 4.5% of total user revenues, the inclusion of out-of-state heavy vehicles as a separate class would not make any significant difference in the overall results of revenue/cost comparisons. Nevertheless, it is recognized that a large portion of truck traffic on Indiana highways is due to out-of-state vehicles and an effort is needed to make these vehicles pay a more equitable share of the highway costs.

Another point that needs clarification is that exempt vehicles were not excluded from cost-allocation and revenue attribution analysis. Vehicles with various forms of exemptions include vehicles owned by governmental agencies,



non-profit organizations, farm trucks, school buses and transit buses. In Indiana, the exempt vehicles were estimated to comprise about 2% of all vehicles. Even one assumes each exempt vehicle travels the same mileage per year as other vehicles, the impact of these vehicles would be minimal. Furthermore, the distribution of exempt vehicles is uniform among automobiles, buses and trucks, and thus the exclusion of these vehicles in both cost-allocation and revenue attribution would not introduce any bias in revenue/cost comparisons.

Highway cost allocation and subsequent analysis of revenue attribution should not be considered as a one-time exercise. Instead, it should be recognized as a part of a continuing process of pricing and financing highway services in Indiana. A periodic updating of the cost responsibility and revenue attribution factors is essential in order to keep abreast with the changing traffic distributions, changing expenditure patterns, changing program emphasis, and changing technology. In addition, the procedure and methodology of the highway cost allocation process itself change with time, as new information on such key elements as relationships between traffic load, weather, and pavement and structure damage is generated.



### APPENDIX A

#### DATA BASE

## Traffic Data

A detailed traffic count data for the state highway system are available in the IDOH. However, the available truck classification and weight data were collected not on the basis of random statistical sampling to represent the highway classes in the state. Consequently, a comprehensive vehicle classification survey was undertaken in the present study. In order to make the collected truck data usable for other purposes by the IDOH, the highway classes and vehicle classes were made to match the FHWA and IDOH truck weight study requirements.

The vehicle classification survey included a series of 24-hour manual vehicle counts and a series of 24-hour machine vehicle counts on statistically sampled sections of highways during the summer of 1983. A detailed discussion of the traffic data is presented in Appendix B of this report.

The truck weight data for several years including 1983 from weigh stations were available through the Planning Division of the IDOH. These loadometer data provide operating weight, registered weight, vehicle type, number of axles and their configurations.

# Cost Data

Cost data were collected separately for the state highway system, county roads and city streets.



## State Highway System

The cost and highway physical inventory was compiled for the state system on the basis of the following data sources:

- 1. Road Life Records The information is based on actual contracts, and it provides a detailed description of pavement characteristics. The data from all of the 874 sections were extracted manually from the IDOH records and coded and entered in computer. Although this source provides a detailed description of the various highway activities performed on the state highway system, cost information is often not complete. When available, the cost items are given as follows: Grading and Drainage, Subgrade, Surface and Base, Bridges, Traffic Service, Landscape, and Engineering Inspection.
- 2. Construction Reports These reports, prepared periodically by the Construction Division of the IDOH, provide cost information (total cost) for any contract or a group of contracts in a given time period. These data were computer coded and used when the Road Life Records did not contain enough cost information.
- 3. Itemized Cost Estimates For any contract, a cost estimate proposal is prepared by the IDOH Construction Division. These itemized estimates can be used to obtain the distribution of contract costs for different expenditure items (earthwork, culverts, pavement, shoulder, etc.). These data were also computer coded.
- 4. Routine Maintenance Records The IDOH Maintenance Division prepares crew day cards files to keep records of all routine maintenance activities



done in a given year. Data for the last four years were obtained and information on type of maintenance, location, production units, man-hours, material types and quantities were analyzed.

5. Highway Inventory - The highway inventory files are stored in the IDOH

Computer system and are updated on an annual basis. These files include
information similar to that of road life records files. Highway inventory files, however, do not include cost or structural information. On
the other hand, they include information on all physical characteristics
as length, width, median, etc. Also, they include roughness and traffic

(ADT) information.

In addition to the above sources, expenditure data reported by the IDOH on the PR-534 and on HPMS sections were also analyzed.

#### Local Roads

- 1. Road Inventory An inventory of physical characteristics of the highway system in Indiana is available at the Planning Division. It should be noted, however, that the available data needed extensive updating.
- 2. County and Municipal Highway Expenditure Data From the 1982 Annual Reports, data on total receipts and disbursements by fund category for each county were extracted. Similar information was gathered for municipalities from the Bureau of Census. The major categories of expenditures include administrative costs, maintenance and repair, and construction and reconstruction.



3. Personal Interviews - Personal contacts were made with a group of county and city highway agencies to receive detailed cost data that were used to distribute the aggregated data collected from the available information in various reports.

## Revenue Data

Highway revenues in Indiana primarily consist of user taxes and fees, including motor fuel taxes and special fuel taxes, vehicle registration fees, motor carrier fees and vehicle operator's fees. There are some other revenues in the form of fines and charges. The highway revenues also include intergovernmental transfer of funds from federal to state and local governments and from state to local governments.

Revenue data for the base period were collected from appropriate agencies including Indiana Department of Highways, Indiana Department of Revenue, Bureau of Motor Vehicles, Public Service Commission and the State Auditor. Further information on highway revenues at local levels was collected from Annual Reports and personal interviews. Information on federal revenue was collected from the Federal Highway Administration. Supplementary data were also used from several Federal Highway Administration reports including <a href="Highway Statistics">Highway Taxes</a> and <a href="Fees">Fees</a> [44]</a>, and <a href="Road User and Property Taxes">Road User and Property</a> <a href="Taxes">Taxes</a> on Selected Motor Vehicles [25].



#### APPENDIX B

## PROCEDURE FOR TRAFFIC DATA COLLECTION

One of the most critical data items necessary for a cost-allocation study is information on number of vehicle-miles traveled for each type of vehicles on each of the highway classifications. In addition, traffic data are also necessary to estimate the number of axle-miles traveled by each vehicle class on each highway type. In the present study, a detailed vehicle count survey was undertaken to estimate vehicle miles of travel. Combining these estimates with the data primarily from the IDOH Truck Weight Study, information on vehicle weight and axle-miles was compiled.

## Vehicle Count

The study team conducted a vehicle classification field survey at about 60 randomly selected sites throughout Indiana during the summer of 1983. The resulting data were converted to represent an average day of the year with factors developed from the FHWA report, Vehicle Classification Case Study [26].

To obtain valid estimates of the travel by the various vehicle types on Indiana highways, it was necessary to perform classification counts at many randomly located sites. The basis for selecting a section of road was its length. This made subsequent VMT calculations easier because the VMT on a section of road with uniform flow is the product of the flow at a point and the section's length.

The counting stations were selected form the state's HPMS sample. These roads had already been picked with the probability of selection proportional



to their length, and the locations were documented and marked on maps. Counting stations were determined by randomly picking mileposts from along the mileage in each highway classification.

The number of sites counted within each study class is presented in Table B.l. The variable number of sites in each study class is due to the fact that the present study classifies highway differently than the HPMS classification scheme and because 10 sites were selected from most of the HPMS classes.

The number of sites within each HPMS class is also presented in Table B.1. Only two rural interstate sites were selected because the state already has much information on these highways. Also, the percentage of vehicles within each vehicle type on rural interstates is quite stable, according to an examination of sites observed by the IDOH in 1981.

## Field Data Collection Procedures

Most of the data collection was performed by a team of 4 data collectors and a team leader in 4 shifts of 6 hours each day. Partway into the data collection, a program became available for the Streeter-Amet Traficomp that accurately classifies vehicles according to axle number and spacing. Machine volume recorders were used on 11 2-lane roads late in the data collection period.

In Table B.2 is presented a list of counting sites used in the present study.

## Data Reduction and Analysis

For each road section, the raw figures for the number of vehicles of each



Table B.I. Number of Traffic Count Sites

| Study Class            | Number of Sites |
|------------------------|-----------------|
|                        |                 |
| Interstate Urban       | 9               |
| Interstate Rural       | 2               |
| State Routes Primary   | 22              |
| State Routes Secondary | 7               |
| County Roads           | 4               |
| City Streets           | 8               |

| HPMS Class                      | Number of Sites |
|---------------------------------|-----------------|
|                                 |                 |
| Rural Interstate                | 2               |
| Rural Other Principal Arterials | 8               |
| Rural Minor Arterials           | 6               |
| Rural Major Collectors          | 2               |
| Rural Minor Collectors          | 3               |
|                                 |                 |
| Urban Interstate                | 9               |
| Urban Freeways and Expressways  | 8               |
| Urban Other Principal Arterials | 9               |
| Urban Minor Arterials           | 4               |
| Urban Collectors                | 1               |



SR 18 between US 421 and Flora Corporation Line in Carroll County CR 167 between CR 2 (Howard County Line) and CR 6 in Miami County US 24 between Wabash County Line and 0.1 mile east of SR 37 and SR 9 in Huntington County SR 114 between Huntington County Road and US 24 in Whitley County Park Drive between Huntington Corporation Line and Bartlett Street in Huntington County SR 127 between westbound US 20 (Maumee St.) and Angola Corporation Line in Steuben County US 35 between CR 70 and LaPorte County Line in Starke County 73rd Avenue between Hendricks St. and Van Buren St. in Merrillville US 50 between CR 261 and Martin County Line near Loogootee in Davies County SR 56 between Washington County Line and CR 59

SR 135 between US 50 and SR 58

US 41 at Sullivan and Knox County lines

State Street in the city of Washington between 21st and Evergreen I-64 1.1 miles west of US 41

Tater Road between SR 56 and US 150 - east of Paoli CR 46 between CR 23 and CR 73 - north of Rushville

SR 3 north of US 50 - north of North Vernon

US 50 west of Aurora

US 52 at CR 800 E. in Rush County near Franklin County line.
I-65 at milepost 108 between Raymond St. and Keystone Ave. in Indianapolis
I-70 between Emerson Ave. and Shadeland Ave. in Indianapolis
Shadeland Ave. (SR 100) at southwest loop ramp of US 40 in Indianapolis.
Masschussetts Ave. between Sherman Drive and 30th in Indianapolis
I-74 between SR 25 and SR 341

SR 213 (CR 900 E.) at junction with SR 26 (CR 400 S.) CR 1150 E. (Main Street) at corner of Division Street in Idaville



Table B.2. (cont'd)

SR 55 at the corner of 57th Avenue in Merrillville CR 875 North between McCool Road and SR 149

US 31 between SR 2 and US 20 in South Bend

SR 15 (Main Street) at corner of Kercher Road in Goshen
Raymond Street Expressway (Airport Expressway)
between Holt Road and I 70
I-70 at I 465 interchange (Mile Post 90) - east of Indianapolis
I-70 between Holt Road and Airport Expressway (Mile Post 76) - west of Indianapolis
SR 37 south of Edgewood - southside of Indianapolis

SR 32 east of CR 650 E. - east of Muncie

I-70 west of US 27 - north of Richmond

US 35 at junction with SR 29 in Logansport

US 31 at intersection with SR 14 - west of Rochester SR 3 at Ludwig Road in Fort Wayne

I-69 between US 33 and SR 1

US 30 at junction with Oak Road in Plymouth

I-80/90 east of junction with US 31 - east of South Bend US 30 between Horse Road and West Street - west of SR 2 and Valparaiso I-65 south of US 30 in Merrillville

US 41 at corner of CR 350 S - south of Princeton

Division Street at the corner of Canal Street in Evansville
I-265 west of I-65 (mile post 6) - north of
Clarksville
SR 62 0.7 mile east of junction with SR 131 in
Clarksville
SR 37 at corner of That Road - south of
Bloomington
US 41 (Indianapolis Ave.) at the northwest
corner of 41st St. and US 41 in Highland
US 20 at the junction with CR 275 E. - northeast
of Chesterton
8th Street just west of Henry St. in Anderson

I-70 at the junction with Greenfield in Hancock County (Truck Weight Study ID = 270)



## Table B.2. (cont'd)

I-70 in Wayne County (Truck Weight Study ID = 070)

1-65 north of 2 Lake County (Truck Weight Study ID = 165)

I-65 4.0 miles south of SR 10 in Jasper County (Truck Weight Study ID = 156)

I-69 2.0 miles north of SR 5 in Huntington County (Truck Weight Study ID = 069)

I-74 2.0 miles east of SR 229 in Ripley County (Truck Weight Study ID = 074)

I-70 3.2 miles west of Putman County Line in Clay County (Truck Weight Study ID = 470)

I-64 5 miles east of junction with SR 66 in Harrison County (Truck Weight Study ID = 064)

I-74 2.0 miles west of SR 341 in Fountain County (Truck Weight Study ID = 774)

I-94 in Porter County (Truck Weight Study ID = 094)

I-65 1.4 miles west of US 50 in Jackson County (Truck Weight Study ID = 065)



type that use that road on a summer weekday were available. The collected data were then adjusted to account for daily and seasonal variations. For this, we used the information from the report, Vehicle Classification Case Study [26]. In several other states, data were collected year-round and on both weekdays and weekends. From these data factors were developed that reflected the change in travel of each type of vehicle on roads within each HPMS functional class. These factors were used to adjust the observed data estimate the yearly volume counts.

## Estimation of Vehicle-Miles of Travel

Since road sections were selected with probability of selection proportional to the the section's length, the number of vehicle-miles traveled for a given vehicle type on roads of a certain highway class is simply the arithmetic average of the number of vehicles counted on the sample sites in that class times the total number of actual miles in the class times 365 days a year.

Table B.3 through B.8 show the 1983 percentage VMT computed for the formula used in the present costateen vehicle classes and all the weight groups used in the present costallocation study. Similar traffic data were also estimated for the years and 1986 on the basis of the projected growth rates by vehicle class. The traffic growth rates were estimated on the basis of the model used by the I cost allocation study [9]. The formula used is as follows:

$$VMT_1 = VMT_0 e^{r * y}$$



Table B.3. Percent VMT of Vehicle Classes on Rural Interstate (1983)

| Veh   | Sub-  | Vehicle    | -M(1o.7   | Veh  | Sub-    | Vehicle   | -Mile Z   |
|-------|-------|------------|-----------|------|---------|-----------|-----------|
|       |       |            | Sub-Group |      |         | Veh Class | Sub-Group |
| CISSS | Group | VEIL CIABB | 3db-Grodb | 0240 | , orony |           |           |
| 1     | 1     | 15.640     | 15.640    | 11   | 6       |           | 0.230     |
| •     | •     | 131040     |           | 11   | 7       |           | 0.195     |
| 2     | 1     | 48.840     | 48.840    | 11   | 8       |           | 0.180     |
| 2     | 1     | 40.040     | 40.040    | 11   | 9       |           | 0.213     |
| _     |       |            | 0.051     | 11   | 10      |           | 0.195     |
| 3     | 1     | 2.400      | 0.054     |      |         |           | 0.195     |
| 3     | 2     |            | 0.182     | 11   | 11      |           | 0.180     |
| 3     | 3     |            | 0.218     | 11   | 12      |           |           |
| 3     | 4     |            | 0.618     | 11   | 13      |           | 0.148     |
| 3     | 5     |            | 0.473     |      |         | 07 000    | 0.05/     |
| 3     | 6     |            | 0.346     | 12   | 1       | 27.200    | 0.054     |
| 3     | 7     |            | 0.182     | 12   | 2       |           | 0.272     |
| 3     | 8     |            | 0.145     | 12   | 3       |           | 0.944     |
| 3     | 9     |            | 0.182     | 12   | 4       |           | 2.657     |
|       |       |            |           | 12   | 5       |           | 2.149     |
| 4     | 1     | 0.310      | 0.310     | 12   | 6       |           | 1.333     |
|       |       |            |           | 12   | 7       |           | 1.115     |
| 5     | 1     | 1.120      | 1.120     | 12   | 8       |           | 0.979     |
| -     |       |            | *         | 12   | 9       |           | 0.898     |
| 6     | 1     | 0.420      | 0.051     | 12   | 10      |           | 0.827     |
| 6     | 2     |            | 0.025     | 12   | 11      |           | 0.800     |
| 6     | 3     |            | 0.038     | 12   | 12      |           | 0.770     |
| 6     | 4     |            | 0.076     | 12   | 13      |           | 0.680     |
| 6     | 5     |            | 0.064     | 12   | 14      |           | 0.800     |
| 6     | 6     |            | 0.038     | 12   | 15      |           | 0.870     |
|       | 7     |            | 0.038     | 12   | 16      |           | 1.104     |
| 6     | 8     |            | 0.025     | 12   | 17      |           | 0.979     |
| 6     | 9     |            | 0.023     | 12   | 18      |           | 0.925     |
| 6     | 9     |            | 0.004     | 12   | 19      |           | 1.034     |
| -     |       | 0.360      | 0.012     | 12   | 20      |           | 1.496     |
| 7     | 1     | 0.360      | 0.012     | 12   | 21      |           | 2.258     |
| 7     | 2     |            |           | 12   | 22      |           | 2.394     |
| 7     | 3     |            | 0.048     | 12   | 23      |           | 1.170     |
| 7     | 4     |            | 0.072     | 12   | 24      |           | 0.552     |
| 7     | 5     |            | 0.036     | 12   | 25      |           | 0.044     |
| 7     | 6     |            | 0.012     | 12   | 26      |           | 0.101     |
| 7     | 7     |            | 0.108     | 12   | 20      |           | 0.20.     |
| 7     | 8     |            | 0.036     | 13   | 1       | 0.760     | 0.088     |
| 7     | 9     |            | 0.012     | 13   | 2       | 0.700     | 0.146     |
| _     |       |            | 0.060     | 13   | 3       |           | 0.029     |
| 8     | 1     | 0.060      | 0.060     | 13   | 4       |           | 0.059     |
|       |       |            |           |      | 5       |           | 0.029     |
| 9     | 1     | 0.170      | 0.085     | 13   | 6       |           | 0.029     |
| 9     | 2     |            | 0.085     | 13   |         |           | 0.059     |
|       |       |            |           | 13   | 7       |           | 0.029     |
| 10    | 1     | 0.070      | 0.014     | 13   | 8       |           |           |
| 10    | 2     |            | 0.014     | 13   | 9       |           | 0.029     |
| 10    | 3     |            | 0.028     | 13   | 10      |           | 0.059     |
| 10    | 4     |            | 0.014     | 13   | 11      |           | 0.029     |
|       |       |            |           | 13   | 12      |           | 0.087     |
| 11    | 1     | 2.500      | 0.050     | 13   | 13      |           | 0.087     |
| 11    | 2     |            | 0.097     |      |         |           | 0.053     |
| 11    | 3     |            | 0.360     | 14   | 1       | 0.160     | 0.053     |
| 11    | 4     |            | 0.163     | 14   | 2       |           | 0.053     |
| 11    | 5     |            | 0.295     | 14   | 3       |           | 0.053     |
|       |       |            |           |      |         |           |           |



Table B.4. Percent VMT of Vehicle Classes on Urban Interstate (1983)

|       |       |           | M4.1 . W  | Veh   | Sub-  | Vehicle-  | -Mila 7   |
|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh   | Sub-  | Vehicle-  |           |       |       | Veh Class |           |
| Class | Group | Veh Class | Sub-Group | CIASS | Group | VEH CIASS | 3db drodp |
| I     | 1     | 20.700    | 20.700    | 11    | 6     |           | 0.074     |
|       |       | 201700    | 201.00    | 11    | 7     |           | 0.062     |
| 2     | 1     | 63.300    | 63.300    | 11    | 8     |           | 0.058     |
| 2     | r     | 63.300    | 03.300    | 11    | 9     |           | 0.068     |
| _     |       | 0.140     | 0.0/0     | 11    | 10    |           | 0.062     |
| 3     | 1     | 2.160     | 0.049     |       |       |           | 0.062     |
| 3     | 2     |           | 0.164     | 11    | 11    |           |           |
| 3     | 3     |           | 0.196     | 11    | 12    |           | 0.058     |
| 3     | 4     |           | 0.556     | 11    | 13    |           | 0.047     |
| 3     | 5     |           | 0.426     |       |       |           |           |
| 3     | 6     |           | 0.311     | 12    | 1     | 10.400    | 0.021     |
| 3     | 7     | •         | 0.164     | 12    | 2     |           | 0.104     |
| 3     | 8     |           | 0.131     | 12    | 3     |           | 0.361     |
| 3     | 9     |           | 0.164     | 12    | 4     |           | 1.016     |
|       | -     |           |           | 12    | 5     |           | 0.822     |
| 4     | 1     | 0.290     | 0.290     | 12    | 6     |           | 0.510     |
| -     | •     | 0.27      |           | 12    | 7     |           | 0.426     |
| 5     | 1     | 0.860     | 0.860     | 12    | 8     |           | 0.374     |
| ,     | •     | 0.000     | 0.000     | 12    | 9     |           | 0.343     |
| 6     | 1     | 0.370     | 0.045     | 12    | 10    |           | 0.316     |
| 6     | 2     | 0.370     | 0.022     | 12    | 11    |           | 0.306     |
| 6     | 3     |           | 0.034     | 12    | 12    |           | 0.294     |
| 6     | 4     |           | 0.067     | 12    | 13    |           | 0.260     |
|       | 5     |           | 0.056     | 12    | 14    |           | 0.306     |
| 6     | 6     |           | 0.034     | 12    | 15    |           | 0.333     |
| 6     |       |           |           | 12    | 16    |           | 0.422     |
| 6     | 7     |           | 0.034     | 12    | 17    |           | 0.374     |
| 6     | 8     |           | 0.022     | 12    | 18    |           | 0.354     |
| 6     | 9     |           | 0.056     | 12    | 19    |           | 0.395     |
|       |       |           |           |       |       |           | 0.572     |
| 7     | 1     | 0.260     | 0.009     | 12    | 20    |           | 0.863     |
| 7     | 2     |           | 0.017     | 12    | 21    |           |           |
| 7     | 3     |           | 0.035     | 12    | 22    |           | 0.915     |
| 7     | 4     |           | 0.052     | 12    | 23    |           | 0.447     |
| 7     | 5     |           | 0.026     | 12    | 24    |           | 0.211     |
| 7     | 6     |           | 0.009     | 12    | 25    |           | 0.017     |
| 7     | 7     |           | 0.078     | 12    | 26    |           | 0.038     |
| 7     | 8     |           | 0.026     |       |       |           |           |
| 7     | 9     |           | 0.009     | 13    | 1     | 0.400     | 0.046     |
|       |       |           |           | 13    | 2     |           | 0.077     |
| 8     | 1     | 0.300     | 0.300     | 13    | 3     |           | 0.015     |
| _     |       |           |           | 13    | 4     |           | 0.031     |
| 9     | 1     | 0.070     | 0.035     | 13    | 5     |           | 0.015     |
| ģ     | 2     |           | 0.035     | 13    | 6     |           | 0.015     |
| ,     | -     |           | ******    | 13    | 7     |           | 0.031     |
| 10    | I     | 0.030     | 0.006     | 13    | 8     |           | 0.015     |
| 10    | 2     | 0.030     | 0.006     | 13    | 9     |           | 0.015     |
| 10    | 3     |           | 0.012     | 13    | 10    |           | 0.031     |
| 10    | 4     |           | 0.006     | 13    | 11    |           | 0.015     |
| 10    | *     |           | 0.000     | 13    | 12    |           | 0.046     |
| 11    | 1     | 0.800     | 0.016     | 13    | 13    |           | 0.046     |
| 11    | 2     | 0.000     | 0.031     |       |       |           |           |
| 11    | 3     |           | 0.115     | 14    | 1     | 0.060     | 0.015     |
|       | 4     |           | 0.052     | 14    | 2     |           | 0.022     |
| 11    | 5     |           | 0.094     | 14    | 3     |           | 0.022     |
| 11    | )     |           | 0.034     | 14    | _     |           |           |



Table B.5. Percent VMT of Vehicle Classes on State Primary (1983)

|       |       |           |           | Vel | _           | Sub-  | Vehicle-   | -M11e 7   |
|-------|-------|-----------|-----------|-----|-------------|-------|------------|-----------|
| Veh   | Sub-  | Vehicle-  | Mile Z    | Vel | n           |       | Veh Class  | Sub-Group |
| Class | Group | Veh Class | Sub-Group | CI  | <b>a</b> 35 | Group | AGII CIGGO | Sub Stoop |
| 1     | 1     | 20.200    | 20.200    | 1   | 1           | 6     |            | 0.059     |
| 1     |       | 20.200    | 201200    | 1   |             | 7     |            | 0.007     |
|       |       | (0 (00    | 60 600    | · 1 |             | 8     |            | 0.008     |
| 2     | 1     | 68.600    | 68.600    | 1   |             | 9     |            | 0.007     |
|       |       |           |           |     |             | 10    |            | 0.008     |
| 3     | 1     | 2.400     | 0.138     | 1   |             |       |            | 0.005     |
| 3     | 2     |           | 0.369     | 1   |             | 11    |            | 0.005     |
| 3     | 3     |           | 0.369     | 1   |             | 12    |            |           |
| 3     | 4     |           | 0.509     | 1   | .1          | 13    |            | 0.005     |
| 3     | 5     |           | 0.415     |     |             |       |            |           |
| 3     | 6     |           | 0.230     | 1   | 2           | 1     | 5.770      | 0.017     |
| 3     | 7     |           | 0.139     | 1   | 2           | 2     |            | 0.121     |
| 3     | 8     |           | 0.139     | 1   | 2           | 3     |            | 0.563     |
| 3     | 9     |           | 0.091     | 1   | 2           | 4     |            | 0.733     |
| ,     | ,     |           | 0.007     | 1   | 2           | 5     |            | 0.444     |
| ,     | 1     | 0.090     | 0.090     |     | 2           | 6     |            | 0.271     |
| 4     | 1     | 0.090     | 0.000     |     | 2           | 7     |            | 0.171     |
|       |       | 0 500     | 0 520     |     | 2           | 8     |            | 0.185     |
| 5     | 1     | 0.530     | 0.530     | _   | 12          | 9     |            | 0.138     |
|       |       |           |           |     |             |       |            | 0.153     |
| 6     | 1     | 0.940     | 0.329     |     | 12          | 10    |            | 0.190     |
| 6     | 2     |           | 0.141     |     | 12          | 11    |            |           |
| 6     | 3     |           | 0.188     |     | 12          | 12    |            | 0.138     |
| 6     | 4     |           | 0.141     | 1   | 12          | 13    |            | 0.138     |
| 6     | 5     |           | 0.023     | 1   | 12          | 14    |            | 0.205     |
| 6     | 6     |           | 0.023     | 1   | 12          | 15    |            | 0.138     |
| 6     | 7     |           | 0.031     |     | 12          | 16    |            | 0.375     |
| 6     | 8     |           | 0.031     |     | 12          | 17    |            | 0.254     |
|       | 9     |           | 0.032     |     | 12          | 18    |            | 0.271     |
| 6     | 9     |           | 0.032     |     | 12          | 19    |            | 0.188     |
| _     |       | 0 000     | 0.066     |     | 12          | 20    |            | 0.171     |
| 7     | 1     | 0.330     | 0.066     |     | 12          | 21    |            | 0.375     |
| 7     | 2     |           | 0.022     |     | 12          | 22    |            | 0.306     |
| 7     | 3     |           | 0.022     |     |             |       |            | 0.171     |
| 7     | 4     |           | 0.022     |     | 12          | 23    |            | 0.171     |
| 7     | 5     |           | 0.040     |     | 12          | 24    |            | 0.017     |
| 7     | 6     |           | 0.040     |     | 12          | 25    |            |           |
| 7     | 7     |           | 0.040     |     | 12          | 26    |            | 0.017     |
| 7     | 8     |           | 0.040     |     |             |       |            |           |
| 7     | 9     |           | 0.040     |     | 13          | 1     | 0.150      | 0.045     |
| ,     |       |           |           |     | 13          | 2     |            | 0.030     |
| 8     | 1     | 0.210     | 0.210     |     | 13          | 3     |            | 0.022     |
| 0     |       | 0.2.10    | 0.223     |     | 13          | 4     |            | 0.015     |
| 0     | 1     | 0.190     | 0.027     |     | 13          | 5     |            | 0.008     |
| 9     |       | 0.130     | 0.163     |     | 13          | 6     |            | 0.008     |
| 9     | 2     |           | 0.103     |     | 13          | 7     |            | 0.008     |
|       |       | 0.070     | 0.010     |     | 13          | 8     |            | 0.003     |
| 10    | 1     | 0.040     | 0.010     |     | 13          | 9     |            | 0.003     |
| 10    | 2     |           | 0.010     |     | 13          | 10    |            | 0.003     |
| 10    | 3     |           | 0.010     |     |             |       |            | 0.003     |
| 10    | 4     |           | 0.010     |     | 13          | 11    |            | 0.002     |
|       |       |           |           |     | 13          | 12    |            |           |
| 11    | 1     | 0.470     | 0.030     |     | 13          | 13    |            | 0.002     |
| 11    | 2     |           | 0.073     |     |             |       |            | 0.027     |
| 11    | 3     |           | 0.117     |     | 14          | 1     | 0.110      | 0.037     |
| 11    | 4     |           | 0.088     |     | 14          | 2     |            | 0.037     |
| 11    | 5     |           | 0.059     |     | 14          | 3     |            | 0.037     |
| 11    | J     |           | 0.037     |     |             |       |            |           |



Table B.6. Percent VMT of Vehicle Classes on State Secondary (1983)

|       |       |           | W41- W    | Vel | h   | Sub-  | Vehicle-   | Mile I    |
|-------|-------|-----------|-----------|-----|-----|-------|------------|-----------|
| Veh   | Sub-  | Vehicle-  |           |     |     |       | Veh Class  |           |
| Class | Group | Veh Class | Sub-Group | CI  | 435 | Group | 7611 01000 | oob orosp |
| 1     | 1     | 20.200    | 20.200    | 1   | 1   | 6     |            | 0.084     |
|       |       | 20.200    | 20.200    | 1   |     | 7     |            | 0.021     |
|       |       | 71 750    | 71.750    | î   |     | 8     |            | 0.021     |
| 2     | 1     | 71.750    | /1./30    | 1   |     | 9     |            | 0.011     |
|       |       |           |           | _   | _   |       |            | 0.011     |
| 3     | 1     | 3.300     | 0.906     | 1   |     | 10    |            | 0.011     |
| 3     | 2     |           | 0.323     |     | 1   | 11    |            |           |
| 3     | 3     |           | 0.906     | -   | 1   | 12    |            | 0.011     |
| 3     | 4     |           | 0.518     | 1   | 1   | 13    |            | 0.021     |
| 3     | 5     |           | 0.129     |     |     |       |            |           |
| 3     | 6     |           | 0.323     | 1   | 2   | 1     | 2.500      | 0.018     |
| 3     | 7     |           | 0.129     | 1   | 2   | 2     |            | 0.035     |
| 3     | 8     |           | 0.033     | 1   | 2   | 3     |            | 0.104     |
| 3     | 9     |           | 0.033     | 1   | 2   | 4     |            | 0.470     |
| ,     | ,     |           | 01033     |     | 2   | 5     |            | 0.104     |
| ,     |       | 0.060     | 0.060     |     | 2   | 6     |            | 0.190     |
| 4     | 1     | 0.000     | 0.000     |     | 2   | 7     |            | 0.018     |
| _     |       | 0 (00     | 0 (00     | -   | 2   | 8     |            | 0.070     |
| 5     | 1     | 0.490     | 0.490     | _   | 2   | 9     |            | 0.156     |
|       |       |           | 0.100     | -   | 2   | 10    |            | 0.140     |
| 6     | 1     | 0.520     | 0.182     |     |     | _     |            | 0.035     |
| 6     | 2     |           | 0.130     |     | 2   | 11    |            | 0.052     |
| 6     | 3     |           | 0.052     |     | 2   | 12    |            | 0.032     |
| 6     | 4     |           | 0.052     |     | 2   | 13    |            |           |
| 6     | 5     |           | 0.013     |     | 2   | 14    |            | 0.052     |
| 6     | 6     |           | 0.013     |     | 2   | 15    |            | 0.052     |
| 6     | 7     |           | 0.013     |     | 2   | 16    |            | 0.035     |
| 6     | 8     |           | 0.013     | 1   | 12  | 17    |            | 0.052     |
| 6     | 9     |           | 0.052     | 1   | 12  | 18    |            | 0.190     |
| •     |       |           |           | 1   | 12  | 19    |            | 0.087     |
| 7     | 1     | 0.270     | 0.034     | 1   | 12  | 20    |            | 0.155     |
| 7     | 2     | 012/0     | 0.034     | 1   | 12  | 21    |            | 0.190     |
| 7     | 3     |           | 0.034     |     | 12  | 22    |            | 0.104     |
|       | 4     |           | 0.034     |     | 12  | 23    |            | 0.104     |
| 7     |       |           | 0.034     |     | 12  | 24    |            | 0.013     |
| 7     | 5     |           |           |     | 12  | 25    |            | 0.002     |
| 7     | 6     |           | 0.027     |     | 12  | 26    |            | 0.002     |
| 7     | 7     |           | 0.027     | 4   | 1.4 | 20    |            | 0,000     |
| 7     | 8     |           | 0.027     | ,   | 13  | 1     | 0.090      | 0.027     |
| 7     | 9     |           | 0.027     |     |     | 2     | 0.070      | 0.027     |
|       |       |           |           |     | 13  |       |            | 0.018     |
| 8     | I     | 0.210     | 0.210     |     | 13  | 3     |            | 0.009     |
|       |       |           |           |     | 13  | 4     |            |           |
| 9     | 1     | 0.030     | 0.004     |     | 13  | 5     |            | 0.009     |
| 9     | 2     |           | 0.026     |     | 13  | 6     |            | 0.        |
|       |       |           |           |     | 13  | 7     |            | 0.        |
| 10    | 1     | 0.060     | 0.015     |     | 13  | 8     |            | 0.        |
| 10    | 2     |           | 0.015     |     | 13  | 9     |            | 0.        |
| 10    | 3     |           | 0.015     |     | 13  | 10    |            | 0.        |
| 10    | 4     |           | 0.015     |     | 13  | 11    |            | 0.        |
|       | •     |           |           |     | 13  | 12    |            | 0.        |
| 11    | 1     | 0.460     | 0.063     |     | 13  | 13    |            | 0.        |
| 11    | 2     | 0.400     | 0.063     |     |     |       |            |           |
| 11    | 3     |           | 0.084     |     | 14  | 1     | 0.060      | 0.020     |
| 11    | 4     |           | 0.042     |     | 14  | 2     |            | 0.020     |
| 11    | 5     |           | 0.021     |     | 14  | 3     |            | 0.020     |
| 11    | )     |           | 0.021     |     | -   |       |            |           |



Table B.7. Percent VMT of Vehicle Classes on County Roads (1983)

|        |       | W. b. 4 - 1 - | W 1 - 9       | Vah   | Sub-  | Vehicle-   | -W11a 7   |
|--------|-------|---------------|---------------|-------|-------|------------|-----------|
| Veh    | Sub-  | Vehicle       |               | Veh   |       | Veh Class  |           |
| Class  | Group | Veh Class     | Sub-Group     | CIRRR | Group | AGII CTGBB | 3db-Group |
| 1      | 1     | 17.950        | 17.950        | 11    | 6     |            | 0.049     |
|        |       | 17.730        | 1, 1, 2, 3, 0 | 11    | 7     |            | 0.012     |
| 2      | 1     | 75.340        | 75.340        | 11    | 8     |            | 0.012     |
| 2      | 1     | 734540        | 738340        | 11    | 9     |            | 0.006     |
| 3      | 1     | 3.900         | 1.071         | 11    | 10    |            | 0.006     |
| 3      | 2     | 3.900         | 0.382         | 11    | 11    |            | 0.006     |
| 3      | 3     |               | 1.071         | 11    | 12    |            | 0.006     |
| 3      | 4     |               | 0.612         | 11    | 13    |            | 0.012     |
| 3      | 5     |               | 0.152         |       |       |            |           |
| 3      | 6     |               | 0.382         | 12    | 1     | 0.630      | 0.004     |
| 3      | 7     |               | 0.152         | 12    | 2     |            | 0.009     |
| 3      | 8     |               | 0.039         | 12    | 3     |            | 0.026     |
| 3      | 9     |               | 0.039         | 12    | 4     |            | 0.118     |
| )      | 7     |               | 0.039         | 12    | 5     |            | 0.026     |
| 4      | 1     | 0.050         | 0.050         | 12    | 6     |            | 0.048     |
| 4      | ī     | 0.030         | 0.030         | 12    | 7     |            | 0.004     |
| 5      | 1     | 0.630         | 0.630         | 12    | á     |            | 0.018     |
| )      | 1     | 0.030         | 0.030         | 12    | 9     |            | 0.039     |
| ,      | 1     | 0.860         | 0.301         | 12    | 10    |            | 0.035     |
| 6      | 2     | 0.000         | 0.215         | 12    | 11    |            | 0.009     |
| 6      | 3     |               | 0.086         | 12    | 12    |            | 0.013     |
| 6      | 4     |               | 0.086         | 12    | 13    |            | 0.018     |
| 6<br>6 | 5     |               | 0.000         | 12    | 14    |            | 0.013     |
|        | 6     |               | 0.021         | 12    | 15    |            | 0.013     |
| 6      | 7     |               | 0.021         | 12    | 16    |            | 0.009     |
| 6      | 8     |               | 0.021         | 12    | 17    |            | 0.013     |
| 6      | 9     |               |               | 12    | 18    |            | 0.048     |
| 6      | 9     |               | 0.086         | 12    | 19    |            | 0.022     |
| 7      | ,     | 0.050         | 0.006         | 12    | 20    |            | 0.039     |
| 7      | 1     | 0.050         | 0.006         | 12    | 21    |            | 0.048     |
| 7<br>7 | 2     |               | 0.006         | 12    | 22    |            | 0.026     |
| 7      | 4     |               | 0.006         | 12    | 23    |            | 0.026     |
| 7      | 5     |               | 0.005         | 12    | 24    |            | 0.003     |
| 7      | 6     |               | 0.005         | 12    | 25    |            | 0.001     |
| 7      | 7     |               | 0.005         | 12    | 26    |            | 0.001     |
| 7      | 8     |               | 0.005         |       |       |            |           |
| 7      | 9     |               | 0.005         | 13    | 1     | 0.180      | 0.054     |
| ,      | ,     |               | 0.003         | 13    | 2     |            | 0.054     |
| 8      | 1     | 0.            | 0.            | 13    | 3     |            | 0.036     |
|        | •     | •             | •             | 13    | 4     |            | 0.018     |
| 9      | 1     | 0.050         | 0.007         | 13    | 5     |            | 0.018     |
| 9      | 2     | 0.030         | 0.043         | 13    | 6     |            | 0.        |
| ,      | 2     |               | 0.043         | 13    | 7     |            | 0.        |
| 10     | 1     | 0.            | 0.            | 13    | 8     |            | 0.        |
| 10     | 2     | •             | o.            | 13    | 9     |            | 0.        |
| 10     | 3     |               | 0.            | 13    | 10    |            | 0.        |
| 10     | 4     |               | 0.            | 13    | 11    |            | 0.        |
| 10     | 7     |               |               | 13    | 12    |            | 0.        |
| 11     | 1     | 0.270         | 0.037         | 13    | 13    |            | 0.        |
| 11     | 2     | 0.2.0         | 0.037         |       |       |            |           |
| 11     | 3     |               | 0.049         | 14    | 1     | 0.090      | 0.030     |
| 11     | 4     |               | 0.025         | 14    | 2     |            | 0.030     |
| 11     | 5     |               | 0.012         | 14    | 3     |            | 0.030     |
| 4.4    | ,     |               | 0.010         | - '   |       |            |           |



Table B.8. Percent VMT of Vehicle Classes on City Streets (1983)

| Veh      | Sub-   | Vehicle   |                | Veh      | Sub-     | Vehicle<br>Veh Class |                |
|----------|--------|-----------|----------------|----------|----------|----------------------|----------------|
| Class    | Group  | ven Class | Sub-Group      | CIASS    | Group    | ven class            | Sab Group      |
| i        | 1      | 19.340    | 19.340         | 11       | 6        |                      | 0.078          |
|          |        |           |                | 11       | 7        |                      | 0.019          |
| 2        | 1      | 74.000    | 74.000         | 11       | 8        |                      | 0.019          |
|          |        |           |                | 11       | 9        |                      | 0.010          |
| 3        | 1      | 2.160     | 0.593          | 11       | 10       |                      | 0.010          |
| 3        | 2      |           | 0.212          | 11       | 11       |                      | 0.010          |
| 3        | 3      |           | 0.593          | 11       | 12       |                      | 0.010          |
| 3        | 4<br>5 |           | 0.339          | 11       | 13       |                      | 0.020          |
| 3        | 6      |           | 0.084<br>0.212 | 12       | 1        | 2.360                | 0.017          |
| 3<br>3   | 7      |           | 0.084          | 12       | 2        | 2.300                | 0.033          |
| 3        | 8      |           | 0.022          | 12       | 3        |                      | 0.098          |
| 3        | 9      |           | 0.022          | 12       | 4        |                      | 0.444          |
| ,        | ,      |           | 0.022          | 12       | 5        |                      | 0.098          |
| 4        | 1      | 0.230     | 0.230          | 12       | 6        |                      | 0.179          |
| ~        | •      | 01230     | 0.200          | 12       | 7        |                      | 0.017          |
| 5        | 1      | 0.480     | 0.480          | 12       | 8        |                      | 0.066          |
|          | _      |           |                | 12       | 9        |                      | 0.148          |
| 6        | 1      | 0.720     | 0.252          | 12       | 10       |                      | 0.132          |
| 6        | 2      |           | 0.180          | 12       | 11       |                      | 0.033          |
| 6        | 3      |           | 0.072          | 12       | 12       |                      | 0.050          |
| 6        | 4      |           | 0.072          | 12       | 13       |                      | 0.066          |
| 6        | 5      |           | 0.018          | 12       | 14       |                      | 0.050          |
| 6        | 6      |           | 0.018          | 12       | 15       |                      | 0.050          |
| 6        | 7      |           | 0.018          | 12       | 16       |                      | 0.033          |
| 6        | 8      |           | 0.018          | 12       | 17       |                      | 0.050          |
| 6        | 9      |           | 0.072          | 12       | 18       |                      | 0.179<br>0.082 |
| -        |        | 0.000     | 0.008          | 12<br>12 | 19<br>20 |                      | 0.062          |
| 7<br>7   | 1 2    | 0.060     | 0.008          | 12       | 21       |                      | 0.179          |
| 7        | 3      |           | 0.008          | 12       | 22       |                      | 0.098          |
| 7        | 4      |           | 0.008          | 12       | 23       |                      | 0.098          |
| 7        | 5      |           | 0.006          | 12       | 24       |                      | 0.012          |
| 7        | 6      |           | 0.006          | 12       | 25       |                      | 0.002          |
| 7        | 7      |           | 0.006          | 12       | 26       |                      | 0.002          |
| 7        | 8      |           | 0.006          |          |          |                      |                |
| 7        | 9      |           | 0.006          | 13       | 1        | 0.097                | 0.029          |
|          |        |           |                | 13       | 2        |                      | 0.029          |
| 8        | 1      | 0.        | 0.             | 13       | 3        |                      | 0.019          |
|          |        |           |                | 13       | 4        |                      | 0.010          |
| 9        | 1      | 0.050     | 0.007          | 13       | 5        |                      | 0.010          |
| 9        | 2      |           | 0.043          | 13       | 6<br>7   |                      | 0.             |
|          |        | 0.045     | 0.011          | 13<br>13 | 8        |                      | 0.             |
| 10       | 1      | 0.045     | 0.011          | 13       | 9        |                      | 0.             |
| 10       | 2      |           | 0.011          | 13       | 10       |                      | 0.             |
| 10<br>10 | 3      |           | 0.011          | 13       | 11       |                      | 0.             |
| 10       | 4      |           | 0.011          | 13       | 12       |                      | 0.             |
| 11       | 1      | 0.430     | 0.058          | 13       | 13       |                      | 0.             |
| 11       | 2      | 0.450     | 0.058          | -        |          |                      |                |
| 11       | 3      |           | 0.078          | 14       | 1        | 0.032                | 0.011          |
| 11       | 4      |           | 0.039          | 14       | 2        |                      | 0.011          |
| 11       | 5      |           | 0.020          | 14       | 3        |                      | 0.011          |
|          |        |           |                |          |          |                      |                |



where,

VMT, = future year VMT for a vehicle class;

VMT = base year VMT of the given vehicle class;

r = rate of traffic growth per year for the vehicle class;

y = number of intervening years between the base and future periods.

The appropriate r-values for various classes were estimated on the basis of the 1977 and the 1985 projected national data [35] used in the Federal study [9]. The 1983 Indiana VMT figures were then projected to 1985-86 using the above formula. The 1985-86 percentage VMT values are shown in Table B.9 through B.14. The total annual VMT values for 1983 and 1985-86 by highway functional class are given in Table B.15.

# VMT Correspondence Matrices for Registered and Operating Weight Groups

Truck registration fees in Indiana are collected in terms of vehicle registration weight classification which is different from the operating weight vehicle classification defined in Tables 1 and 2 and used in cost-responsibility computations. The vehicle registration weight classification used by the Indiana Bureau of Motor Vehicles is summarized in Table B.16.

The development of the relationship between the two types of classification is not straight forward because of the fact that vehicle weights were defined differently in each. While the cost responsibility classification was based upon the gross operating weights of vehicles, gross registered weight capacity was used in the Bureau of Motor Vehicles classification. For the purpose of distributing revenues to appropriate cost responsibility vehicle



classes and weight groups, a series of correspondence matrices were developed to relate registered vehicle weight classes to operating vehicle weight classes. These matrices are presented in Tables B.17 through B.25.

The primary source of data for establishing these correspondence matrices was the IDOH Truck Weight Survey Records. Every two years, IDOH conducts a truck weight survey. Data on truck weights by truck type are collected at 28 permanent weigh stations and at several temporary locations. The data file includes records of the truck type, axle configuration, axle weights, registration weight classification and other administrative identification codes for every truck weighed. The 1981 and 1983 truck weight survey data were used in this study.

The procedure used in setting up the corresponding matrices is simple in concept. It was basically an accounting process by recording each truck weight data in the appropriate cell of one of the nine two-way classification matrices. These numbers were subsequently converted into percentages for revenue allocation purpose.

Due to the limited amount of data available from IDOH Truck Weight Survey Records, some empty cells were observed within a row of cells with finite values. These inconsistencies were corrected on the basis of information from other midwestern states [4,21,48] and the 1977 <u>Truck Inventory and Use Survey</u> [5].



Table B.9. Percent VMT of Vehicle Classes on Rural Interstate (1985-86)

| 1         1         15.563         15.563         11         6         0.233           2         1         48.599         48.599         11         8         0.182           3         1         2.331         0.053         11         19         0.215           3         2         0.176         11         11         12         0.182           3         4         0.598         11         13         0.148           3         5         0.458         11         13         0.148           3         6         0.334         12         1         27.554         0.055           3         7         0.176         12         2         0.275           3         8         0.141         12         3         0.954           4         1         0.302         0.302         12         6         1.348           5         1         1.114         1.14         12         8         0.990           6         1         0.417         0.049         12         10         0.836           5         1         1.114         1.14         12         8         0.990 </th <th>Veh<br/>Class</th> <th>Sub-<br/>Group</th> <th>Vehicle-<br/>Veh Class</th> <th></th> <th>Veh<br/>Class</th> <th>Sub-<br/>Group</th> <th>Vehicle-<br/>Veh Class</th> <th></th>   | Veh<br>Class | Sub-<br>Group | Vehicle-<br>Veh Class |        | Veh<br>Class | Sub-<br>Group | Vehicle-<br>Veh Class |       |
|--|--------------|---------------|-----------------------|--------|--------------|---------------|-----------------------|-------|
| 11   | 1            | 1             | 15.563                | 15.563 | 11           | 6             |                       | 0.233 |
| 2         1         48,599         48,599         11         8         0.182           3         1         2.331         0.053         11         10         0.197           3         2         0.176         11         11         0.197           3         3         0.211         11         12         0.182           3         4         0.598         11         13         0.148           3         5         0.458         0.141         12         2         0.275           3         6         0.334         12         1         27.554         0.055           3         7         0.176         12         2         0.275           3         8         0.141         12         3         0.954           4         1         0.302         12         6         1.348           12         1         0.342         12         1         27.554         0.055           3         9         0.184         12         1         2.687         1.128           4         1         0.302         12         1         1         0.894           5  | •            | •             |                       |        |              |               |                       |       |
| 11    9  | 2            | 1             | 48 500                | 48 599 |              |               |                       |       |
| 3         1         2.331         0.053         11         10         0.197           3         2         0.176         11         11         12         0.182           3         4         0.598         11         13         0.148           3         5         0.458         0.176         12         2         0.275           3         6         0.334         12         1         27.554         0.055           3         7         0.176         12         2         0.275           3         8         0.141         12         3         0.954           3         9         0.184         12         4         2.687           4         1         0.302         0.302         12         6         1.348           12         7         1.128         0.990         0.908           6         1         0.417         0.049         12         9         0.998           6         1         0.417         0.049         12         10         0.836           6         2         0.025         12         11         0.896         0.998           6 <td>2</td> <th></th> <td>40.333</td> <td>40.377</td> <td></td> <td></td> <td></td> <td></td>   | 2            |               | 40.333                | 40.377 |              |               |                       |       |
| 1  | 2            | ,             | 2 221                 | 0.053  |              |               |                       |       |
| 1  |              |               | 2.331                 |        |              |               |                       |       |
| 1  |              |               |                       |        |              |               |                       |       |
| 3  |              |               |                       |        |              |               |                       |       |
| 3         6         0.334         12         1         27.554         0.055           3         7         0.176         12         2         0.275           3         8         0.141         12         3         0.954           3         9         0.184         12         4         2.687           4         1         0.302         12         6         1.348           12         7         1.128         0.990           5         1         1.114         1.114         12         8         0.990           6         1         0.417         0.049         12         10         0.836           6         2         0.025         12         11         0.804           6         3         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.876           6         7         0.039         12         16         1.111           1         0.364         0.012         12         17         0.985  |              |               |                       |        | 11           | 1.3           |                       | 0.146 |
| 3         7         0.176         12         2         0.275           3         8         0.141         12         3         0.954           3         9         0.184         12         4         2.687           4         1         0.302         0.302         12         6         1.348           12         7         1.128         0.990         12         7         1.128           5         1         1.114         1.114         12         8         0.990           6         1         0.417         0.049         12         10         0.836           6         2         0.025         12         11         0.809           6         2         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.804           6         7         0.039         12         16         1.111           6         8         0.026         12         17         0.985           6         9         0.024         12  |              |               |                       |        |              |               |                       | 0.000 |
| 3       8       0.141       12       3       0.954         3       9       0.184       12       4       2.687         4       1       0.302       0.302       12       6       1.348         5       1       1.114       1.114       12       8       0.990         6       1       0.417       0.049       12       10       0.836         6       2       0.025       12       11       0.809         6       3       0.037       12       12       0.778         6       4       0.074       12       13       0.684         6       5       0.064       12       14       0.804         6       6       0.039       12       15       0.876         6       7       0.039       12       16       1.111       0.985         6       9       0.064       12       18       0.930         12       19       1.040       19       12       19       1.040         7       1       0.364       0.012       12       20       1.505       1.505       11       1.006       1.008 <t< td=""><td></td><th></th><td></td><td></td><td></td><td></td><td>27.554</td><td></td></t<>  |              |               |                       |        |              |               | 27.554                |       |
| 1  |              |               |                       |        |              |               |                       |       |
| 12   5   2.173   1.348   1.3 | 3            | 8             |                       | 0.141  |              |               |                       |       |
| 4       1       0.302       0.302       12       6       1.348         5       1       1.114       1.114       12       8       0.990         6       1       0.417       0.049       12       10       0.836         6       2       0.025       12       11       0.809         6       3       0.037       12       12       0.778         6       4       0.074       12       13       0.684         6       5       0.064       12       14       0.804         6       6       0.039       12       15       0.876         6       7       0.039       12       15       0.876         6       7       0.039       12       16       1.111         6       8       0.026       12       17       0.985         6       9       0.064       12       18       0.930         12       19       1.040       12       18       0.930         7       1       0.364       0.012       12       20       1.505         7       2       0.024       12       21       21 <td>3</td> <th>9</th> <td></td> <td>0.184</td> <td></td> <td></td> <td></td> <td></td>  | 3            | 9             |                       | 0.184  |              |               |                       |       |
| 5         1         1.114         1.114         12         8         0.990           6         1         0.417         0.049         12         10         0.836           6         2         0.025         12         11         0.809           6         3         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.804           6         6         0.039         12         15         0.876           6         7         0.039         12         16         1.111           6         8         0.026         12         17         0.985           6         9         0.054         12         18         0.930           12         19         1.040           7         1         0.364         0.012         12         20         1.505           7         2         0.024         12         21         2.312         2.312           7         4         0.073         12         23         1.200         2.452   |              |               |                       |        | 12           |               |                       |       |
| 5         1         1.114         1.2         8         0.990           6         1         0.417         0.049         12         10         0.836           6         2         0.025         12         11         0.809           6         3         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.804           6         6         0.039         12         15         0.876           6         7         0.039         12         16         1.111           6         8         0.026         12         17         0.985           6         9         0.064         12         18         0.930           7         1         0.364         0.012         12         20         1.505           7         2         0.024         12         21         20         1.505           7         2         0.048         12         22         2.452         2.452           7         4         0.073         12  | 4            | 1             | 0.302                 | 0.302  | 12           | 6             |                       | 1.348 |
| 6       1       0.417       0.049       12       10       0.836         6       2       0.025       12       11       0.809         6       3       0.037       12       12       0.778         6       4       0.074       12       13       0.684         6       5       0.064       12       14       0.804         6       6       0.039       12       15       0.876         6       7       0.039       12       16       1.111         6       8       0.026       12       17       0.985         6       9       0.064       12       18       0.980         6       9       0.064       12       18       0.985         6       9       0.064       12       18       0.985         6       9       0.064       12       18       0.985         7       1       0.364       0.012       12       20       1.505         7       2       0.024       12       21       21       2.312         7       3       0.036       12       24       0.056   |              |               |                       |        | 12           | 7             |                       | 1.128 |
| 6       1       0.417       0.049       12       10       0.836         6       2       0.025       12       11       0.809         6       3       0.037       12       12       0.778         6       4       0.074       12       13       0.684         6       5       0.064       12       14       0.804         6       6       0.039       12       15       0.876         6       7       0.039       12       16       1.111         6       8       0.026       12       17       0.985         6       9       0.064       12       18       0.930         7       1       0.364       0.012       12       20       1.505         7       2       0.024       12       21       20       1.505         7       2       0.024       12       21       23       1.200         7       4       0.073       12       23       1.200         7       5       0.036       12       24       0.566         7       7       0.109       12       26       0.103  | 5            | 1             | 1.114                 | 1.114  | 12           | 8             |                       | 0.990 |
| 6 2 0.025 12 11 0.809 6 3 0.037 12 12 12 0.778 6 4 0.074 12 13 0.684 6 5 0.064 12 14 0.804 6 6 6 0.039 12 15 0.876 6 7 0.039 12 16 1.111 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 7 1 0.364 0.012 12 19 1.040 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.045 7 7 9 0.012 12 25 0.045 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 7 9 0.012 13 1 0.768 0.089 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 1 0.168 0.082 13 5 0.029 10 1 0.071 0.014 13 8 0.059 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 4 0.014 13 11 0.009 11 2 0.088 11 1 2.5527 0.051 13 13 10 0.090 11 2 0.090 11 2 0.364 14 1 0.162 0.054 11 1 0.076   | _            |               |                       |        | 12           | 9             |                       | 0.908 |
| 6         3         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.804           6         6         0.039         12         15         0.876           6         7         0.039         12         16         1.111           6         8         0.026         12         17         0.985           6         9         0.064         12         18         0.930           12         19         1.040         19         1.040           7         1         0.364         0.012         12         20         1.505           7         2         0.024         12         21         2.312         2.312           7         2         0.024         12         21         2.312         2.312           7         3         0.048         12         22         2.452         2.452           7         4         0.073         12         23         1.200         1.300           7         5         0.036         12 <td>6</td> <th>1</th> <td>0.417</td> <td>0.049</td> <td>12</td> <td>10</td> <td></td> <td>0.836</td>   | 6            | 1             | 0.417                 | 0.049  | 12           | 10            |                       | 0.836 |
| 6         3         0.037         12         12         0.778           6         4         0.074         12         13         0.684           6         5         0.064         12         14         0.804           6         6         0.039         12         15         0.876           6         7         0.039         12         16         1.111           6         8         0.026         12         17         0.985           6         9         0.064         12         18         0.930           12         19         1.040         19         1.040           7         1         0.364         0.012         12         20         1.505           7         2         0.024         12         21         2.312         2.312           7         2         0.024         12         21         2.312         2.312           7         3         0.048         12         22         2.452         2.452           7         4         0.073         12         23         1.200         1.300           7         5         0.036         12 <td>6</td> <th>2</th> <td></td> <td>0.025</td> <td>12</td> <td>11</td> <td></td> <td>0.809</td>  | 6            | 2             |                       | 0.025  | 12           | 11            |                       | 0.809 |
| 6 4 0.074 12 13 0.684 6 5 0.064 12 14 0.804 6 6 6 0.039 12 15 0.876 6 7 0.039 12 16 1.111 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 17 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.045 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 3 0.028 13 10 0.029 10 4 0.014 13 9 0.029 11 3 1 0.069 11 1 2.527 0.051 13 11 0.009 11 2 0.099 11 3 12 0.088 11 1 2.527 0.051 13 13 0.0090 11 2 0.064 14 1 0.069 11 1 0.071 1 0.014 13 11 0.0099 11 1 3 0.364 14 1 0.162 0.054 11 1 0.364 0.364 14 1 0.162 0.054  |              | 3             |                       |        | 12           | 12            |                       | 0.778 |
| 6 5 0.064 12 14 0.804 6 6 6 0.039 12 15 0.876 6 7 0.039 12 16 1.111 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 12 20 1.505 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 13 4 0.059 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 3 0.028 13 10 0.029 11 1 2.527 0.051 13 12 0.068 11 1 2.527 0.051 13 13 0.009 11 1 2.527 0.051 13 13 10 0.029 11 3 12 0.088 11 1 2.527 0.051 13 13 10 0.029 11 3 12 0.088 11 1 2.527 0.051 13 13 10 0.090 11 2 0.099 11 3 12 0.088 11 1 1 2.527 0.051 13 13 10 0.090  |              | 4             |                       |        | 12           | 13            |                       | 0.684 |
| 6 6 6 0.039 12 15 0.876 6 7 0.039 12 16 1.111 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 7 1 0.364 0.012 12 19 1.040 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 7 9 0.012 13 1 0.768 0.089 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 9 0.029 10 3 0.028 13 10 0.059 11 1 2.527 0.051 13 11 0.069 11 2 0.088 11 1 2.527 0.051 13 11 0.029 11 2 0.088 11 1 2.527 0.051 13 11 0.029 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2   |              |               |                       |        | 12           | 14            |                       | 0.804 |
| 6 7 0.039 12 16 1.111 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 1 12 19 1.040 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 7 8 0.036 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 1 0.062 11 1 2.527 0.051 13 13 10 0.090 11 1 0.0764 14 15 0.068 11 1 0.079 11 2 0.099 11 3 0.068 14 1 1 0.162 0.054 11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       | 0.876 |
| 6 8 0.026 12 17 0.985 6 9 0.064 12 18 0.930 17 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 13 2 0.148 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 10 3 0.028 13 10 0.059 11 1 2.527 0.051 13 11 0.029 11 2 0.099 11 1 2.527 0.051 13 11 0.029 11 2 0.099 11 2 0.064 14 1 0.062 0.088 11 1 1 2.527 0.051 13 11 0.029 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2  |              |               |                       |        |              |               |                       |       |
| 6 9 0.064 12 18 0.930 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 8 1 0.059 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 13 10 0.099 11 2 2.527 0.051 13 13 10 0.099 11 2 0.364 14 1 0.162 0.054 11 1 2 0.099 11 3 0.364 14 1 0.162 0.054 11 1 4 0.164 14 2 0.054  |              |               |                       |        |              |               |                       |       |
| 7       1       0.364       0.012       12       19       1.040         7       1       0.364       0.012       12       20       1.505         7       2       0.024       12       21       2.312         7       3       0.048       12       22       2.452         7       4       0.073       12       23       1.200         7       5       0.036       12       24       0.566         7       6       0.012       12       25       0.045         7       7       0.109       12       26       0.103         7       8       0.036       7       0.012       13       1       0.768       0.089         8       1       0.060       0.060       13       3       0.030       0.148         8       1       0.060       0.060       13       3       0.039         9       1       0.168       0.082       13       5       0.029         9       2       0.086       13       6       0.029         10       1       0.071       0.014       13       8       0.029   |              |               |                       |        |              |               |                       |       |
| 7 1 0.364 0.012 12 20 1.505 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 8 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 11 0.099 11 2.527 0.051 13 13 0.090 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2  | 0            | 7             |                       | 0.004  |              |               |                       |       |
| 7 2 0.024 12 21 2.312 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 3 0.028 13 10 0.029 10 4 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 10 0.029 11 1 2 0.099 11 2 0.099 11 2 0.064 14 1 0.162 0.088   | 7            | ,             | 0.264                 | 0.012  |              |               |                       |       |
| 7 3 0.048 12 22 2.452 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2 0.099 11 1 2.527 0.051 13 13 10 0.090 11 2 0.090 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054  |              |               | 0.304                 |        |              | -             |                       |       |
| 7 4 0.073 12 23 1.200 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 13 4 0.059 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 10 0.029 11 1 2 0.099 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       |       |
| 7 5 0.036 12 24 0.566 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 13 4 0.059 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 9 2 0.086 13 7 0.059 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 8 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 13 10 0.059 11 2 0.099 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2  |              |               |                       |        |              |               |                       |       |
| 7 6 0.012 12 25 0.045 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 13 4 0.059 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 8 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 12 0.088 11 1 2 0.099 11 2 0.364 14 1 0.162 0.054 11 3 0.364 14 1 0.162 0.054  |              |               |                       |        |              |               |                       |       |
| 7 7 7 0.109 12 26 0.103 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.059 10 2 0.014 13 9 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 12 0.088 11 1 2 0.099 11 2 0.064 14 1 0.162 0.054 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2  |              |               | •                     |        |              |               |                       |       |
| 7 8 0.036 7 9 0.012 13 1 0.768 0.089 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 12 0.088 11 1 2 0.099 11 2 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054  |              |               |                       |        |              |               |                       |       |
| 7 9 0.012 13 1 0.768 0.089 13 2 0.148 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 10 0.090 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054   |              |               |                       |        | 12           | 20            |                       | 0.103 |
| 8 1 0.060 0.060 13 3 0.030 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 12 0.088 11 1 2 0.099 11 2 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054   |              |               |                       |        |              |               | 0.760                 | 0.000 |
| 8       1       0.060       0.060       13       3       0.030         9       1       0.168       0.082       13       5       0.029         9       2       0.086       13       6       0.029         10       1       0.071       0.014       13       8       0.029         10       2       0.014       13       9       0.029         10       3       0.028       13       10       0.059         10       4       0.014       13       11       0.029         10       4       0.014       13       11       0.029         11       1       2.527       0.051       13       13       13       0.090         11       2       0.099       11       3       0.364       14       1       0.162       0.054         11       4       0.164       14       2       0.054   | 7            | 9             |                       | 0.012  |              |               | 0.700                 |       |
| 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 12 0.088 11 1 2 0.099 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       |       |
| 9 1 0.168 0.082 13 5 0.029 9 2 0.086 13 6 0.029 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.059 11 1 2.527 0.051 13 12 0.088 11 1 2 0.099 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054   | 8            | 1             | 0.060                 | 0.060  |              |               |                       |       |
| 9 2 0.086 13 6 0.029<br>13 7 0.059<br>10 1 0.071 0.014 13 8 0.029<br>10 2 0.014 13 9 0.029<br>10 3 0.028 13 10 0.059<br>10 4 0.014 13 11 0.029<br>11 1 2.527 0.051 13 13 0 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       |       |
| 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2.527 0.051 13 13 0 0.090 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054  | -            |               | 0.168                 |        |              |               |                       |       |
| 10 1 0.071 0.014 13 8 0.029 10 2 0.014 13 9 0.029 10 3 0.028 13 10 0.059 10 4 0.014 13 11 0.029 11 1 2 0.099 11 2 0.099 11 3 0.364 14 1 0.162 0.054 11 4 0.164 14 2 0.054  | 9            | 2             |                       | 0.086  |              |               |                       |       |
| 10 2 0.014 13 9 0.029<br>10 3 0.028 13 10 0.059<br>10 4 0.014 13 11 0.029<br>13 12 0.088<br>11 1 2.527 0.051 13 13 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       |       |
| 10 3 0.028 13 10 0.059<br>10 4 0.014 13 11 0.029<br>13 12 0.088<br>11 1 2.527 0.051 13 13 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054  | 10           |               | 0.071                 |        |              |               |                       |       |
| 10 4 0.014 13 11 0.029<br>13 12 0.088<br>11 1 2.527 0.051 13 13 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054  | 10           |               |                       |        |              |               |                       |       |
| 13 12 0.088<br>11 1 2.527 0.051 13 13 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054  | 10           |               |                       |        |              |               |                       |       |
| 11 1 2.527 0.051 13 13 0.090<br>11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   | 10           | 4             |                       | 0.014  |              |               |                       |       |
| 11 2 0.099<br>11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   |              |               |                       |        |              |               |                       |       |
| 11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   | 11           | 1             | 2.527                 | 0.051  | 13           | 13            |                       | 0.090 |
| 11 3 0.364 14 1 0.162 0.054<br>11 4 0.164 14 2 0.054   | 11           | 2             |                       | 0.099  |              |               |                       |       |
| 11 4 0.164 14 2 0.054  | 11           |               |                       | 0.364  | 14           |               | 0.162                 |       |
| 11 5 0.298 14 3 0.055  | 11           | 4             |                       | 0.164  |              | 2             |                       |       |
|  | 11           | 5             |                       | 0.298  | 14           | 3             |                       | 0.055 |



Table B.10. Percent VMT of Vehicle Classes on Urban Interstate (1985-86)

| Veh      | Sub-  | Vehicle   | -Mile %   | Veh   | Sub-  | Vehicle-  |           |
|----------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Class    | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
| 1        | 1     | 20.668    | 20.668    | 11    | 6     |           | 0.075     |
|          |       |           |           | 11    | 7     |           | 0.063     |
| 2        | 1     | 63.203    | 63.203    | 11    | 8     |           | 0.058     |
|          |       |           |           | 11    | 9     |           | 0.069     |
| 3        | 1     | 2.105     | 0.048     | 11    | 10    |           | 0.063     |
| 3        | 2     |           | 0.159     | 11    | 11    |           | 0.063     |
| 3        | 3     |           | 0.191     | 11    | 12    |           | 0.058     |
| 3        | 4     |           | 0.540     | 11    | 13    |           | 0.048     |
| 3        | 5     |           | 0.413     |       |       |           |           |
| 3        | 6     |           | 0.302     | 12    | 1     | 10.571    | 0.021     |
| 3        | 7     |           | 0.159     | 12    | 2     |           | 0.106     |
| 3        | 8     |           | 0.127     | 12    | 3     |           | 0.366     |
| 3        | 9     |           | 0.166     | 12    | 4     |           | 1.031     |
| ,        | ,     |           | 0.100     | 12    | 5     |           | 0.834     |
| 4        | 1     | 0.283     | 0.283     | 12    | 6     |           | 0.517     |
| 4        | 1     | 0.203     | 0.203     | 12    | 7     |           | 0.433     |
| -        | ,     | 0.050     | 0.050     | 12    | s s   |           | 0.380     |
| 5        | 1     | 0.859     | 0.859     |       | 9     |           | 0.348     |
|          |       |           | 0.040     | 12    |       |           | 0.348     |
| 6        | 1     | 0.368     | 0.043     | 12    | 10    |           |           |
| 6        | 2     |           | 0.022     | 12    | 11    |           | 0.310     |
| 6        | 3     |           | 0.033     | 12    | 12    |           | 0.299     |
| 6        | 4     |           | 0.065     | 12    | 13    |           | 0.262     |
| 6        | 5     |           | 0.057     | 12    | 14    |           | 0.309     |
| 6        | 6     |           | 0.034     | 12    | 15    |           | 0.336     |
| 6        | 7     |           | 0.034     | 12    | 16    |           | 0.426     |
| 6        | 8     |           | 0.023     | 12    | 17    |           | 0.378     |
| 6        | 9     |           | 0.057     | 12    | 18    |           | 0.357     |
|          |       |           |           | 12    | 19    |           | 0.399     |
| 7        | 1     | 0.264     | 0.009     | 12    | 20    |           | 0.577     |
| 7        | 2     |           | 0.018     | 12    | 21    |           | 0.887     |
| 7        | 3     |           | 0.035     | 12    | 22    |           | 0.941     |
| 7        | 4     |           | 0.053     | 12    | 23    |           | 0.460     |
| 7        | 5     |           | 0.026     | 12    | 24    |           | 0.217     |
| 7        | 6     |           | 0.009     | 12    | 25    |           | 0.017     |
| 7        | 7     |           | 0.079     | 12    | 26    |           | 0.040     |
| 7        | 8     |           | 0.026     |       |       |           |           |
| 7        | 9     |           | 0.009     | 13    | 1     | 0.406     | 0.047     |
| ,        | ,     |           | 0.007     | 13    | 2     |           | 0.078     |
| 8        | 1     | 0.300     | 0.300     | 13    | 3     |           | 0.016     |
| 0        |       | 0.500     | 0.500     | 13    | 4     |           | 0.031     |
| 9        | 1     | 0.070     | 0.034     | 13    | 5     |           | 0.016     |
| 9        | 2     | 0.070     | 0.036     | 13    | 6     |           | 0.016     |
| 7        | 2     |           | 0.000     | 13    | 7     |           | 0.031     |
| 10       | 1     | 0.030     | 0.006     | 13    | 8     |           | 0.016     |
| 10       | 1 2   | 0.030     | 0.006     | 13    | 9     |           | 0.016     |
| 10<br>10 | 3     |           | 0.006     | 13    | 10    |           | 0.031     |
| 10       | 4     |           | 0.006     | 13    | 11    |           | 0.016     |
| 10       | 4     |           | 0.000     | 13    | 12    |           | 0.046     |
| 1.1      | ,     | 0.011     | 0.016     | 13    | 13    |           | 0.047     |
| 11       | 1     | 0.811     | 0.016     | 13    | 13    |           | 0 10 11   |
| 11       | 2     |           | 0.032     | 14    | 1     | 0.061     | 0.015     |
| 11       | 3     |           | 0.117     | 14    | 2     | 0.001     | 0.023     |
| 11       | 4     |           | 0.053     | 14    | 3     |           | 0.023     |
| 11       | 5     |           | 0.096     | 14    | 2     |           | 0.023     |



Table B.11. Percent VMT of Vehicle Classes on State Primary Routes (1985-86)

| Veh    | Sub-   | Vehicle:  |                | Veh      | Sub-     | Vehicle-  |           |
|--------|--------|-----------|----------------|----------|----------|-----------|-----------|
| Class  | Group  | Veh Class | Sub-Group      | Class    | Group    | Veh Class | Sub-Group |
| 1      | 1      | 20.187    | 20.187         | 11       | 6        |           | 0.060     |
| _      |        |           |                | 11       | 7        |           | 0.007     |
| 2      | 1      | 68.556    | 68.556         | 11       | 8        |           | 0.008     |
| _      |        |           | 0 105          | 11       | 9        |           | 0.007     |
| 3      | 1      | 2.338     | 0.135          | 11       | 10       |           | 0.008     |
| 3      | 2      |           | 0.359          | 11<br>11 | 11       |           | 0.005     |
| 3      | 3      |           | 0.359<br>0.495 | 11       | 13       |           | 0.005     |
| 3      | 5      |           | 0.404          | 11       | 13       |           | 0.003     |
| 3      | 6      |           | 0.224          | 12       | 1        | 5.863     | 0.018     |
| 3      | 7      |           | 0.135          | 12       | 2        | 3.003     | 0.123     |
| 3      | 8      |           | 0.135          | 12       | 3        |           | 0.572     |
| 3      | 9      |           | 0.093          | 12       | 4        |           | 0.744     |
| ,      | ,      |           | 0.075          | 12       | 5        |           | 0.451     |
| 4      | I      | 0.088     | 0.088          | 12       | 6        |           | 0.275     |
| 7      | •      | 0.000     | 0.000          | 12       | 7        |           | 0.173     |
| 5      | 1      | 0.530     | 0.530          | 12       | 8        |           | 0.188     |
| -      | -      |           |                | 12       | 9        |           | 0.141     |
| 6      | 1      | 0.920     | 0.320          | 12       | 10       |           | 0.156     |
| 6      | 2      |           | 0.137          | 12       | 11       |           | 0.193     |
| 6      | 3      |           | 0.183 •        | 12       | 12       |           | 0.141     |
| 6      | 4      |           | 0.137          | 12       | 13       |           | 0.140     |
| 6      | 5      |           | 0.024          | 12       | 14       |           | 0.207     |
| 6      | 6      |           | 0.024          | 12       | 15       |           | 0.140     |
| 6      | 7      |           | 0.032          | 12       | 16       |           | 0.379     |
| 6      | 8      |           | 0.032          | 12       | 17       |           | 0.257     |
| 6      | 9      |           | 0.033          | 12       | 18       |           | 0.274     |
|        |        |           |                | 12       | 19       |           | 0.189     |
| 7      | 1      | 0.335     | 0.067          | 12       | 20       |           | 0.173     |
| 7      | 2      |           | 0.022          | 12       | 21       |           | 0.386     |
| 7      | 3      |           | 0.022          | 12       | 22       |           | 0.315     |
| 7      | 4      |           | 0.022          | 12       | 23<br>24 |           | 0.176     |
| 7<br>7 | 5<br>6 |           | 0.040          | 12<br>12 | 25       |           | 0.018     |
| 7      | 7      |           | 0.040<br>0.040 | 12       | 26       |           | 0.018     |
| 7      | 8      |           | 0.040          | 12       | 20       |           | 0.010     |
| 7      | 9      |           | 0.040          | 13       | 1        | 0.152     | 0.046     |
| ,      |        |           | 0.040          | 13       | 2        | 07132     | 0.030     |
| 8      | 1      | 0.210     | 0.210          | 13       | 3        |           | 0.023     |
| _      | •      | 0.210     | 0.00           | 13       | 4        |           | 0.015     |
| 9      | 1      | 0.192     | 0.026          | 13       | 5        |           | 0.008     |
| 9      | 2      |           | 0.166          | 13       | 6        |           | 0.008     |
| -      | _      |           |                | 13       | 7        |           | 0.008     |
| 10     | 1      | 0.041     | 0.010          | 13       | 8        |           | 0.003     |
| 10     | 2      |           | 0.010          | 13       | 9        |           | 0.003     |
| 10     | 3      |           | 0.010          | 13       | 10       |           | 0.003     |
| 10     | 4      |           | 0.010          | 13       | 11       |           | 0.003     |
|        |        |           |                | 13       | 12       |           | 0.002     |
| 11     | 1      | 0.477     | 0.030          | 13       | 13       |           | 0.002     |
| 11     | 2      |           | 0.074          |          |          |           | 0.007     |
| 11     | 3      |           | 0.119          | 14       | 1        | 0.112     | 0.037     |
| 11     | 4      |           | 0.090          | 14       | 2        |           | 0.037     |
| 11     | 5      |           | 0.060          | 14       | 3        |           | 0.038     |



Table B.12. Percent VMT of Vehicle Classes on State Secondary Routes (1985-86)

| Veh    | Sub-  | Vehicle     |           | Veh   | Sub-  | Vehicle   | -Mile %   |
|--------|-------|-------------|-----------|-------|-------|-----------|-----------|
| Class  | Group | Veh Class   | Sub-Group | Class | Group | Veh Class | Sub-Group |
| 1      | 1     | 20.208      | 20.208    | 11    | 6     |           | 0.085     |
|        |       |             |           | 11    | 7     |           |           |
| 2      | 1     | 71.778      | 71.778    | 11    | 8     |           | 0.021     |
|        |       |             |           | 11    | 9     |           | 0.011     |
| 3      | 1     | 3.212       | 0.881     | 11    | 10    |           | 0.011     |
| 3      | 2     | • • • • • • | 0.315     | 11    | 11    |           | 0.011     |
| 3      | 3     |             | 0.881     | 11    | 12    |           | 0.011     |
| 3      | 4     |             | 0.504     | 11    | 13    |           | 0.021     |
| 3      |       |             | 0.125     | • •   |       |           |           |
| 3      | 5     |             | 0.315     | 12    | 1     | 2.546     | 0.018     |
| 3      | 6     |             |           | 12    | 2     | 2.5.0     | 0.036     |
| 3      | 7     |             | 0.125     | 12    | 3     |           | 0.106     |
| 3      | 8     |             | 0.032     |       | 4     |           | 0.478     |
| 3      | 9     |             | 0.034     | 12    |       |           | 0.106     |
|        |       |             |           | 12    | 5     |           |           |
| 4      | 1     | 0.059       | 0.059     | 12    | 6     |           | 0.193     |
|        |       |             |           | 12    | 7     |           | 0.018     |
| 5      | 1     | 0.490       | 0.490     | 12    | 8     |           | 0.071     |
|        |       |             |           | 12    | 9     |           | 0.159     |
| 6      | I     | 0.511       | 0.177     | 12    | 10    |           | 0.142     |
| 6      | 2     |             | 0.126     | 12    | 11    |           | 0.036     |
| 6      | 3     |             | 0.051     | 12    | 12    |           | 0.053     |
| 6      | 4     |             | 0.051     | 12    | 13    |           | 0.071     |
| 6      | 5     |             | 0.013     | 12    | 14    |           | 0.053     |
| 6      | 6     |             | 0.013     | 12    | 15    |           | 0.053     |
| 6      | 7     |             | 0.013     | 12    | 16    |           | 0.035     |
|        |       |             | 0.013     | 12    | 17    |           | 0.053     |
| 6      | В     |             |           | 12    | 18    |           | 0.192     |
| 6      | 9     |             | 0.053     | 12    | 19    |           | 0.088     |
| _      |       | 0.07/       | 0.03/     | 12    | 20    |           | 0.157     |
| 7      | 1     | 0.274       | 0.034     | 12    | 21    |           | 0.196     |
| 7      | 2     |             | 0.034     |       |       |           | 0.107     |
| 7      | 3     |             | 0.034     | 12    | 22    |           | 0.108     |
| 7      | 4     |             | 0.034     | 12    | 23    |           | 0.013     |
| 7<br>7 | 5     |             | 0.027     | 12    | 24    |           | 0.003     |
| 7      | 6     |             | 0.027     | 12    | 25    |           |           |
| 7      | 7     |             | 0.027     | 12    | 26    |           | 0.003     |
| 7      | 8     |             | 0.027     |       |       |           |           |
| 7      | 9     |             | 0.027     | 13    | I     | 0.091     | 0.027     |
|        |       |             |           | 13    | 2     |           | 0.027     |
| 8      | 1     | 0.210       | 0.210     | 13    | 3     |           | 0.018     |
|        |       |             |           | 13    | 4     |           | 0.009     |
| 9      | 1     | 0.031       | 0.        | 13    | 5     |           | 0.009     |
| ģ      | 2     |             | 0.031     | 13    | 6     |           | 0.        |
| ,      | -     |             | 0,000     | 13    | 7     |           | 0.        |
| 10     | 1     | 0.061       | 0.015     | 13    | 8     |           | 0.        |
| 10     | 2     | 0.001       | 0.015     | 13    | 9     |           | 0.        |
| 10     | 3     |             | 0.015     | 13    | 10    |           | 0.        |
|        | 4     |             | 0.015     | 13    | 11    |           | 0.        |
| 10     | 4     |             | 0.013     | 13    | 12    |           | 0.        |
|        |       | 0.468       | 0.064     | 13    | 13    |           | 0.        |
| 11     | 1     | 0.408       | 0.064     | 13    |       |           |           |
| 11     | 2     |             |           | 14    | 1     | 0.061     | 0.020     |
| 11     | 3     |             | 0.085     | 14    | 2     | 0.001     | 0.020     |
| 11     | 4     |             | 0.043     | 14    | 3     |           | 0.021     |
| 11     | 5     |             | 0.022     | 14    | 3     |           | 0.024     |



Table B.13. Percent VMT of Vehicle Classes on County Roads (1985-86)

| 17 - 1- | C     | Vehicle-       | M(1a 7    | Veh   | Sub-  | Vehicle-  | -Mile Z   |
|---------|-------|----------------|-----------|-------|-------|-----------|-----------|
| Veh     | Sub-  | Veh Class      | Sub-Group | Class | Group | Veh Class | Sub-Group |
| Class   | Group | ven Class      | 3ub-Stoup | 0200  |       |           |           |
| 1       | 1     | 17.968         | 17.968    | 11    | 6     |           | 0.050     |
| •       | •     | 2              |           | 11    | 7     |           | 0.012     |
|         | ,     | 75.415         | 75.415    | 11    | 8     |           | 0.012     |
| 2       | i     | /5.413         | /3.413    | 11    | 9     |           | 0.006     |
|         |       |                |           |       |       |           | 0.006     |
| 3       | 1     | 3.7 <b>9</b> 9 | 1.042     | 11    | 10    |           |           |
| 3       | 2     |                | 0.372     | 11    | 11    |           | 0.006     |
| 3       | 3     |                | 1.042     | 11    | 12    |           | 0.006     |
| 3       | 4     |                | 0.596     | 11    | 13    |           | 0.012     |
| 3       | 5     |                | 0.148     |       |       |           |           |
| 3       | 6     |                | 0.372     | 12    | I     | 0.642     | 0.004     |
| 3       |       |                | 0.148     | 12    | 2     |           | 0.009     |
| 3       | 7     |                |           | 12    | 3     |           | 0.027     |
| 3       | 8     |                | 0.038     | 12    | 4     |           | 0.120     |
| 3       | 9     |                | 0.040     |       | 5     |           | 0.027     |
|         |       |                |           | 12    |       |           | 0.049     |
| 4       | 1     | 0.049          | 0.049     | 12    | 6     |           |           |
|         |       |                |           | 12    | 7     |           | 0.004     |
| 5       | 1     | 0.631          | 0.631     | 12    | 8     |           | 0.018     |
| ,       | -     |                |           | 12    | 9     |           | 0.040     |
| ,       | 1     | 0.845          | 0.293     | 12    | 10    |           | 0.036     |
| 6       |       | 0.043          | 0.209     | 12    | 11    |           | 0.009     |
| 6       | 2     |                |           | 12    | 12    |           | 0.013     |
| 6       | 3     |                | 0.084     | 12    | 13    |           | 0.018     |
| 6       | 4     |                | 0.084     |       |       |           | 0.013     |
| 6       | 5     |                | 0.022     | 12    | 14    |           |           |
| 6       | 6     |                | 0.022     | 12    | 15    |           | 0.013     |
| 6       | 7     |                | 0.022     | 12    | 16    |           | 0.009     |
| 6       | 8     |                | 0.022     | 12    | 17    |           | 0.013     |
|         | 9     |                | 0.088     | 12    | 18    |           | 0.048     |
| 6       | 9     |                | 0.000     | 12    | 19    |           | 0.022     |
| _       |       |                | 0.000     | 12    | 20    |           | 0.040     |
| 7       | 1     | 0.051          | 0.006     |       |       |           | 0.049     |
| 7       | 2     |                | 0.006     | 12    | 21    |           | 0.027     |
| 7       | 3     |                | 0.006     | 12    | 22    |           |           |
| 7       | 4     |                | 0.006     | 12    | 23    |           | 0.027     |
| 7       | 5     |                | 0.005     | 12    | 24    |           | 0.003     |
| 7       | 6     |                | 0.005     | 12    | 25    |           | 0.001     |
| 7       | 7     |                | 0.005     | 12    | 26    |           | 0.001     |
| 7       | 8     |                | 0.005     |       |       |           |           |
|         |       |                | 0.005     | 13    | 1     | 0.183     | 0.055     |
| 7       | 9     |                | 0.003     | 13    | 2     |           | 0.055     |
|         |       |                |           | 13.   | 3     |           | 0.037     |
| 8       | 1     | 0.             | 0.        |       | 4     |           | 0.018     |
|         |       |                |           | 13    |       |           | 0.018     |
| 9       | 1     | 0.051          | 0.        | 13    | 5     |           |           |
| 9       | 2     |                | 0.051     | 13    | 6     |           | 0.        |
| -       |       |                |           | 13    | 7     |           | 0.        |
| 10      | 1     | 0.             | 0.        | 13    | 8     |           | 0.        |
|         | 2     | •              | 0.        | 13    | 9     |           | 0.        |
| 10      |       |                | 0.        | 13    | 10    |           | 0.        |
| 10      | 3     |                |           | 13    | 11    |           | 0.        |
| 10      | 4     |                | 0.        |       | 12    |           | 0.        |
|         |       |                |           | 13    |       |           | 0.        |
| 11      | 1     | 0.275          | 0.037     | 13    | 13    |           | 0.        |
| 11      | 2     |                | 0.037     |       |       |           | 0.021     |
| 11      | 3     |                | 0.050     | 14    | 1     | 0.092     | 0.031     |
| 11      | 4     |                | 0.025     | 14    | 2     |           | -0.030    |
| 11      | 5     |                | 0.013     | 14    | 3     |           | 0.031     |
| 1.1     | ,     |                | 0.013     |       |       |           |           |



Table B.14. Percent VMT of Vehicle Classes on City Streets (1985-86)

| , | Veh   | Sub-  | Vehicle-  | -M1le %   | Veh | Sub- | Vehicle-  | -H11e % |
|---|-------|-------|-----------|-----------|-----|------|-----------|---------|
|   |       |       | Veh Class |           |     |      | Veh Class |         |
| , | 31030 | осоор |           |           |     |      |           |         |
|   | 1     | 1     | 19.344    | 19.344    | 11  | 6    |           | 0.080   |
|   |       |       |           |           | 11  | 7    |           | 0.020   |
|   | 2     | 1     | 74.013    | 74.013    | 11  | 8    |           | 0.020   |
|   | -     | -     | 74.013    | 14013     | 11  | 9    |           | 0.010   |
|   | 2     | ,     | 2 102     | 0 577     | 11  | 10   |           | 0.010   |
|   | 3     | 1     | 2.102     | 0.577     |     | 11   |           | 0.010   |
|   | 3     | 2     |           | 0.206     | 11  |      |           |         |
|   | 3     | 3     |           | 0.577     | 11  | 12   |           | 0.010   |
|   | 3     | 4     |           | 0.330     | 11  | 13   |           | 0.020   |
|   | 3     | 5     |           | 0.082     |     |      |           |         |
|   | 3     | 6     |           | 0.206     | 12  | I    | 2.403     | 0.017   |
|   | 3     | 7     |           | 0.082     | 12  | 2    |           | 0.034   |
|   | 3     | 8     |           | 0.021     | 12  | 3    |           | 0.100   |
|   | 3     | 9     |           | 0.022     | 12  | 4    |           | 0.451   |
|   | 3     | 9     |           | 0.022     | 12  | 5    |           | 0.100   |
|   |       |       |           |           |     | 6    |           | 0.182   |
|   | 4     | 1     | 0.225     | 0.225     | 12  |      |           |         |
|   |       |       |           |           | 12  | 7    |           | 0.017   |
|   | 5     | 1     | 0.480     | 0.480     | 12  | 8    |           | 0.067   |
|   |       |       |           |           | 12  | 9    |           | 0.150   |
|   | 6     | 1     | 0.707     | 0.245     | 12  | 10   |           | 0.134   |
|   | 6     | 2     |           | 0.175     | 12  | 11   |           | 0.034   |
|   | 6     | 3     |           | 0.070     | 12  | 12   |           | 0.050   |
|   |       |       |           | 0.070     | 12  | 13   |           | 0.067   |
|   | 6     | 4     |           |           | 12  | 14   |           | 0.050   |
|   | 6     | 5     |           | 0.018     |     |      |           |         |
|   | 6     | 6     |           | 0.018     | 12  | 15   |           | 0.050   |
|   | 6     | 7     |           | 0.018     | 12  | 16   |           | 0.033   |
|   | 6     | 8     |           | 0.018     | 12  | 17   |           | 0.050   |
|   | 6     | 9     |           | 0.073     | 12  | 18   |           | 0.181   |
|   | •     | -     |           | • • • • • | 12  | 19   |           | 0.083   |
|   | 7     | 1     | 0.061     | 0.008     | 12  | 20   |           | 0.148   |
|   |       |       | 0.001     |           | 12  | 21   |           | 0.185   |
|   | 7     | 2     |           | 0.008     |     |      |           | 0.101   |
|   | 7     | 3     |           | 0.008     | 12  | 22   |           |         |
|   | 7     | 4     |           | 0.008     | 12  | 23   |           | 0.101   |
|   | 7     | 5     |           | 0.006     | 12  | 24   |           | 0.012   |
|   | 7     | 6     |           | 0.006     | 12  | 25   |           | 0.002   |
|   | 7     | 7     |           | 0.006     | 12  | 26   |           | 0.002   |
|   | 7     | В     |           | 0.006     |     |      |           |         |
|   | 7     | 9     |           | 0.006     | 13  | 1    | 0.099     | 0.030   |
|   | •     | -     |           | ••••      | 13  | 2    |           | 0.030   |
|   | n     | 1     | 0         | 0         | 13  | 3    |           | 0.020   |
|   | 8     | 1     | 0.        | 0.        | 13  | 4    |           | 0.010   |
|   |       |       |           | _         |     |      |           | 0.010   |
|   | 9     | 1     | 0.051     | 0.        | 13  | 5    |           |         |
|   | 9     | 2     |           | 0.051     | 13  | 6    |           | 0.      |
|   |       |       |           |           | 13  | 7    |           | 0.      |
|   | 10    | 1     | 0.046     | 0.011     | 13  | 8    |           | 0.      |
|   | 10    | 2     |           | 0.011     | 13  | 9    |           | 0.      |
|   | 10    | 3     |           | 0.011     | 13  | 10   |           | 0.      |
|   | 10    | 4     |           | 0.011     | 13  | 11   |           | 0.      |
|   | 10    | 4     |           | 0.011     | 13  | 12   |           | 0.      |
|   | 1.7   |       | 0 / 37    | 0.050     | 13  | 13   |           | 0.      |
|   | 11    | 1     | 0.437     | 0.059     | 1.3 | 13   |           |         |
|   | 11    | 2     |           | 0.059     | 1.1 | ,    | 0.033     | 0.011   |
|   | 11    | 3     |           | 0.080     | 14  | 1    | 0.033     | 0.011   |
|   | 11    | 4     |           | 0.040     | 14  | 2    |           | 0.011   |
|   | 11    | 5     |           | 0.020     | 14  | 3    |           | 0.011   |
|   |       |       |           |           |     |      |           |         |



Table B.15 VMT Values by Highway Functional Class

|                          |                | Average        |
|--------------------------|----------------|----------------|
| Highway Functional Class | 1983 VMT       | 1985-86 VMT    |
|                          |                |                |
| Interstate Rural         | 4,403,050,390  | 4,548,825,803  |
| Interstate Urban         | 3,648,196,397  | 3,756,549,624  |
| State Routes Primary     | 7,895,474,051  | 8,120,381,844  |
| State Routes Secondary   | 5,406,210,594  | 5,556,036,215  |
| County Roads             | 6,038,969,997  | 6,202,652,957  |
| City Streets             | 11,354,525,755 | 11,671,149,284 |
|                          |                |                |
| Total                    | 38,746,427,184 | 39,855,595,727 |
|                          |                |                |



Table B.16 Indiana Bureau of Motor Vehicles Registered Vehicle
Classification

## (A) Single-Unit Trucks

| Group | Registered Gross Weight (1bs) |
|-------|-------------------------------|
| 1     | 0-6999                        |
| 2     | 7000-8999                     |
| 3     | 9000-10999                    |
| 4     | 11000-15999                   |
| 5     | 16000-19999                   |
| 6     | 20000-25999                   |
| 7     | 26000-29999                   |
| 8     | 30000-35999                   |
| 9     | 36000-41999                   |
| 10    | 42000-47999                   |
| 11    | 48000-53999                   |
| 12    | 54000-59999                   |
| 13    | 60000-65999                   |
| 14    | 66000-99999                   |
|       |                               |

## (B) Combination Trucks

| Group | Registered Gross Weight (1bs) |
|-------|-------------------------------|
| 1     | 0-19999                       |
| 2     | 20000-25999                   |
| 3     | 26000-29999                   |
| 4     | 30000-35999                   |
| 5     | 36000-41999                   |
| 6     | 42000-47999                   |
| 7     | 48000-53999                   |
| 8     | 54000-59999                   |
| 9     | 60000-65999                   |
| . 10  | 66000-71999                   |
| 11    | 72000-73999                   |
| 12    | 74000-75999                   |
| 13    | 76000-77999                   |
| 14    | 78000-99999                   |



Table B.17 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Single-Unit Trucks Class 3

| Registration | Operating Weight Group Percentages |    |    |    |    |    |    |    |    |  |  |
|--------------|------------------------------------|----|----|----|----|----|----|----|----|--|--|
| Weight (1bs) | 1                                  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9  |  |  |
|              |                                    |    |    |    |    |    |    |    |    |  |  |
|              |                                    |    |    |    |    |    |    |    |    |  |  |
| 0-6999       | 72                                 | 20 | 8  |    |    |    |    |    |    |  |  |
| 7000-8999    | 67                                 | 28 | 4  | 1  |    |    |    |    |    |  |  |
| 9000-10999   | 39                                 | 33 | 20 | 6  | 2  |    |    |    |    |  |  |
| 11000-15999  | 20                                 | 40 | 20 | 10 | 9  | 1  |    |    |    |  |  |
| 16000-19999  | 15                                 | 29 | 10 | 7  | 7  | 4  | 3  |    |    |  |  |
| 20000-25999  | 6                                  | 10 | 16 | 22 | 18 | 13 | 7  | 4  | 4  |  |  |
| 26000-29999  |                                    | 6  | 11 | 23 | 27 | 18 | 7  | 5  | 3  |  |  |
| 30000-35999  |                                    | 9  | 9  | 23 | 23 | 11 | 7  | 7  | 11 |  |  |
| 36000-41999  |                                    |    | 13 | 16 | 20 | 13 | 13 | 7  | 18 |  |  |
| 42000-47999  |                                    |    | 6  | 10 | 16 | 20 | 10 | 16 | 22 |  |  |
| 48000-53999  |                                    |    | 5  | 10 | 15 | 25 | 10 | 15 | 20 |  |  |
| 54000-59999  |                                    |    |    | 2  | 5  | 20 | 28 | 15 | 30 |  |  |
| 60000-65999  |                                    |    |    | 3  | 5  | 20 | 27 | 15 | 30 |  |  |
| 66000-99999  |                                    |    |    | 3  | 5  | 20 | 27 | 15 | 30 |  |  |
|              | 1                                  |    |    |    |    |    | 1  |    | 1  |  |  |



Table B.18 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Single-Unit Trucks Class 6

| Registration | Operating Weight Group Percentages |    |    |    |    |    |     |    |    |  |
|--------------|------------------------------------|----|----|----|----|----|-----|----|----|--|
| Weight (1bs) | 1                                  | 2  | 3  | 4  | 5  | 6  | 7 ( | 8  | 9  |  |
|              |                                    |    |    |    |    |    |     |    |    |  |
|              |                                    |    |    |    |    |    |     |    |    |  |
| 0-6999       | 100                                |    |    |    |    |    |     |    |    |  |
| 7000-8999    | 100                                |    |    |    |    |    |     |    |    |  |
| 9000-10999   | 90                                 | 10 |    |    |    |    |     |    |    |  |
| 11000-15999  | 75                                 | 20 | 5  |    |    |    |     |    |    |  |
| 16000-19999  | 60                                 | 25 | 13 | 2  |    |    |     |    |    |  |
| 20000-25999  | 50                                 | 10 | 20 | 10 | 6  | 4  |     |    |    |  |
| 26000-29999  | 35                                 | 5  | 10 | 11 | 15 | 15 | 7   | 2  |    |  |
| 30000-35999  | 20                                 | 6  | 8  | 10 | 6  | 15 | 15  | 12 | В  |  |
| 36000-41999  | 10                                 | 6  | 8  | 8  | 10 | 12 | 17  | 17 | 12 |  |
| 42000-47999  |                                    | 7  | 7  | 10 | 12 | 13 | 18  | 18 | 15 |  |
| 48000-53999  |                                    | 7  | 8  | 10 | 15 | 14 | 14  | 14 | 18 |  |
| 54000-59999  |                                    |    | 10 | 10 | 15 | 15 | 15  | 15 | 20 |  |
| 60000-65999  |                                    |    | 8  | 10 | 12 | 15 | 15  | 15 | 25 |  |
| 66000-99999  |                                    |    |    | 5  | 15 | 15 | 20  | 20 | 25 |  |
|              |                                    |    |    | 1  |    |    |     |    | 1  |  |



Table B.19 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 7

| Registration |    | Operating Weight Group Percentages |     |    |    |    |    |    |    |  |  |  |  |
|--------------|----|------------------------------------|-----|----|----|----|----|----|----|--|--|--|--|
| Weight (lbs) | 1  | 2                                  | 3   | 4  | 5  | 6  | 7  | 8  | 9  |  |  |  |  |
|              |    |                                    |     |    |    |    |    |    |    |  |  |  |  |
|              | 50 | 15                                 | 1.5 | 10 | 5  | -  |    |    |    |  |  |  |  |
| 0-19999      | 50 | 15                                 | 15  | 10 | )  | 5  |    |    |    |  |  |  |  |
| 20000-25999  | 30 | 10                                 | 15  | 10 | 10 | 10 | 10 | 5  |    |  |  |  |  |
| 26000-29999  | 25 | 5                                  | 10  | 12 | 10 | 10 | 18 | 7  | 3  |  |  |  |  |
| 30000-35999  | 20 | 5                                  | 6   | 9  | 14 | 14 | 14 | 10 | 8  |  |  |  |  |
| 36000-41999  | 15 | 5                                  | 7   | 11 | 11 | 11 | 18 | 12 | 10 |  |  |  |  |
| 42000-47999  | 10 | 4                                  | 8   | 11 | 12 | 12 | 19 | 12 | 12 |  |  |  |  |
| 48000-53999  | 6  | 5                                  | 8   | 10 | 10 | 14 | 20 | 12 | 15 |  |  |  |  |
| 54000-59999  | 6  | 5                                  | 9   | 9  | 12 | 12 | 18 | 13 | 16 |  |  |  |  |
| 60000-65999  | 4  | 5                                  | 9   | 10 | 8  | 8  | 20 | 16 | 20 |  |  |  |  |
| 66000-71999  |    | 5                                  | 7   | 9  | 8  | 8  | 21 | 22 | 20 |  |  |  |  |
| 72000-73999  |    | 4                                  | 8   | 8  | 10 | 13 | 15 | 22 | 20 |  |  |  |  |
| 74000-75999  |    | 2                                  | 3   | 5  | 7  | 11 | 17 | 25 | 30 |  |  |  |  |
| 76000-77999  |    | 2                                  | 2   | 4  | 8  | 11 | 18 | 20 | 35 |  |  |  |  |
| 78000-99999  |    |                                    | 1   | 3  | 3  | 3  | 15 | 30 | 45 |  |  |  |  |
|              |    |                                    | 1   |    |    |    |    |    |    |  |  |  |  |



Table B.20 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Single-Unit Trucks Class 9

| Registration | Оре | eratio | ng We | e <b>i</b> gh: | Gro | oup 1 | Perce | entages |
|--------------|-----|--------|-------|----------------|-----|-------|-------|---------|
| Weight (lbs) | 1   | 2      | 3     | 4              | 5   | 6     | 7     | 8       |
|              |     |        |       |                |     |       |       |         |
|              |     |        |       |                |     |       |       |         |
| 0-6999       | 100 |        |       |                |     |       |       |         |
| 7000-8999    | 100 |        |       |                |     |       |       |         |
| 9000-10999   | 100 |        |       |                |     |       |       |         |
| 11000-15999  | 100 |        |       |                |     |       |       |         |
| 16000-19999  | 80  | 20     |       |                |     |       |       |         |
| 20000-25999  | 60  | 40     |       |                |     |       |       |         |
| 26000-29999  | 40  | 60     |       |                |     |       |       |         |
| 30000-35999  | 30  | 70     |       |                |     |       |       |         |
| 36000-41999  | 20  | 80     |       |                |     |       |       |         |
| 42000-47999  | 10  | 90     |       |                |     |       |       |         |
| 48000-53999  | 5   | 95     |       |                |     |       |       |         |
| 54000-59999  | 5   | 95     |       |                |     |       |       |         |
| 60000-65999  |     | 100    |       |                |     |       |       |         |
| 66000-99999  |     | 100    |       |                |     |       |       |         |
|              |     |        | 1     |                |     | 1     |       | 1       |



Table B.21 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 10

| Registration | Operating Weight Group Percentages |    |    |    |   |   |   |   |   |  |  |  |
|--------------|------------------------------------|----|----|----|---|---|---|---|---|--|--|--|
| Weight (1bs) | 1 [                                | 2  | 3  | 4  | 5 | 6 | 7 | 8 | 9 |  |  |  |
|              |                                    |    |    |    |   |   |   |   |   |  |  |  |
|              |                                    |    |    |    |   |   |   |   |   |  |  |  |
| 0-19999      | 100                                |    |    |    |   |   |   |   |   |  |  |  |
| 20000-25999  | 90                                 | 10 |    |    |   |   |   |   |   |  |  |  |
| 26000-29999  | 60                                 | 35 | 5  |    |   |   |   |   |   |  |  |  |
| 30000-35999  | 35                                 | 25 | 25 | 15 |   |   |   |   |   |  |  |  |
| 36000-41999  | 15                                 | 25 | 25 | 35 |   |   |   |   |   |  |  |  |
| 42000-47999  | 10                                 | 20 | 25 | 45 |   |   |   |   |   |  |  |  |
| 48000-53999  | 10                                 | 10 | 30 | 50 |   |   |   |   |   |  |  |  |
| 54000-59999  | 5                                  | 15 | 30 | 50 |   |   |   |   |   |  |  |  |
| 60000-65999  | 4                                  | 14 | 27 | 55 |   |   |   |   |   |  |  |  |
| 66000-71999  | 2                                  | 8  | 30 | 60 |   |   |   |   |   |  |  |  |
| 72000-73999  | 2                                  | 8  | 30 | 60 |   |   |   |   |   |  |  |  |
| 74000-75999  | 2                                  | 3  | 25 | 70 |   |   |   |   |   |  |  |  |
| 76000-77999  | 2                                  | 3  | 25 | 70 |   |   |   |   |   |  |  |  |
| 78000-99999  | 2                                  | 3  | 25 | 70 |   |   |   |   |   |  |  |  |
|              | 1                                  |    |    |    | I | 1 | 1 | 1 | 1 |  |  |  |



Table B.22 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 11

| Registration | Operating Weight Group Percentages |    |    |    |    |    |    |    |     |    |    |    |    |
|--------------|------------------------------------|----|----|----|----|----|----|----|-----|----|----|----|----|
| Weight (1bs) | 1                                  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9 ( | 10 | 11 | 12 | 13 |
|              |                                    |    |    |    |    |    |    |    |     |    |    |    | -  |
|              |                                    |    |    |    |    |    |    |    |     |    |    |    |    |
| 0-19999      | 90                                 | 8  | 2  |    |    |    |    |    | l   |    |    |    |    |
| 20000-25999  | 60                                 | 20 | 15 | 5  |    |    |    |    |     |    |    |    |    |
| 26000-29999  | 30                                 | 20 | 20 | 15 | 10 | 5  |    |    |     |    |    |    |    |
| 30000-35999  | 10                                 | 10 | 15 | 20 | 17 | 15 | 10 | 3  |     |    |    |    |    |
| 36000-41999  | 3                                  | 6  | 9  | 12 | 15 | 15 | 15 | 11 | 8   | 6  |    |    |    |
| 42000-47999  |                                    | 4  | 5  | 7  | 8  | 9  | 12 | 15 | 10  | 10 | 10 | 7  | 3  |
| 48000-53999  |                                    | 1  | 3  | 4  | 8  | 8  | 9  | 10 | 10  | 12 | 15 | 13 | 7  |
| 54000-59999  |                                    | 1  | 2  | 5  | 6  | 7  | 9  | 10 | 13  | 11 | 11 | 11 | 14 |
| 60000-65999  |                                    |    | 3  | 4  | 7  | 9  | 10 | 10 | 10  | 10 | 10 | 12 | 15 |
| 66000-71999  |                                    |    | 2  | 4  | 8  | 8  | 8  | 8  | 9   | 10 | 11 | 15 | 17 |
| 72000-73999  |                                    |    | 2  | 4  | 7  | 8  | 8  | 8  | 8   | 10 | 12 | 15 | 18 |
| 74000-75999  |                                    |    | 2  | 4  | 7  | 8  | 8  | 8  | 8   | 10 | 12 | 15 | 18 |
| 76000-77999  |                                    |    |    | 5  | 5  | 7  | 7  | 7  | 10  | 11 | 12 | 16 | 20 |
| 78000-99999  |                                    |    |    | 5  | 5  | 7  | 7  | 7  | 10  | 11 | 12 | 16 | 20 |
|              |                                    |    |    |    |    |    | 1  |    | 1   | 1  | 1  |    |    |



Table B.23 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 12

| Registration | Operating Weight Group Percentages |            |    |    |    |    |    |    |    |    |    |    |    |
|--------------|------------------------------------|------------|----|----|----|----|----|----|----|----|----|----|----|
| Weight (1bs) | 1                                  | 2          | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 | 11 | 12 | 13 |
|              |                                    |            |    |    |    |    |    |    |    |    |    |    |    |
|              |                                    |            |    |    |    |    |    |    |    |    |    |    |    |
| 0-19999      | 70                                 | 18         | 7  | 5  |    |    |    |    |    |    |    |    |    |
| 20000-25999  | 45                                 | <b>3</b> 0 | 20 | 5  |    |    |    |    |    |    |    |    |    |
| 26000-29999  | 25                                 | 20         | 20 | 15 | 10 | 5  | 5  |    |    |    |    |    |    |
| 30000-35999  | 10                                 | 10         | 15 | 20 | 17 | 15 | 10 | 3  |    |    |    |    |    |
| 36000-41999  | 3                                  | 6          | 9  | 12 | 15 | 15 | 15 | 11 | 8  | 6  |    |    |    |
| 42000-47999  |                                    | 4          | 5  | 7  | 8  | 9  | 12 | 15 | 10 | 10 | 10 | 7  | 3  |
| 48000-53999  |                                    | 1          | 3  | 4  | 5  | 5  | 8  | 10 | 10 | 12 | 10 | 10 | 8  |
| 54000-59999  |                                    | 1          | 2  | 2  | 3  | 5  | 6  | 6  | 6  | 8  | 8  | 8  | 10 |
| 60000-65999  |                                    |            | 2  | 2  | 3  | 4  | 4  | 5  | 5  | 5  | 5  | 7  | 7  |
| 66000-71999  |                                    | Į.         |    | 2  | 3  | 3  | 3  | 4  | 4  | 4  | 5  | 5  | 5  |
| 72000-73999  |                                    |            |    | 2  | 2  | 3  | 3  | 3  | 4  | 4  | 4  | 5  | 5  |
| 74000-75999  |                                    |            |    | 1  | 1  | 2  | 3  | 3  | 3  | 4  | 4  | 4  | 5  |
| 76000-77999  |                                    |            |    | 1  | 1  | 2  | 3  | 3  | 3  | 4  | 4  | 4  | 5  |
| 78000-99999  |                                    |            |    | 1  | 1  | 2  | 3  | 3  | 3  | 4  | 4  | 4  | 5  |
|              | 1                                  |            |    |    |    |    |    |    | -  | Į. |    | 1  | İ  |



Table B.23 (Continued)

| Registration | Operating Weight Group Percentages |    |    |    |    |    |    |    |    |    |    |    |    |
|--------------|------------------------------------|----|----|----|----|----|----|----|----|----|----|----|----|
| Weight (1bs) | 14                                 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
|              | <b></b>                            |    |    |    |    |    |    |    |    |    |    |    |    |
|              |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 0-19999      |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 20000-25999  |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 26000-29999  |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 30000-35999  |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 36000-41999  |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 42000-47999  |                                    |    |    |    |    |    |    |    |    |    |    |    |    |
| 48000-53999  | 7                                  | 4  | 3  |    |    |    |    |    |    |    |    |    |    |
| 54000-59999  | 10                                 | 8  | 8  | 6  | 3  |    |    |    |    |    |    |    |    |
| 60000-65999  | 7                                  | 9  | 9  | 8  | 6  | 6  | 4  | 2  |    |    |    |    |    |
| 66000-71999  | 6                                  | 6  | 8  | 8  | 8  | 8  | 7  | 5  | 4  | 2  |    |    |    |
| 72000-73999  | 5                                  | 6  | 6  | 8  | 8  | 8  | 8  | 6  | 4  | 4  | 2  |    |    |
| 74000-75999  | 5                                  | 5  | 6  | 6  | 7  | 8  | 8  | 8  | 6  | 4  | 4  | 2  | 1  |
| 76000-77999  | 5                                  | 5  | 6  | 6  | 7  | 8  | 8  | 8  | 6  | 4  | 4  | 2  | 1  |
| 78000-99999  | 5                                  | 5  | 6  | 6  | 7  | 8  | 8  | 8  | 6  | 4  | 4  | 2  | 1  |



Table B.24 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 13

| Registration | Operating Weight Group Percentages |    |    |    |     |    |   |   |    |    |    |    |    |
|--------------|------------------------------------|----|----|----|-----|----|---|---|----|----|----|----|----|
| Weight (1bs) | 1                                  | 2  | 3  | 4  | 5   | 6  | 7 | 8 | 9  | 10 | 11 | 12 | 13 |
|              |                                    |    |    |    |     |    |   |   |    |    |    |    |    |
|              | 100                                | :  |    |    |     |    |   |   |    |    |    |    |    |
| 0-19999      | 100                                |    |    |    |     |    |   |   |    |    |    |    |    |
| 20000-25999  | 100                                |    |    |    |     |    |   |   |    |    |    |    |    |
| 26000-29999  | 100                                |    |    |    |     |    |   |   |    |    |    |    |    |
| 30000-35999  | 100                                |    |    |    |     |    |   |   |    |    |    |    |    |
| 36000-41999  | 85                                 | 10 | 5  |    |     |    |   |   |    |    |    |    |    |
| 42000-47999  | 65                                 | 13 | 12 | 7  | 3   |    |   |   |    |    |    | :  |    |
| 48000-53999  | 45                                 | 12 | 10 | 10 | 8   | 7  | 5 | 3 |    |    |    |    |    |
| 54000-59999  | 30                                 | 8  | 8  | 8  | 10  | 10 | 8 | 8 | 6  | 4  |    |    |    |
| 60000-65999  | 25                                 | 5  | 5  | 5  | 7   | 7  | 7 | 9 | 9  | 8  | 6  | 4  | 3  |
| 66000-71999  | 20                                 | 4  | 4  | 5  | - 5 | 7  | 8 | 9 | 10 | 10 | 8  | 6  | 4  |
| 72000-73999  | 20                                 | 3  | 4  | 5  | 5   | 7  | 8 | 9 | 10 | 10 | 8  | 6  | 5  |
| 74000-75999  | 20                                 | 3  | 4  | 5  | 5   | 7  | 8 | 9 | 10 | 10 | 8  | 6  | 5  |
| 76000-77999  | 20                                 | 3  | 4  | 5  | 5   | 7  | 8 | 9 | 10 | 10 | 8  | 6  | 5  |
| 78000-99999  | 20                                 | 3  | 4  | 5  | 5   | 7  | 8 | 9 | 10 | 10 | 8  | 6  | 5  |
|              |                                    |    | l  | 1  |     |    |   |   |    |    | -  |    |    |



Table B.25 Vehicle Registration Weight-Operating Weight Correspondence

Matrix for Combination Trucks Class 14

| Registration | Operating Weight Group Percentages |    |    |          |   |   |   |   |   |    |    |    |    |
|--------------|------------------------------------|----|----|----------|---|---|---|---|---|----|----|----|----|
| Weight (1bs) | 1                                  | 2  | 3  | 4        | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|              |                                    |    |    | <u> </u> |   |   |   |   |   |    |    |    |    |
|              |                                    |    |    |          |   |   |   |   |   |    |    |    |    |
| 0-19999      | 100                                |    |    |          |   |   |   |   |   |    |    |    |    |
| 20000-25999  | 100                                |    |    |          |   |   |   |   |   |    |    |    |    |
| 26000-29999  | 100                                |    |    |          |   |   |   |   |   |    |    |    |    |
| 30000-35999  | 95                                 | 5  |    |          |   |   |   |   |   |    |    |    | i  |
| 36000-41999  | 90                                 | 10 |    |          |   |   |   |   |   |    |    |    |    |
| 42000-47999  | 70                                 | 30 |    | •        |   |   |   |   |   |    |    |    |    |
| 48000-53999  | 65                                 | 35 |    |          |   |   |   |   |   |    |    |    |    |
| 54000-59999  | 55                                 | 45 |    |          |   |   |   |   |   |    |    |    |    |
| 60000-65999  | 45                                 | 45 | 10 |          |   |   |   |   |   |    |    |    |    |
| 66000-71999  | 40                                 | 48 | 12 |          |   |   |   |   |   |    |    |    |    |
| 72000-73999  | 35                                 | 50 | 15 |          |   |   |   |   |   |    |    |    |    |
| 74000-75999  | 30                                 | 50 | 20 |          |   |   |   |   |   |    |    |    |    |
| 76000-77999  | 25                                 | 50 | 25 |          |   |   |   |   |   |    |    |    |    |
| 78000-99999  | 25                                 | 50 | 25 |          |   |   |   |   |   |    |    |    |    |
|              |                                    |    |    |          |   | 1 | 1 |   | 1 | ł  |    |    |    |



#### APPENDIX C

### HIGHWAY CONSTRUCTION COST ALLOCATION

#### General

Highway construction costs are divided into the following items for cost-allocation purposes:

Right-of-Way costs

Grading and earthwork costs

Drainage and erosion control costs

Pavement costs

Shoulder costs

Miscellaneous costs

There are 874 contract sections of State highway in the IDOH Road Life Records. New construction project contracts are first identified. Cost information of these contracts is then extracted from Road Life Records, Construction Reports File and Itemized Proposal File. Further classification of these extracted costs is possible by highway type (Interstate, State Route or US Route), by surface type (concrete and bituminous), and by area type (rural, urban or mixed) from Road Life Records. Breakdown of each contract cost into the five allocation items mentioned above is derived from itemized costs available in Road Life Records and Itemized Proposal File.

# Right-of-Way Costs

The total right-of-way width is the sum of the widths of the following elements: pavements, shoulders, medians and borders. Pavement, shoulder and



median costs will be treated separately under headings of pavement costs and shoulder costs.

Costs considered under right-of-way include acquisition costs of right-of-way, preparation costs of right-of-way, relocation cost, utility adjustment cost and roadside development costs. Since right-of-way requirements are not the same for different highway classes, it is necessary to separate right-of-way costs according to the types of highways. A more complex procedure is to classify right-of-way costs by highway class, terrain type, and location (urban or rural). An analysis of the cost data is needed to determine if a detailed classification of right-of-way costs is justifiable.

Depending upon the design practice used in each state, right-of-way cost may or may not be a function of vehicle characteristics. For instance, Maryland [42] considered all right-of-way costs to be basic cost, whereas in Wisconsin study [48], only 47.4% are basic costs, the remaining 52.6% are allocated by incremental method with vehicle-miles used as the inter-group cost-allocator. Oregon study [33] allocated right-of-way cost incrementally by observed vehicle gross weight which was used as a proxy for vehicle size.

Of the various components of right-of-way costs, the land acquisition cost appears relatively easy to be allocated in the sense that it can be assumed to be proportional to overall right-of-way width. For other costs, there is no obvious logical procedure to be followed for allocation.

There is no specific right-of-way width requirements in Indiana. Generally the AASHTO standard [1] is adopted in practice. A summary of AASHTO right-of-way width design guidelines is shown in Table C.l. These design widths are applicable for rural highways where land acquisition is not a major



Table C.1. Right-of-Way Width Requirements

| Highway Type  |   | Right-of-way Width (ft.)                                     |
|---|---|--|
| 2-lane low type surface intermediate type surface high type surface |   | 66-80<br>80-100<br>100-120                                   |
| 4-lane divided highway  | restricted<br>intermediate<br>desirable | 90-110<br>140-180<br>210-310                                 |
| 6-lane and 8-lane highways  |   | add width of 12-ft<br>lanes to 4-lane right-<br>of-way width |



problem. Such widths are usually not attainable in urban highway construction.

An incremental approach may be developed for right-of-way costs on the basis that right-of-way width bears some relationship to design-hour volume expressed in passenger-car equivalents. This approach is not used in the present study for the following reasons:

- 1. As traffic volume increases, wider pavement, shoulder and median are needed to provide certain desired level of service. Wider right-of-way is required as a result. However, an increase in traffic volume generally represents a proportionate increase in all classes of vehicles rather than in a particular class of vehicle.
- 2. Greater width requirement represents a relatively small percentage of total right-of-way width. For a rural 4-lane highway with a right-of-way width of say 200 feet, an additional width of 8 ft accounts for only 4% of total width. Any additional responsibility of truck is likely to be offset by the automobile responsibility mentioned in item 3.
- 3. Wider highway is designed to accommodate peak traffic volume. For both rural and urban highways, studies [16] have indicated that the percentage of passenger cars and light trucks in design-hour volume is higher than their percentage in average daily traffic. On this aspect, passenger cars and light trucks tend to have higher responsibility than their percentage in ADT suggests.

The present study defines two components of right-of-way costs. The first portion of cost corresponds to a minimum right-of-way width as defined



by the AASHTO standard [1] - 66 feet for 2-lane highway, 90 feet for 4-lane, 108 and 120 feet for 6 and 8 lane highway, respectively. These form non-attributable portions of the right-of-way cost which is to be shared by all vehicles using the highway. The vehicle-miles of travel, which measures the relative use of highway by different vehicle classes, was used to allocate this common cost. The right-of-way costs of any highway with a right-of-way width below the stipulated minimum was allocated entirely on the basis of VMT.

Any additional width above the stipulated minimum, which leads to the second portion of right-of-way costs, can be considered to be capacity-related requirement. As such, they should be allocated in proportion to PCE-VMT (passenger car equivalent (PCE) - miles of travel).

In summary, the common cost portion of right-of-way costs is computed as the ratio of minimum right-of-way width to the actual width of the right-of-way. This cost portion is allocated on the basis of VMT. The remaining right-of-way costs are allocated according to VMT weighted by PCE.

## Grading and Earthwork Costs

Most studies consider the amount of grading and earthwork to be related to vehicle width and thus is a function of pavement width. Maryland study [42] divided these costs into two increments, namely the base facility costs for automobiles and the second increment for trucks and buses. The cost-allocator used within the two increments is PCE-miles of travel. Based upon the design criteria for different terrain characteristics, Wisconsin study [48] utilized computations for three standard terrain types (flat, rolling and hilly) to estimate the effect of different vehicle sizes. An incremental



analysis based on vehicle width was then used to allocate grading and earthwork costs. Oregon study [33] also allocated these costs incrementally by observed gross weight of vehicles.

In the present study, grading and earthwork costs represent the sum of roadbed excavation, filling, leveling and compaction costs. These cost items were extracted from data base compiled from IDOH cost files.

Following the same approach as in allocation of right-of-way costs, the grading and earthwork costs associated with a minimum road width was specified as common costs to be shared by all vehicles. Cost associated with additional road width in excess of the minimum was considered to be facility needed to satisfy capacity and level of service requirements. For the first portion of costs which correspond to work performed within the minimum road width, the cost-allocator was vehicle-miles of travel. The remainder of the costs was allocated on the basis of PCE-miles of travel.

AASHTO design guides [1] for traveled way widths were adopted for defining the minimum widths which were computed as the sum of minimum widths of pavement, median and shoulder, as shown in Table C.2.

A refinement in the allocation of grading and earthwork costs would have been possible if compaction costs could be extracted from the cost data. This compacted subgrade layer is frequently included in pavement design as a structural component of flexible pavement [49]. It serves to reduce the structural requirements of the pavement resting on it. It would therefore be more logical to distribute the compaction costs with a weight-related cost-allocator.

The costs of excavation in rolling or hilly terrain require a more



Table C.2. Traveled-Way Width Requirements

| Highway Type   | Min. Traveled -<br>Way Width (ft.) |
|----------------|------------------------------------|
| 2-lane highway | 2 6                                |
| 4-lane highway | 4 4                                |
| 6-lane highway | 56                                 |
| 8-lane highway | 68                                 |
|                |                                    |



detailed allocation procedure. Studies [17,40,46] have shown that the rate and length of a given grade have more effects in reducing the speeds of heavy vehicle. It has been found that the travel speed of vehicles on grades is a function of their weight-power ratio. AASHTO [1] provides recommended critical length of grade for design based on the requirement of heavy trucks with a weight-power ratio of 600 pounds per horsepower. Similar critical length and rate of grade relationships can be derived for other weight-power ratios. An incremental approach for allocation of grading costs in rolling or hilly terrain may be developed based on the different critical length and grade requirements of vehicles with different weight-power ratios.

This refined analysis was found unnecessary for the present study for the following reasons. Construction records for the base period (1980-83) show that most of the construction projects were reconstruction which were mainly improvements involving very little or no excavation of slopes. Of the few new construction projects completed within the base period, the length constructed in each project was relatively short. None of these construction projects were found to involve critical length consideration. The pattern of future construction in the study period (1985-86) is expected to remain the same, that is, predominantly reconstruction to improve geometric features and safety. Exclusion of critical length analysis for excavation costs therefore does not have any significant effect on the overall grading and earthwork cost-allocation.

## Drainage and Erosion Control Costs

Highway drainage facilities are constructed to remove storm water from paved roadway as well as across the entire width of the right-of-way.



Properly designed highway drainage facilities are essential to erosion prevention and control. The extent of drainage facilities and erosion control measures required is directly related to the amount of runoff expected. A logical allocation parameter for drainage and erosion control costs is therefore the runoff quantity which, for a given rainfall intensity, is a function of the area and surface type of the runoff watershed concerned.

Virtually all previous cost-allocation studies chose to combine drainage costs with grading costs and these costs were allocated largely on the basis of VMT or PCE-VMT. However, recognizing the distinct feature of design consideration concerning drainage and erosion control facilities as discussed in the preceding paragraph, it was decided in the present study to treat the costs associated with providing these facilities separately from grading and earthwork costs.

The allocation procedure for drainage and erosion control costs adopted in this study has its basis on the long-used rational method for runoff estimation. This method is still the most practical approach for calculating the peak rate of runoff for roadway. The basic equation is:

Q = ciA

where,

Q = peak rate of runoff, in cfs;

c = runoff coefficient;

i = rainfall intensity in/hr;

A = watershed area in acres.



For heavily vegetated area, the runoff coefficient was taken as 0.2 and for paved surfaces, it was 0.9. This means that, for a given rainfall intensity, a unit area of paved surface would produce 4.5 times as much runoff as that from a unit area of vegetated ground. Using this value of 4.5 as weighting factor for paved surfaces, the cost-allocating procedure proceeded as follows:

- i. The total drainage and erosion control cost was first split into two components, namely paved-surface responsibility cost, and non-paved-surface responsibility cost. These two cost components were computed in proportion to their respective weighted widths. Paved surface is basically the roadway itself and the weighting factor is 4.5. For non-paved surface, the weighting factor is 1.0.
- ii. The paved-surface responsibility cost was allocated by first defining a minimum roadway width. This minimum roadway width is the sum of minimum traveled way width and minimum shoulder width, specified respectively in Table C.2 and in section on allocation of shoulder costs. Cost associated with the minimum roadway width was allocated as common cost on the basis of VMT. Cost corresponding to additional roadway width in excess of the minimum was allocated on the basis of PCE-miles of travel.
- iii. The non-paved-surface responsibility cost was allocated by considering minimum non-paved-surface width which is given by the difference between minimum right-of-way defined in Table C.2 and the minimum roadway width computed in Step ii above. Again, costs associated with the minimum width was allocated on the basis of VMT, and that associated with excess width on the basis of PCE-VMT.



iv. For each vehicle class, its total cost responsibility was determined by the sum of its respective cost responsibility computed in Steps ii and iii.

## New Pavement Costs

This section covers allocation of costs for constructing new pavement only. Cost of repair for pavement deterioration with age or pavement damage through vehicle use are dealt with in the section on rehabilitation cost allocation. Because of this distinction, it was decided that allocation of new pavement cost would not be based on wear-related criteria. Instead, occasioned costs were determined by analyzing engineering details involved in the design of pavement. The appropriate costs were assigned to the responsible vehicle class or classes accordingly.

The procedure of rigid and flexible pavement design adopted by IDOH [50] formed the basis of engineering analysis for pavement cost in this study. This procedure followed essentially the method outlined in 1980 AASHTO Interim Guide for Design of Pavement Structures [2]. Traffic loadings were expressed in terms of equivalent 18-kip single axle load applications (ESAL) for design of both flexible and rigid pavements. Thickness of flexible pavement was obtained by converting the structural number of the pavement concerned using Indiana material factors recommended by IDOH [50]. The structural number, determined with charts in AASHTO Interim Guide [2], is a function of serviceability index, soil support value, regional location, ADT factor and total 18 kip single axle load applications. Thickness of rigid pavement is derived directly from



charts in AASHTO Interim Guide [2] with the following input data: serviceability index, modulus of subgrade reaction, load transfer factor for reinforced concrete (RC) pavement, working stress and modulus of elasticity of concrete, ADT factor and total 18 kip single axle load applications.

Traditionally, pavement thickness costs have been allocated using the standard incremental method [24] developed almost two decades ago. However, recent research on pavement performance suggests several drawbacks of the traditional incremental method of new pavement costallocation. The most important drawback is that this method arbitrarily assigns the benefits of economy of scale to heavier vehicles [7].

A revised incremental procedure was developed in the present study aiming to (i) overcome the problem of economies of scale in pavement cost-allocation, and (ii) be in consistence with the design procedure used in Indiana.

The cost-allocation procedure, known as the Thickness Incremental Method, was developed by Fwa and Sinha [12] for the present study. It begins by defining pavement thickness increments, in contrast to the common practice of starting with traffic increments or decrements. There are two advantages with the proposed approach: (a) by beginning with a given thickness, no iterative procedure is necessary in calculating ESALs; (b) because pavement cost is more directly related to pavement thickness than traffic loading, a better control over the accuracy of the result can be achieved by using pavement thickness as the starting parameter.



In defining the number and magnitude of pavement thickness increments, the minimum practical pavement thickness must first be determined. In accordance with IDOH design practice, the following minimum thicknesses were considered to be the basic cost components which are required for flexible pavement regardless of the traffic level:

Surface Course 1 inch

Base Course 3 inches

Subbase Course 4 inches (if subbase is used)

For rigid pavements, the minimum thickness was taken as 4-1/2 inches. Only those costs corresponding to the thickness in excess of the specified minimum were allocated by the incremental approach described in this section. The pavement costs associated with the minimum thickness were allocated on the basis of VMT.

The total thickness in excess of a specified minimum is divided into increments, the number and thickness of which depend on the desired accuracy of the final results. Beginning with the specified minimum thickness, a thickness increment is first added. With this total thickness, the ESAL of each vehicle type or a representative vehicle type of a vehicle class can be computed directly from the following equation which was developed from the AASHO Road Test [2,15]:

$$Log ESAL_{x} = G_{t} \left[ \frac{1}{b_{18}} - \frac{1}{b_{x}} \right] + Log \left\{ \left[ \frac{L_{x} + L_{2}}{19} \right]^{A} / L_{2}^{B} \right\}$$

where,  $ESAL_{x}$  = equivalent single axle load of axle type x;



G<sub>t</sub> = a function of the ratio of loss in
 serviceability to the potential loss
 taken to a point where terminal serviceability
 index (p<sub>t</sub>) is 1.5;

b = a function related to axle weight of
 vehicle type x, pavement strength and
 pavement thickness;

b = a function related to a single axle weight
of 18 kips, pavement strength and
pavement thickness;

L = axle load in kips;

L<sub>2</sub> = 1 for single axles, 2 for tandem axles;

A = 4.79 for flexible pavement, 4.62 for rigid pavement;

B = 4.33 for flexible pavement,
3.28 for rigid pavement.

In calculating ESAL with the above formula, Indiana practice [50] was followed. A terminal serviceability index  $p_t$  value of 2.5 or 2.0 was used for flexible pavement, and 2.5 for rigid pavement. The following material constants were used for computing pavement strength:

Bituminous Surface = 0.4/inch

Bituminous Binder = 0.34/inch

Bituminous Base = 0.3/inch

Bituminous Stabilized Subbase = 0.24/inch



Compacted Aggregate Type "p" = 0.14/inch

Granular Subbase = 0.08/inch

The same procedure was repeated for each additional increment until the total thickness was reached. The incremental pavement thickness cost corresponding to each thickness increment was assigned to all vehicle classes based on their need for that thickness according to pavement design procedure. Accordingly, the proportional amount of pavement thickness cost attributable to a given vehicle is in direct proportion to its ESAL value. With the same reasoning, the proportional cost responsibility of a given vehicle class is equal to its proportional contribution to the total ESAL of the entire traffic stream.

At any given pavement thickness, it is possible to calculate the corresponding total ESAL. However, this information is not essential because only the proportional contribution of ESAL from individual vehicle classes are needed. It can be logically assumed that the traffic responsible for any intermediate pavement thickness has the same vehicle class composition as that of the actual traffic stream for which the total pavement thickness is designed. Since the proportions of individual vehicle classes in the entire traffic stream are known, their proportional ESAL at any given pavement thickness can be obtained by multiplying each vehicle class traffic proportion by a single vehicle ESAL representative of the vehicle class. However, as the procedure can be made more accurate with information on axle weight distribution within each vehicle class, the analysis in this study was performed in terms of axle weight groups. Extending the idea further, the same cost-



allocation procedure can be even followed using individual vehicle type, instead of vehicle class or axle weight group, as the basic unit. This means that a separate within-class cost-allocation step is not necessary with the proposed procedure.

By having each vehicle class proportionally represented each time an incremental cost is allocated, the cost-allocation procedure described above effectively eliminates the economies of scale problem associated with the traditional incremental method. It also allocates all pavement thickness in excess of a specified minimum in consistence with thickness design concept and avoids the problem of having an unaccounted for residual thickness as is found when using Wisconsin's BAR method [48]. Iterative procedure which is a routine in all existing methods is bypassed by taking thickness increment as the starting parameter. Furthermore, the procedure is easy to understand because it follows the usual thinking of increasing pavement thickness to account for increasing traffic. A description of the computational algorithm of the thickness incremental method is presented below.

Inputs to the algorithm include (a) cost information, (b) pavement data, (c) traffic composition, vehicle axle configuration and axle-weight data. For rigid pavement, cost can be assumed to be directly proportional to the slab thickness. For flexible pavement, separate costs for surface, base and subbase construction are needed.

The computation algorithm for cost-allocation involves the following steps:



- 1. Divide the pavement thickness in excess of a practical minimum into N equal increments. In the case of flexible pavement, each increment is composed of thickness of surface, base and subbase materials in the same proportions as are in the total 'excess' thickness to be allocated.
- Calculate the cost for the minimum thickness and distribute to all vehicle classes on the basis of VMT.
- Calculate the incremental thickness cost.
- 4. Add an increment to the minimum thickness, and compute ESAL for all vehicle classes (or vehicle types if desired) using AASHTO ESAL equations.
- 5. Compute the cost responsibility factor of each vehicle class (or vehicle types) as the following ratio:

$$F(i,j) = P(i) \times ESAL(i,j) / \sum_{r=1}^{M} \left[ P(r) \times ESAL(r,j) \right]$$

where,

P(i) = proportion of vehicle class i in traffic stream

ESAL(i,j) = ESAL of vehicle class i for thickness increment j
M = total number of vehicle classes

6. Allocate incremental thickness cost to each vehicle class as follows:



$$c(i,j) = F(i,j) \times Cd(j)$$

where,

c(1,j) = cost allocated to vehicle class i for thickness
increment j

- Cd(j) = incremental cost for thickness increment j
- 7. Repeat steps 5 and 6 for each new thickness increment until the full pavement thickness is reached.
- 8. Calculate the total allocated cost for vehicle class j by summing up its cost responsibility for all increments:

$$C(i) = Cm(i) + \sum_{j=1}^{N} c(i,j)$$

where,

C(i) = total cost responsibility of vehicle class i

Cm(1) = cost responsibility of vehicle class i for the
 miniumum thickness

N = total number of thickness increments

For new pavement width in excess of a specified minimum pavement width, a slightly modified allocation procedure is required. A pavement width of 9 feet per lane was taken as the minimum width in the present study. The portion of pavement width in excess of 9 feet was allocated by the same incremental allocation procedure described earlier, except that the pavement costs associated with each extra thickness increment



for the additional width were allocated differently. Instead of allocating according to each vehicle class' share of total ESAL, a combination of PCE and ESAL is used as the allocator. This is in recognition of the effects larger vehicles have on roadway width and roadway capacity.

## Shoulder Costs

In previous highway cost-allocation studies, shoulder costs have been handled in several different ways. Some studies [7] suggest that shoulder and pavement costs be grouped together on the assumption that both costs are occasioned by the same vehicles in the same proportions. Other studies [32,48] treated shoulder costs separately using a minimum width approach by assuming certain shoulder width is required by all vehicles. Any width in excess of this minimum is taken to be occasioned by larger vehicles.

In the process of selecting a procedure for allocating shoulder costs in the present study, the major functions of a shoulder were first examined. The AASHTO Manual on Geometric Design [1] lists the following shoulder functions:

- 1. Space is provided for stopping free of the traffic lane due to motor trouble, flat tire or other emergency.
- Space is provided for the occasional motorist who desires to stop to consult road maps, to rest, or for any other purpose.
- Space is provided to escape potential accidents or reduce their severity.



- 4. The sense of openness created by shoulders of adequate width contributes much to driving ease and freedom and strain.
- Sight distance is improved in cut sections and, thus, hazard is reduced.
- The capacity of the highway is improved. Uniform speed is encouraged.
- Space is provided for maintenance operations.
- Lateral clearance is provided for signs and guard rails.
- Storm water can be discharged farther from the pavement and seepage adjacent to the pavement minimized.
- 10. Structural support is given to the pavement.

Strictly speaking, only items 1, 2 and 3 are affected by the presence of trucks. It is therefore not entirely correct to claim that shoulder width in excess of a certain minimum is due completely to larger or heavier vehicles. Consequently, it appears that an equitable approach is to allocate excess width costs on the basis of PCE-VMT, which is a parameter more closely related to capacity and level of service considerations.

In allocating shoulder thickness costs, it is realized that shoulder thickness is not designed for the same traffic loading as that for pavement. It may be argued, however, that the same percentage of cars and trucks in traffic stream will make use of the shoulder provided. If this



assumption is true, then it would be acceptable to follow pavement costallocation procedure.

A procedure was developed to satisfy both the shoulder width and thickness criteria described above. Shoulders of 2-foot and 6-foot were considered to be the minimum widths in this study for 2-lane and 4-or more lane highway, respectively. This implies that the costs of all shoulders with width less than the minimum were allocated using the thickness incremental approach developed for pavement cost-allocation. For shoulder width in excess of the minimum, the corresponding cost in proportion to width was allocated by the same procedure, but with the allocation parameter weighted by PCE.

#### Reconstruction Costs

Reconstruction involves construction on approximate alignment of an existing route where old pavement may be removed and replaced. It includes widening projects which provide additional width to existing pavements; improvements of highway geometry such as realignment of roadway on existing right-of-way, and upgrading of unsafe features.

In many cases, reconstruction projects recorded in the IDOH construction records included other incidental improvements such as resurfacing of adjoining existing pavement in a roadway realignment project or resurfacing of existing lanes in a widening contract. These resurfacing costs were separated from new pavement construction cost, and allocated by means of rehabilitation cost-allocation procedure discussed in a later section of this report.



Other expenditures such as right-of-way, shoulder, drainage improvements and earthwork costs in reconstruction projects were allocated using the same procedure developed for allocating the corresponding items in new construction.

# Miscellaneous Items

Construction costs of items not allocated under the four cost categories discussed in previous sections were considered individually to determine the cause for incurring these costs and the appropriate cost-allocator was used.

Engineering services, installation of traffic control devices, pavement marking are examples of cost items which cannot be allocated specifically to any vehicle groups. These costs can be treated as common costs and allocated on the basis of VMT, which is a measure of the relative use of highway by various vehicle groups.

For items which are provided exclusively for a specific group of vehicles, the corresponding costs should be allocated accordingly to this vehicle group only. Some examples are construction of climbing lanes and weigh stations. These facilities are constructed exclusively to serve heavy vehicles. Cost of these items should therefore be allocated entirely to these vehicles. Further within-group distribution of these costs was based on VMT. Miscellaneous costs also included administration and supervision costs. These costs were distributed as common costs among all vehicle classes according to VMT.



#### APPENDIX D

#### HIGHWAY REHABILITATION COST ALLOCATION

#### General

Rehabilitation can be considered as a large scale maintenance operation in the sense that both rehabilitation and maintenance aim at maintaining ride quality and structural condition. They are different, however, since maintenance refers to minor activities which are carried out routinely, whereas rehabilitation activities are required only when routine maintenance operation can no longer maintain the quality of highway desired. It is therefore important to realize in allocating expenditures of a highway item, particularly pavement related expenditures, that although the causes for maintenance and rehabilitation operations are usually the same, there is a significant difference in the scale of deterioration associated with the operations.

Rehabilitation costs in this study are defined as being the expenditures spent to restore the level-of-service of highways in Indiana.

Rehabilitation consists of major reconstruction or resurfacing activities that are not classified and coded as routine maintenance activities of IDOH.

### Previous Studies

Only a few previous cost-allocation studies treated rehabilitation as a separate expenditure category. A majority of these studies grouped rehabilitation costs with construction costs and allocated them based on the same methods used for allocating construction costs [28,33,42]. The



1982 Virginia study [22] separated rehabilitation projects into construction and maintenance categories. Rehabilitation costs were included in construction costs and allocated accordingly if rebuilding occurred along with improvement in capacity, alignment, grade or other features of roadway geometry. Otherwise, they were allocated as maintenance costs.

Wisconsin study [48] allocated rehabilitation costs separately from construction and maintenance costs. Rehabilitation costs were divided into basic, service, and fixed portions. The basic portion included costs required to provide the level-of-service to accommodate the passenger cars. The service portion of costs were required to provide a level-of-service beyond the basic level-of-service. Fixed costs were the costs resulted from natural phenomena. Different methods and cost-allocators were employed to allocate these three types of costs.

In most cases, previous studies allocated common costs based on VMT and traffic attributable costs based on weight-related cost-allocators, such as ESAL, axle-miles, and ton-miles although the methods may vary among the studies. The decision to estimate rehabilitation costs caused by weather only was primarily based on engineering judgments.

The recent FHWA Cost-Allocation Study [9,34] recommended an approach to allocate rehabilitation costs using a series of distress functions. The distress functions were developed for the most important distress types for both flexible and rigid pavements and four different climatic zones were considered. Appropriate load equivalency factors were generated to represent the interaction of traffic and weather in causing a particular distress. These equivalency functions can then be used to



allocate rehabilitation costs, once the proportion of these costs occurrenced by individual distress types are identified.

FHWA model [34] developed for application in nationwide study is not directly applicable to any state level analysis without considerable amount of modification. In addition, FHWA study did not consider routine maintenance costs since routine maintenance is the charge of individual state highway agencies. Consequently, the FHWA procedure does not provide any criterion for differentiating rehabilitation responsibilities from routine maintenance responsibilities of vehicle classes. If FHWA procedure were to be used for allocating rehabilitation costs at state level, one would be confronted with the problem of what type of damage or distress functions should be used for allocating routine maintenance costs. Double counting appears to be unavoidable if a damage function approach is also used for allocating routine maintenance costs.

# Allocation Procedure for Pavement Rehabilitation Costs

Rehabilitation and routine maintenance, though involve different forms of activities and end results, are interdependent and closely related. It is important that a consistent unified approach be used for allocating rehabilitation and routine maintenance costs so that rehabilitation responsibilities could be separated from routine maintenance responsibilities, and that no double counting would occur. Described in this section is a procedure for allocating pavement rehabilitation costs, which presents an attempt to satisfy the above requirements. The corresponding procedure for allocating routine maintenance costs is presented in a subsequent section.



In the section on allocation of new pavement costs. Following this design concept, it implicitly implies that, in an ideal situation where the design conditions are correctly predicted, a pavement constructed accordingly would be able to serve the design traffic until the end of its design life when the pavement PSI reaches a predetermined terminal PSI level at which a rehabilitation is deemed necessary to restore the pavement PSI to its original as-constructed level.

It is logical to say that the cost incurred in designing and constructing the original pavement has accounted for the pavement wear caused by traffic over the period of its design life. The purpose of rehabilitating the pavement is to give it another service life span to serve the traffic. The vehicle classes that use the rehabilitated pavement must therefore pay for the rehabilitation cost. With this reasoning, a cost allocation concept similar to that used for allocating new pavement cost was followed.

Consider again the ideal design conditions and assume that a decision to rehabilitate a pavement is made at the end of the design life of the pavement. If there is no other factors additional to those for which the pavement was designed, the rehabilitation costs incurred would be due to design factors only and therefore have to be shared by all the vehicles that would be using the rehabilitated pavement.

There is no standard or generally accepted overlay design procedure available. AASHTO Interim Guide [2] classifies overlay design practice into several categories. For the purpose of the present study, the



AASHTO Interim Guide procedure was considered to be most suitable in that it provides consistency in approaches in allocating different components of pavement costs.

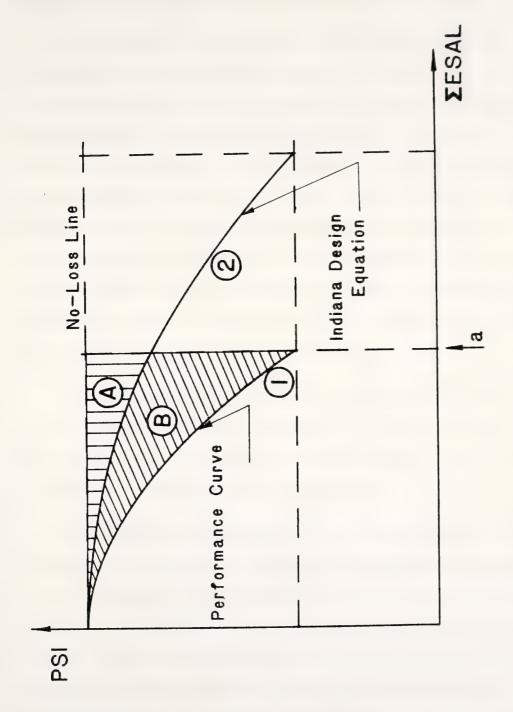
The basic idea of the AASHTO Interim Guide [2] approach for overlay design is to subtract the existing pavement structure thickness from the total thickness required by a new design analysis. In using this procedure, in addition to a soil support value, each of the existing layers is assigned a layer coefficient.

In a cost-allocation analysis, the thickness of overlay constructed is known from the base year data. It is not necessary to go through the design computation again. The procedure developed in the present study for allocating new pavement costs, namely the Thickness Incremental Method, was applied to allocate the part of the rehabilitation cost related entirely to traffic based upon the thickness of overlay constructed.

Factors other than traffic loading which is the primary factor in Indiana pavement design procedure, are also responsible for the loss of PSI of a pavement. These non-traffic factors include severe weather and de-icing chemicals, faults in engineering design, defects in material used, and poor construction quality. If no routine maintenance were carried out, a pavement performance in terms of PSI would fall below the PSI curve predicted by pavement design equations as shown in Figure D.1.

In Figure D.1, area A represents a measure of the pavement wear or damage due to traffic and other design factors, and area B represents the further pavement wear due to non-traffic factors and interaction of





Schematic Diagram Showing Pavement Performance Considered in Highway Rehabilitation Cost Allocation Figure D.1.



traffic and non-traffic factors. We may conclude that the proportion of design-factor related rehabilitation costs is given by  $(\frac{A}{A+B})$ .

The non-traffic plus interaction effects are responsible for  $(\frac{B}{A+B})$  of the costs for rehabilitation at stage 'a'. This portion of the rehabilitation costs would have to be further divided into traffic-related and non-traffic related costs. Direct allocation on the basis of a cost allocator such as VMT or ESAL is undesirable because such approach does not differentiate between traffic and non-traffic effects. Delphi technique has been used in some studies to obtain the proportional responsibility of traffic and non-traffic effects. However, on a topic such as this where there is a wide disparity of views among highway pavement experts, it is doubtful that efforts to find averages from pooling opinions would produce any meaningful results.

A methodology was developed for use in the present study to determine the responsibilities of load-related and non-load-related factors for pavement routine maintenance and rehabilitation costs. The procedure involved is described in detail in Appendix H.

As design criteria are different for different climatic regions, highway classes and types of pavement, it is necessary to group pavements by region, highway class and pavement type. In the present study, two regions, five highway classes and four pavement types are being considered. The two regions refer to northern and southern Indiana. The five highway classes include Interstate, state routes primary, state routes secondary, city streets and county roads. The four pavement types are flexible pavements, rigid pavements with bituminous overlay, JRC and



CRC pavements. Appropriate pavement wear responsibility factors were developed by region, highway class and pavement type.

These factors were then used to compute load-related and non-load-related portions of the pavement rehabilitation cost of a given rehabilitation project. For the load-related portion of the cost, the Thickness Incremental Method was applied for cost-allocation computation. In this instance, the original existing pavement thickness was taken as the basic minimum thickness with zero cost, and the incremental analysis was carried out for the added overlay thickness. The non-load-related portion of the cost was considered to be common cost and it was allocated on the basis of VMT.



#### APPENDIX E

# STRUCTURAL CONSTRUCTION, REPLACEMENT AND REHABILITATION COST ALLOCATIONS

#### General

In the present study, structural expenditures included the following:

- (a) bridge construction
- (b) bridge rehabilitation
- (c) bridge replacement
- (d) culvert construction
- (e) sign structure construction

Definitions of these expenditure items are as follows:

- 1. Bridge Construction: New bridges constructed on new alignment.
- 2. Bridge Replacement: Bridges built to replace existing bridges basically on the same alignment.
- Bridge Rehabilitation: Widening, deck repair and partial replacement.
- 4. Culvert Construction: Drainage structures such as box culverts and metal pipes.
- 5. Sign Sructure Construction: Overhead traffic signs.



An incremental method involving repetitive designing of a given structure for different vehicle loadings was selected for allocating the structure costs.

# Adopted Incremental Method

In this procedure, a bridge was designed and cost estimated for the full design loading anticipated. The first group of heavy vehicles was then removed and a second design was prepared and cost estimated. The difference in costs between the initial design and the second design was assigned to the heavy vehicles removed. Next, a second group of heavy vehicles was removed along with the first, and a third design was made with associated cost estimate. The difference in costs between the second and third designs was assigned to all vehicles removed up to this point. This process was repeated until no significant difference could be observed in the cost of the needed facility due to the removal of a vehicle group. Costs below this point were assigned to all vehicles expected to use the bridge.

# Design Loadings

In this study, bridges were designed according to guidelines prepared by the American Association of State Highway and Transportation Officials (AASHTO). The AASHTO Bridge Specifications [3] provided traffic related loadings designated with a H prefix followed by a number indicating the total weight of trucks in tons for a two-axle trucks or with a HS prefix followed by a number indicating the weight in tons for tractor-trailer combinations. The smallest loading used in the study was



6000 pounds corresponding to AASHTO loading H3. The effect of vehicle weight below this level is almost totally obscured by the effect of snow, wind and the dead weight of the bridge itself. The vehicle loading of H3 corresponded to the 'basic' vehicle in this study.

The AASHTO live load configurations used in the study are shown in Figure E.1. For heavier vehicles, weights were distributed to front and rear axles in accordance with AASHTO specifications [3]. For lighter vehicles, the share of the total weight on each axle was gradually shifted towards the front wheel so that the axle weights become close to the axle weights that result from passenger cars. Since these AASHTO design vehicle are not the trucks seen operating on the highways but rather trucks with configurations that would simulate the most severe live loads on the structure, a quantitative correlation between the real trucks operating on highways and the design index loading was established in order to assign the cost increment to a vehicle group used in the study.

#### Correlation Between AASHTO and Actual Trucks

Many methods of establishing correlation had been established by other cost allocation studies. The FHWA study [9] and the Wisconsin study [48] used the gross vehicle weight (GVW) to correlate the AASHTO vehicle types with the observed vehicle groups. This approach assumes a simple relationship between design vehicle loading and gross vehicle weight of observed vehicles. From the design point of view, this assumption is not justifiable because factors such as axle-load distribution and axle spacing are neglected. The Maryland study [42] used a more



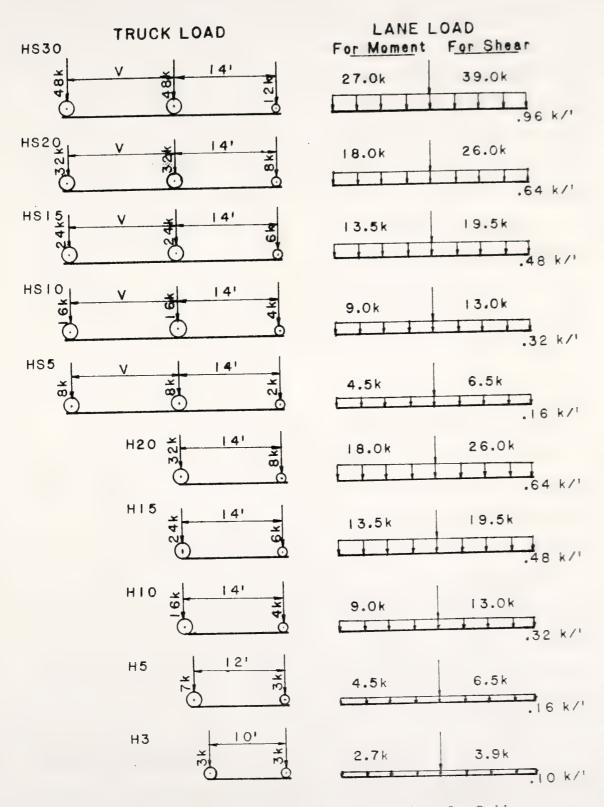


Figure E.1. Modified AASHTO Live Loading Configurations for Bridge Incremental Designs



rational method in establishing the correlation as it incorporated both axle loading and axle spacing. However, each truck type was placed on a series of simple spans instead of a continuous span. The results obtained by using a series of simple spans would involve some approximations when extended to bridges with continuous spans. In this study, design vehicles and the observed vehicles were related according to the bending moment they created on a continuous bridge of typical spans. The observed vehicles were divided into 14 classes and some of these classes consisted of vehicles operating at a wide distribution of weights.

Therefore, the axle-load distribution and axle spacing of each of the vehicle classes were determined by analyzing the 1983 IDOH truck weight survey data. A summary of this analysis is presented in Table E.1. The resulting correlation between design vehicle types and observed vehicle classes is given in Table E.2.

In order to make the correlation between H and HS trucks and the observed vehicles, it was necessary to develop a relationship between AASHTO H and HS trucks as shown in Figure E.2. A computer program was used to obtain this correlation. The program moved a vehicle across a bridge (with variable span lengths) such that each axle in turn falls at the critical point of equal continuous spans. As each axle was positioned, the moment at the critical point was calculated for the whole vehicle on the bridge. The results were expressed in terms of equivalent AASHTO vehicle. A flow diagram of the computer program is shown in Figure E.3.

# Selection of Bridge Samples

After reviewing the data for the base period it was observed that



Table E.L. Study Vehicle Classification and Equivalent AASHTO Designation

|              |         |          |          |          |        | 2        |      |       |        | 3     |       |      | 4                |
|--------------|---------|----------|----------|----------|--------|----------|------|-------|--------|-------|-------|------|------------------|
|              | 1       |          | Doc      | ton Av   | 10 100 | d (Kips) |      | A     | xle Sp |       | (Ft.) |      | Equivalent       |
| Vehicle Type |         | Δ        |          | C V      | D      | E        | F    | AB    | BC     | CD    | DE    | EF   | AASHTG Venicle   |
|              | Kips    | <u>A</u> | <u>B</u> | <u>~</u> |        |          | _    |       |        |       |       |      |                  |
| 1            | 4.0     | 2.0      | 2.0      |          |        |          |      | 7.2   |        |       |       |      | H2.9             |
| 2            | 6.0     | 3.0      | 3.0      |          |        |          | 1    | 0.05  |        |       |       |      | H4.0             |
| 3            | 30.0    | 12.0     | 18.0     |          |        |          | 3    | 31.65 |        |       |       |      | H17.0            |
| 4            | 5-10.0  | 4.5      | 5.5      |          |        |          |      | 1.0   |        |       |       |      | HE.5             |
| 4            | 10-15.0 | 6.5      | 8.5      |          |        |          | 1    | 13.0  |        |       |       |      | H9.41            |
| 4            | 15~20.0 | 7.7      | 12.3     |          |        |          |      | 14.0  |        |       |       |      | H12.95           |
| 4            | 20-25.0 | 10.2     | 14.8     |          |        |          |      | 15.0  |        |       |       |      | H15.29           |
| 4            | 25-30.0 | 12.0     | 18.0     |          |        |          | 1    | 17.0  |        |       |       |      | H17.67           |
| 5            | 9.0     | 4.0      | 4.0      | 1.0      |        |          | 1    | 11.5  | 8.6    |       |       |      | HS3.0            |
| 6            | 10-15.0 | 5.0      | 6.0      | 4.0      |        |          | 1    | 14.0  | 4.0    |       |       |      | HS6.0            |
| 6            | 15-20.0 | 8.0      | 6.0      | 6.0      |        |          | 1    | 14.0  | 4.0    |       |       |      | HS7.0            |
| . 6          | 20-25.0 | 10.0     | 7.0      | 8.0      |        |          | 1    | 14.0  | 4.0    |       |       |      | HS8.0            |
| 6            | 25-30.0 | 12.0     | 8.0      | 10.0     |        |          | 1    | 14.0  | 4.0    |       |       |      | HS10.0           |
| 6            | 30-35.0 | 13.0     | 10.0     | 12.0     |        |          | 1    | 14.0  | 4.0    |       |       |      | HS11.0           |
| 6            | 35-40.0 | 15.0     | 12.0     | 13.0     |        |          |      | 14.0  | 4.0    |       |       |      | HS13.0           |
| 7            | 0-20.0  | 7.0      | 8.0      | 5.0      |        |          |      | 10.0  | 16.0   |       |       |      | HS6.0            |
| 7            | 20-25.0 | 9.0      | 10.0     | 6.0      |        |          |      | 10.0  | 17.0   |       |       |      | HS7.0            |
| 7            | 25-30.0 | 9.0      | 11.0     | 10.0     |        |          |      | 10.0  | 18.0   |       |       |      | HS8.0            |
| 7            | 30-35.0 | 10.0     | 13.0     | 12.0     |        |          |      | 10.0  | 21.0   |       |       |      | HS9.0            |
| 8            | 10.00   | 4.0      | 4.0      | 1.0      | 1.0    |          |      | 11.5  | 8.60   | 5.80  |       |      | HS3.50           |
| 9            | 0-30.0  | 6.0      | 6.0      | 18.0     |        |          |      | 4.0   | 40.0   |       |       |      | HS13.0           |
| 9            | 30-60   | 16.0     | 16.0     | 28.0     |        |          |      | 4.0   | 40.0   |       |       |      | HS23.0           |
| 10           | 0-40.0  | 13.0     | 9.0      | 9.0      | 9.0    |          |      | 17.30 | 4.0    | 21.00 |       |      | HS10.0           |
| 11           | 20-25.0 | 7.0      | 8.0      | 5.0      | 5.0    |          |      | 10.0  | 22.0   | 4.0   |       |      | HS7.0            |
| ii           | 25-30.0 | 8.0      | 10.0     | 6.0      | 6.0    |          |      | 10.0  | 22.0   | 4.0   |       |      | HS8.0            |
| 11           | 30-35.0 | 9.0      | 11.0     | 7.0      | 8.0    |          |      | 10.0  | 22.0   | 4.0   |       |      | HS9.0            |
| 11           | 35-40.0 | 10.0     | 14.0     | 8.0      | 8.0    |          |      | 10.0  | 22.0   | 4.0   |       |      | HS10.0           |
| 11           | 40-45.0 | 10.0     | 15.0     | 10.0     | 10.0   |          |      | 10.0  | 22.0   | 4.0   |       |      | HS11.0           |
| 11           | 45-50.0 | 10.0     | 16.0     | 12.0     | 12.0   |          |      | 10.0  | 22.0   | 4.0   |       |      | HS12.0           |
| 11           | 50-55.0 | 11.0     | 18.0     | 13.0     | 13.0   |          |      | 10.0  | 22.0   | 4.0   |       |      | HS14.0           |
| 12           | 20-25.0 | 7.0      | 6.0      | 6.0      | 3.0    | 3.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS7.0<br>HS8.0   |
| 12           | 25-30.0 | 8.0      | 7.0      | 7.0      | 4.0    | 4.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      |                  |
| 12           | 30-35.0 | 9.0      | 8.0      | 8.0      | 5.0    | 5.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS9.0            |
| 12           | 35-40.0 | 10.0     | 9.0      | 9.0      | 6.0    | 6.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS10.0           |
| 12           | 40-45.0 | 11.0     | 10.0     | 10.0     | 7.0    | 7.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS11.0<br>HS12.0 |
| 12           | 45-50.0 | 12.0     | 11.0     | 11.0     | 8.0    | 8.0      |      | 10.0  | 4.0    | 25.0  | 4.0   |      |                  |
| 12           | 50-55.0 | 11.0     | 12.0     | 12.0     | 10.0   | 10.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS13.0<br>HS14.0 |
| 12           | 55-60.0 | 10.0     | 13.0     | 13.0     | 12.0   | 12.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      |                  |
| 12           | 60-65.0 | 10.0     | 14.0     | 14.0     | 13.0   | 13.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS15.0<br>HS17.0 |
| 12           | 65-70.0 | 10.0     | 16.0     | 16.0     | 14.0   | 14.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      |                  |
| 12           | 70-75.0 | 11.0     |          | 17.0     | 15.0   | 15.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS18.0<br>HS19.0 |
| 12           | 75-80.0 | 12.0     |          | 18.0     | 16.0   | 16.0     |      | 10.0  | 4.0    | 25.0  | 4.0   |      | HS11.0           |
| 13           | 0-40.0  | 5.0      |          | 12.0     | 8.0    | 8.0      |      | 9.0   | 18.0   | 5.0   | 11.0  |      | HS17.0           |
| 13           | 40-70.0 | 10.0     |          | 16.0     | 13.0   | 13.0     |      | 9.0   | 18.0   | 5.0   | 11.0  | 11.0 | HS11.0           |
| 14           | 0-40.0  | 8.0      |          | 7.0      | 8.0    | 5.0      | 5.0  | 10.0  |        | 21.0  | 5.0   | 11.0 | HS19.0           |
| 14           | 40-60.0 | 9.0      |          | 12.0     | 13.0   | 7.0      | 7.0  | 10.0  |        | 21.0  | 5.0   | 11.0 | HS24.0           |
| 14           | 60-80.0 | 9.0      | 16.0     | 16.0     | 17.0   | 11.0     | 11.0 | 10.0  | 4.0    | 21.0  | 0.0   | 11.0 | 1104710          |

<sup>1.</sup> Refer to Table 1 for vehicle type description.

<sup>2.</sup> A = first axle B = second axle C = third axle D = fouth axle E = fifth axle F = sixth axle

<sup>3.</sup> AB, BC, CD, DE, and EF = distance in feet between adjacent axles

<sup>4.</sup> Refer to Figure E.1 for AASHTO vehicle type description.



|   |         |         |         |            |       |       | 07-0  |       |       |      |       |       | 09-05 |      |       |      | 08-09 |     |       |      |      |      |      |
|---|---------|---------|---------|------------|-------|-------|-------|-------|-------|------|-------|-------|-------|------|-------|------|-------|-----|-------|------|------|------|------|
|   | 14      |         |         |            |       |       |       |       |       |      |       |       |       |      |       |      | -09   |     |       |      |      |      |      |
|   | 13      |         |         |            |       |       | 0-40  |       |       |      | 40-70 |       |       |      |       |      |       |     |       |      |      |      |      |
|   | 12      |         |         | 20-75      | 25-30 | 35-40 | 40-45 | 50-55 |       | 9-09 | 65-70 | 70-75 | 75-80 |      |       |      |       |     |       |      |      |      |      |
| 1<br>ype                                    | =       |         |         | 20-75      | 25-30 | 30-35 | 40-45 | 45-50 | 50-55 |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
| Gross Vehicle Weight (Kips) of Vehicle Type | 10      |         |         |            |       | *     |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | 61      |         |         |            |       |       |       | 30    | 5     |      |       |       |       |      | 30-60 |      |       |     |       |      |      |      |      |
|   | 100     |         | *       |            |       |       |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | 7       |         |         | 0-20       | 25-30 |       |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | 10      |         |         | 10-15      | 20-25 | 25-30 | 30-35 | 07    | 35-40 |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | v.      | *       |         |            |       |       |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
| Gross                                       | 41      |         | 5-10    | 10-15      | 15-20 | 20-25 | 7-07  | 25-30 |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | e)      |         |         |            |       |       | *     |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | 71      | *       |         |            |       |       |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
|   | -1      | 4 *     |         |            |       |       |       |       |       |      |       |       |       |      |       |      |       |     |       |      |      |      |      |
| AASHTO<br>Classification                    |         | S 60 -4 | . 60 -2 | <b>.</b> . | m &   | 2     | 7     | 7     | 9     |      | is c  | 2 0   | 6     | 4    | 6, 6  | ا ئى | æ (   |     | xo «  | 7    | , ,  | 9    | .1   |
| 10<br>11f1c                                 | E #     | 1.5     | 2,0     | . 80       | 10.3  | 13.2  | 14.7  | 17.7  | 19.1  | 22.  | 23.5  | 25.0  | 27.9  | 29.4 | 30.9  | 32.3 | 33.8  | 200 | 30.00 | 38.2 | 79.6 | 42.6 | 44.1 |
| AASHTO<br>Class1                            | 2<br>HS | 1 5 7   | 141     | 0 9        | 8     | 6 9   | 2 1   | 12    | 13    | 15   | 16    | 17    | 19    | 20   | 2.1   | 22   | 23    | 47  | 52    | 97   | 78   | 29   | 30   |

1. Refer to Figure E.1 for AASHTO vehicle type description

<sup>2.</sup> HS - single unit trucks

H = combination trucks

<sup>\* -</sup> vehicle class without weight subdivision \* 47



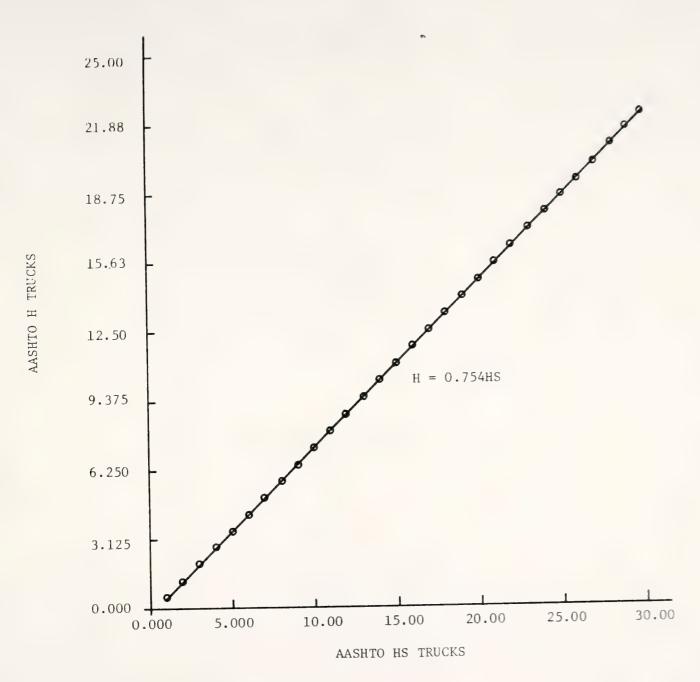


Figure E.2. HS and H Trucks Correlation



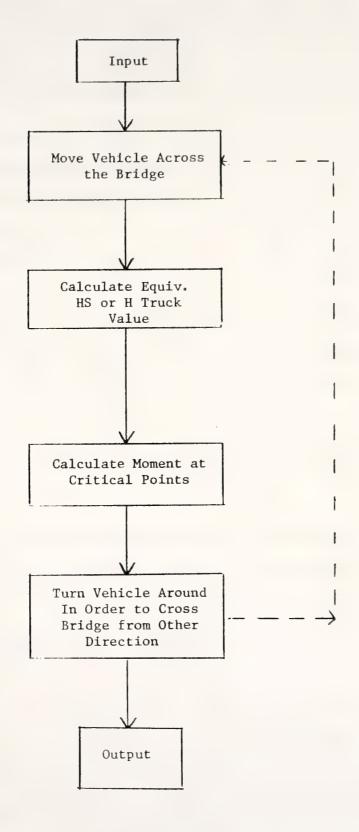


Figure E.3. Flow Chart Illustrating the Data Generation for the Correlation process.



all bridges built in Indiana can be grouped as follows:

- (a) Reinforced Concrete Slab
- (b) Prestressed Concrete I-Beam
- (c) Prestressed Concrete Box-Beam
- (d) Steel Beam
- (e) Steel Girder

For the purpose of incremental cost estimation for each of the bridge types, a combination of the representative method and semi-statistical method was used to develop appropriate cost distribution functions [39]. This approach required selection of representative bridge structures and a detailed incremental analysis was performed. The sample bridges were selected from Indiana Bridge Inventory files.

Table E.3 shows the selected bridges and their characteristics that were considered representative of respective bridge types constructed in the base period.

# Variation of Structure Width with Live Loading

Structure width for different highway categories was selected to be compatible with the width of the approaching highway as specified in AASHTO Manual [1]. The FHWA study [9] assumed a constant width for all classes of vehicle. The Wisconsin study [48] assumed a distinct cut-off point between the basic vehicle and the rest of the design vehicles. In this study, the width of a bridge from curb to curb was proportionally reduced according to



cteristics of Typical Bridges Constructed in the Base Period

| Table E.3 Characteristics of Typical bridges consciucted in the base relied | or iypical brid       | ges constituete | מ דוו רווב חמי      | מס ובדוחת   |
|---|-----------------------|-----------------|---------------------|-------------|
| Bridge Type   | Deck<br>Area (Sq.ft.) | No. of Spans    | Unit Cost (1983 \$) | Design Load |
| Reinforced Concrete Slab  | 3997 •43              | 3               | 33,40               | HS20        |
| Prestressed Box Beam  | 8435.42               | 6               | 36.42               | HS20        |
| Prestressed I-Beam  | 9420.38               | 4               | 36.88               | HS20        |
| Steel Beam  | 9193.75               | 2               | 45.28               | HS20        |
| Steel Girder  | 9441.50               | 2               | 99° 24              | HS20        |



size of design vehicles.

Table E.4 presents the variation of bridge width for different design loadings and for different highway categories. The relationship between design vehicles and observed vehicles as shown in Table E.2 was used to establish the variation of bridge width for different design loadings.

## Distribution Between Highway and Waterway Crossings

Since the cost of substructure of bridges constructed over waterways tend to be more than bridges constructed over highways, a weighing was performed to adjust for this distribution based on data on all bridges built in Indiana within the base period, as shown in Table E.5. Within the base period only a few new or replacement bridges were constructed on local roads. An estimate was therefore made for bridges on local roads on the basis of information from neighboring states.

For highway crossings, the vertical clearance of bridge piers was reduced proportionately of the required vertical clearance of the design vehicle.

This proportionality assumption was found to be reasonable on the basis of actual computations. Vertical clearences associated with design vehicles are 10 ft for H3; 12 ft. for H5 and HS5; and 16 ft. for H10 through HS 20 [48].

### Allocation Factors

Allocation factors were developed for the major structure cost items listed below:

### (a) Superstructure



Table E.4. Bridge Width Under Different Loadings.

|                     |    |    | Bridg | ge Widtl | a (ft.) | by AASH | Bridge Width (ft.) by AASHTO Loading Type | ng Type |      |      |
|---------------------|----|----|-------|----------|---------|---------|---|---------|------|------|
| Highway System      | H3 | H5 | H10   | H15      | Н20     | HS5     | HS10                                      | HS15    | HS20 | HS30 |
| Interstate<br>Rural | 36 | 36 | 07    | 40       | 77      | 36      | 40  | 07      | 77   | 77   |
| Interstate<br>Urban | 38 | 38 | 42    | 42       | 77      | 38      | 42  | 42      | 77   | 77   |
| State<br>Primary    | 34 | 34 | 04    | 40       | 07      | 34      | 07  | 70      | 07   | 07   |
| State<br>Secondary  | 30 | 30 | 34    | 34       | 40      | 30      | 34  | 34      | 07   | 07   |
| County<br>Road      | 28 | 28 | 30    | 30       | 34      | 28      | 30  | 30      | 34   | 34   |
| City<br>Street      | 70 | 07 | 77    | 44       | 8 7     | 05      | 77  | 77      | 87   | 84   |
|                     |    |    |       |          |         |         |   |         |      |      |

1. Refer to Figure E.l for description.



ay Crossings Table E.

| and waterway cross.                                  | Waterway(%)<br>Crossings | 20               | 15               | 50            | 70              | 09    |
|--|--------------------------|------------------|------------------|---------------|-----------------|-------|
| ween Highway   | Highway (%)<br>Crossings | 80               | 85               | 20            | 30              | 40    |
| .5. Distribution Between Highway and Waterway Cross. |                          | Interstate-Rural | Interstate-Urban | State-Primary | State-Secondary | Local |



- (b) Piers, Abutments and Spread Footings
- (c) Piling
- (d) Excavation and Backfill
- (e) Railing
- (f) Drainage Pipes
- (g) Miscellaneous Items

The development of each cost allocation factor was based primarily on the effects of load and width requirements of the design vehicles.

#### Superstructure Cost Factors

The allocation factors for superstructure construction costs were developed through the incremental design method discussed earlier. A series of hypothetical superstructures was designed and cost estimated with various design load increments and design standards specified in the AASHTO Manual [1]. In the design procedure the same materials were included as used in the original design of a sample bridge considered in the base period. The steps taken to obtain the superstructure cost factors were as follows:

- 1. The actual design drawing, plans and bid information for the five representative bridge types shown in Table E.3 were obtained from the Indiana Department of Highways.
- Computer programs were used to determine the following information for each design loading.

Slab Bridge: Negative and positive moments at critical points.



Prestressed I-Beam: Strand pattern at midspan area of steel for main reinforcement.

Prestressed Box-Beam: Strand pattern at midspan area of steel for main reinforcement.

Steel Beam: Beam weight

Steel Girder: Beam weight

There were 10 different design loadings and a total of 50 computer runs were made for 5 bridge types. The original characteristics of these bridges that were independent of the size and weight of design vehicles were retained as much as possible.

- 3. Bids for each sample bridge were analyzed and the unit costs of the three lowest bids were averaged out. Any items that were considered unreasonable were discarded and the engineer's estimate used. It was found that the total cost of superstructure for the sample bridges under full design loading (HS 20) was close to the cost estimated from the computer program used in the study. This was due to the fact that bridge characteristics were kept almost the same as originally built and that there was only a small variation in bid prices. The total cost of superstructure under full design loading calculated was set equal to the total cost of existing superstructure. The ratio of the actual cost and calculated cost was then applied to all subsequent cost estimates associated with different design loadings.
- 4. The unit cost per square foot of deck surface was obtained for each type



of bridge under each design loading. These unit costs were then updated to 1983 dollars using appropriate cost indices. Table E.6 shows the unit cost per square foot for superstructure by design loading and by bridge type.

- 5. The total deck areas constructed for different bridge types and for different highway classes during the base period were obtained from the bridge inventory files of the Indiana Department of Highways and a summary of this information is presented in Table E.7.
- 6. Total deck areas were multiplied by the unit cost to give the superstructure cost factors for each highway class. The resulting factors are presented in Tables E.8 through E.12.
- 7. As mentioned earlier, a semi-statistical approach was used in combination with the representative bridge method to arrive at the allocation functions. A least square analysis was performed on the results of the incremental design analysis. It was found that a parabolic equation of the form,  $a + b \setminus |\overline{x}|$ , where a and b are constants, provided the best fit with a  $r^2 = 0.96 \pm 0.02$ , for all highway classes. Figures E.4 through E.8 present the plots of percent of total superstructure cost versus AASHTO loadings obtained from the regression equations.

#### Substructure Cost Factors

Substructures are structural elements of a bridge that support the superstructure. Typical substructure elements are piers, abutments, piles, and spread footing. An accurate design of piers, piles and other substructure elements in a true incremental context is complicated due to



Table E.6. Bridge Superstructure Unit Costs.

| Unit Cost in Dollars per Sq.Ft of Deck Area by AASHIU Loading 19Pe | HS10 HS15 HS20 HS30 | 14.27 17.44 18.73 19.92 16.41 18.61 19.90 21.17 23.03 | 17.07 18.25 19.45 20.48 17.87 19.30 20.63 22.31 25.02 | 15.53 16.63 17.71 18.62 16.19 17.59 18.75 19.94 22.10 | 15.71 17.36 20.19 22.91 26.31 19.37 23.16 26.48 29.81 32.73 | 19.97 23.22 26.34 30.26 22.85 26.64 30.45 34.29 37.64 |
|--|---------------------|---|---|---|---|---|
|  | HS10                | 18.61   | 19,30   | 17 •59  | 23.16   | 26.64   |
| 200  | HS5                 | 16.41   | 17.87   | 16.19   | 19.37   | 22.85   |
| 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                            | H10 H15 H20 HS5     | 19.92   | 20.48   | 18.62   | 26.31   | 30.26   |
| ho Tod   | H15                 | 18.73   | 19.45   | 17.71   | 22.91   | 26.34   |
| 3  | H10                 | 17.44   | 18.25   | 16.63   | 20.19   | 23.22   |
| 108C TII   | H5                  | 14.27   | 17.07   |   | 17.36   |   |
| 7 7110   | H3                  | 12.19   | 16.03   | 14.78   | 15.71   | 18.07   |
|  | Bridge Type         | Slab  | Box Beam  | I-Beam  | Steel Beam  | Steel<br>Girder                                       |

1. Refer to Figure E.l for description.



Table E.7. Bridge Deck Area

Total Deck Area [Sq.Ft] Constructed in 1980-1983

|                        | Local               | 10967.50 | *        | 2412.00   | *          | *               |
|------------------------|---------------------|----------|----------|-----------|------------|-----------------|
| ation                  | State               | 97795.40 | 4146.90  | 126291.80 | 72970.90   | 91637.50        |
| Highway Classification | State<br>Primary    | 97723.60 | 18566.50 | 188871.30 | 133766.20  | 171835.50       |
| High                   | Interstate<br>Rural | *        | *        | *         | 29702.4    | *               |
|                        | Interstate<br>Urban | *        | *        | 14464 .80 | 17606.30   | *               |
|                        | Bridge<br>Type      | SLAB     | BOX BEAM | I-BEAM    | STEEL BEAM | STEEL<br>GIRDER |

\* No bridge of this type constructed within the base period.



Table E.8. Superstructure Cost Factors for Interstate Rural Bridges

|                       |        |        |        | Cost in Do | llars by A | Cost in Dollars by AASHTO Vehicle Type | le Type |        |        |        |
|-----------------------|--------|--------|--------|------------|------------|--|---------|--------|--------|--------|
| Bridge Type           | H3     | H5     | HS5    | H10        | HS10       | н15 н20                                | HS15    | HS20   | HS30   |        |
| Continuous Steel Beam | 466624 | 515633 | 590186 | 599691     | 680482     | 687907                                 | 781470  | 786519 | 885429 | 972160 |
| Percent of Total Cost | 52     | 58     | 99     | 19         | . 76       | 77                                     | 88      | 88     | 100    | 110    |

1. Refer to Figure E.1 for description.



Table E.9. Superstructure Cost Factors for Interstate Urban Bridges

|                       |        |        |        | Cost in dollars by AASHTO Loading Type | llars by A | ASHTO Load | l<br>ing Type |        |        |        |
|-----------------------|--------|--------|--------|--|------------|------------|---------------|--------|--------|--------|
| Bridge Type           | H3     | H5     | HS5    | H10                                    | HS10       | H15        | H20           | HS15   | HS20   | HS30   |
| Prestressed I Beam    | 213789 | 224638 | 234185 | 240549                                 | 256171     | 254435     | 269334        | 271215 | 286981 | 319672 |
| Continuous Steel Beam | 276595 | 305645 | 349837 | 355471                                 | 403360     | 407761     | 463221        | 466214 | 524843 | 576254 |
| Total                 | 490384 | 530283 | 584022 | 596020                                 | 659531     | 662196     | 732555        | 737429 | 811824 | 895926 |
| Percent of Total Cost | 09     | 65     | 72     | 73                                     | 81         | 81         | 06            | 06     | 100    | 110    |

1. Reference to Figure E.1 for description.



Table E.10. Superstructure Cost Factors for State Primary Highway Bridges

|                          |         |          | Cos      | st in Dolla | ars by AAS | Cost in Dollars by AASHTO Loading Type | g Type   |          |          |          |
|--------------------------|---------|----------|----------|-------------|------------|--|----------|----------|----------|----------|
| Bridge Type              | H3      | HS       | HSS      | H10         | HS10       | H15                                    | H20      | HS15     | HS20     | HS30     |
| Prestressed I-Beam       | 1191250 | 1394515  | 1603644  | 1704299     | 1818636    | 1830363                                | 1876293  | 1944699  | 2068808  | 2250574  |
| Reinforced Concrete Slab | 297620  | 316930   | 331783   | 338839      | 358333     | 361118                                 | 380241   | 383027   | 414218   | 464534   |
| Prestressed Box-Beam     | 2791517 | 2933171  | 3057826  | 3140929     | 3322246    | 3344911                                | 3516784  | 3542128  | 3987570  | 4378167  |
| Continuous Steel Beam    | 2101467 | 2322181  | 2657934  | 2700739     | 3064584    | 3098025                                | 3519388  | 3542128  | 3987570  | 4378167  |
| Continuous Steel Girder  | 3105067 | 3431554  | 3926441  | 3990050     | 4526147    | 4577697                                | 5199742  | 5232390  | 5892239  | 6467888  |
| Total                    | 9486921 | 10398351 | 11577628 | 11874826    | 13089946   | 13212114                               | 14492448 | 14643581 | 16110042 | 17939330 |
| Percent of total Cost    | 58      | 79       | 1.7      | 74          | 81         | 82                                     | 06       | 06       | 100      | 110      |

1. Refer to Figure E.1 for description.



· Table E.11. Superstructure Cost Factors for State Secondary Bridges

|                          |         |         |         | Cost in do | llars by A | Cost in dollars by AASHTO Loading Type | ling Type |         |         |          |
|--------------------------|---------|---------|---------|------------|------------|--|-----------|---------|---------|----------|
| Bridge Type              | H3      | H5      | HS5     | H10        | HS10       | H15                                    | H20       | HS15    | HS20    | HS30     |
| Prestressed I-Beam       | 1192125 | 1395540 | 1604822 | 1705551    | 1819972    | 1831708                                | 1946128   | 1948084 | 2070328 | 2252228  |
| Reinforced Concrete Slab | 92499   | 70788   | 74105   | 75680      | 80035      | 80657                                  | 84928     | 85550   | 92517   | 103755   |
| Prestressed Box-Beam     | 1866592 | 1961311 | 2044664 | 2100232    | 2221473    | 2236628                                | 2351553   | 2367971 | 2505629 | 2791049  |
| Continuous Steel Beam    | 1146372 | 1266774 | 1449932 | 1473282    | 1671763    | 1690006                                | 1919864   | 1932269 | 2175263 | 2388337  |
| Continuous Steel Grider  | 1655889 | 1830000 | 2093916 | 2127822    | 2413731    | 2441223                                | 2772950   | 2790361 | 3142249 | 3449236  |
| Total                    | 5927452 | 6524413 | 7267439 | 7482567    | 8206974    | 8280222                                | 9075423   | 9124231 | 9985982 | 10984605 |
| Percent of Total Cost    | 89      | 9       | 73      | 14         | 82         | 83                                     | 91        | 91      | 100     | 110      |

1. Refer to Pigure E.l for description.



Table E.12. Superstructure Cost Factors for Local Road Bridges

|                          |        |        | S      | Cost in dollars by AASHTO Loading Type | lars by AA | SHTO Loadi | ng Type |        |        |        |
|--------------------------|--------|--------|--------|--|------------|------------|---------|--------|--------|--------|
| Bridge Type              | H3     | 35     | HS5    | H10                                    | HS10       | H15        | H20     | HS15   | HS20   | HS30   |
| Prestressed 1-Beam       | 133693 | 156506 | 179976 | 191273                                 | 204105     | 205421     | 218253  | 218473 | 232182 | 252582 |
| Reinforced Concrete Slab | 35649  | 37458  | 39050  | 40111                                  | 42427      | 42716      | 44911   | 45225  | 47854  | 53305  |
| Total                    | 169342 | 193964 | 219026 | 231384                                 | 246532     | 248137     | 263164  | 263698 | 280036 | 305887 |
| Percent of Total Cost    | 09     | 69     | 78     | 83                                     | 88         | 88         | 96      | 76     | 100    | 110    |
|                          |        |        |        |  |            |            |         |        |        |        |

1. Refer to Figure E.1 for description.



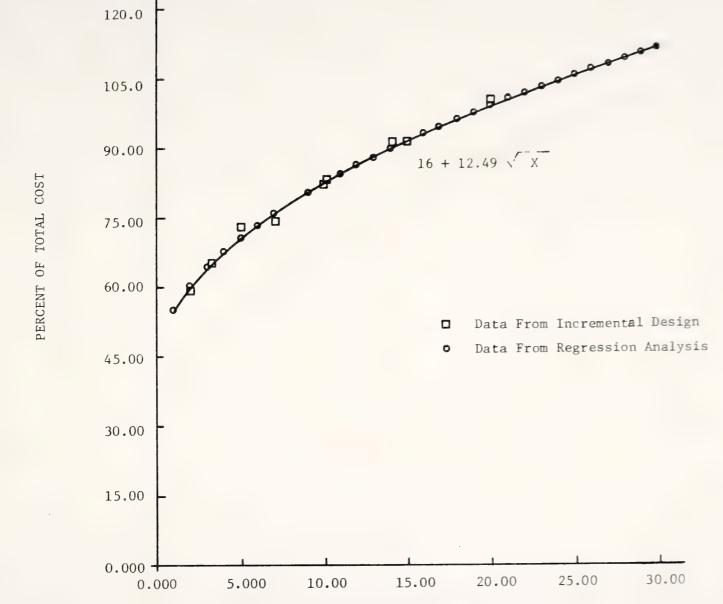


Figure E.4. Percent of Total Superstructure Cost vs. AASHTO HS Loading for Interstate Urban Bridges

AASHTO HS LOADING



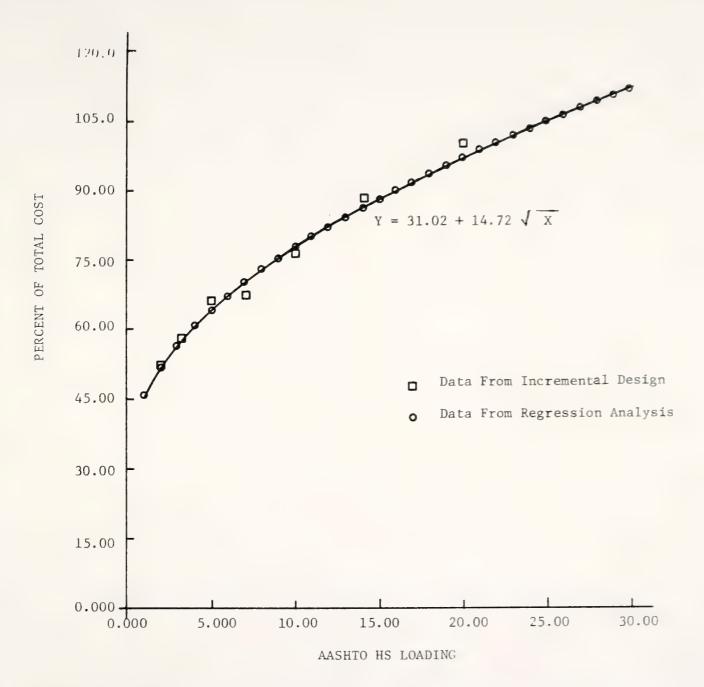


Figure E.5. Percent of Total Superstructure Cost vs. AASHTO HS Loading for Interstate Rural Bridges



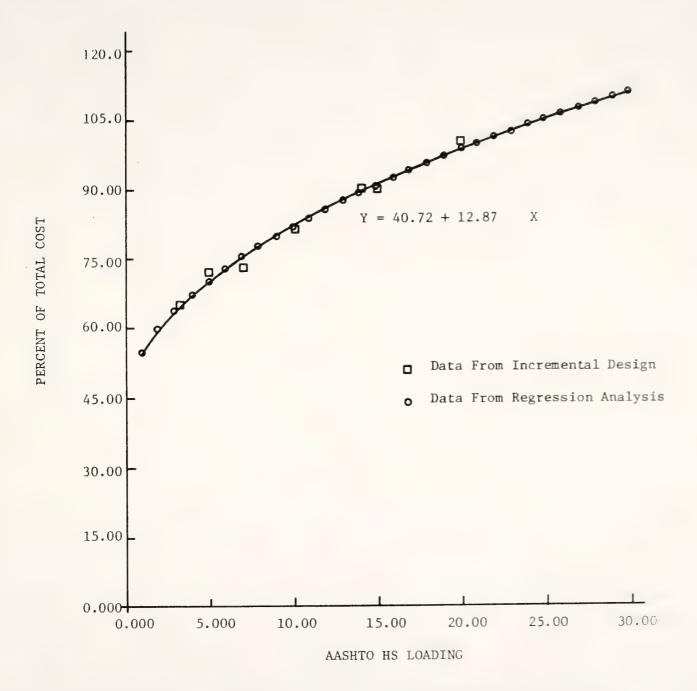


Figure E.6. Percent of Total Superstructure Cost vs. AASHTO HS Loading for State Primary Bridges



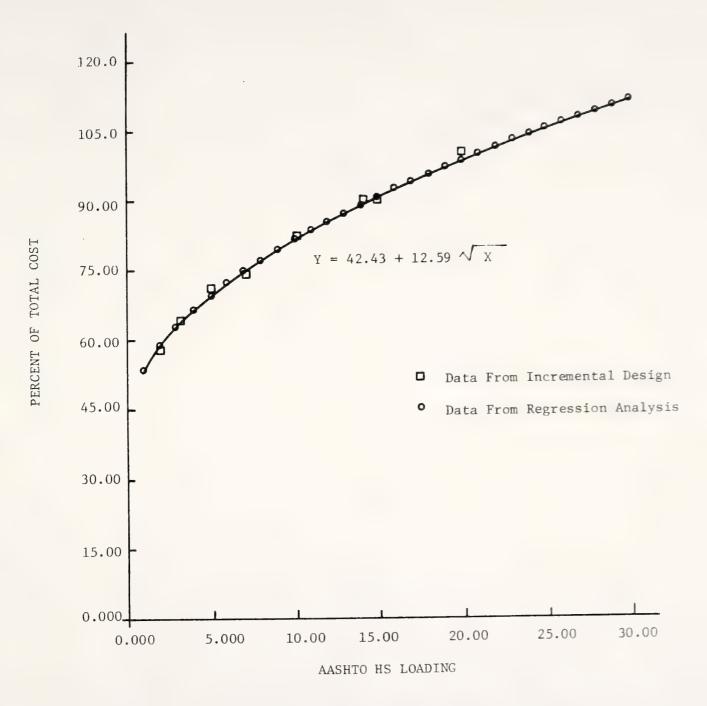


Figure E.7. Percent of Total Superstructure Cost vs. AASHTO HS Loading for State Secondary Bridges



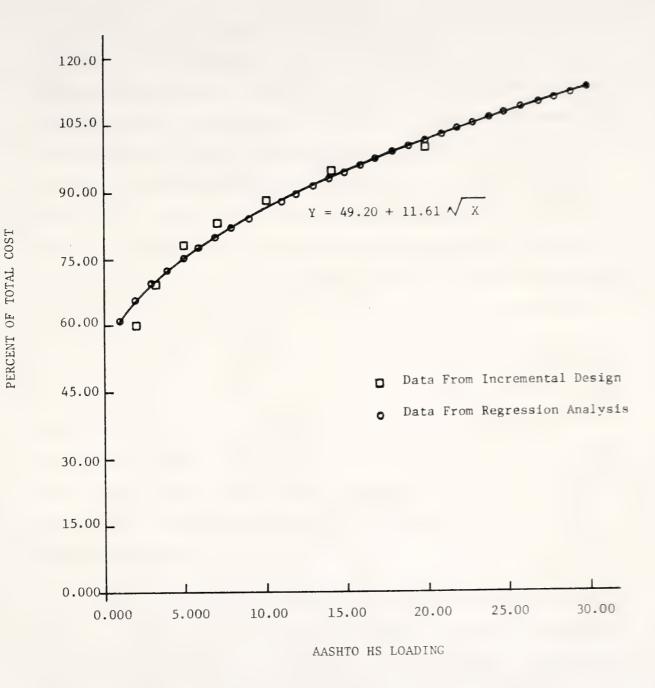


Figure E.8. Percent of Total Superstructure Cost vs. AASHTO ES Loading for Bridges on Local Roads



the effect of other loadings such as ice, thermal stream flow, wind and so on [42]. These loadings affect the design almost independently of vehicle characteristics. Furthermore, the effect of these non-traffic loadings on bridge substructure is difficult to identify. It should also be noted that soil condition and loading capacity of the soil greatly influence the substructure design. Consequently, as in the 1982 FHWA cost allocation study [9], the soil mechanical properties of the sample bridge and hypothetical bridges designed on an incremental basis were assumed to be identical and the loading capacity of the soil was assumed to vary linearly and therefore, proportional to the load placed upon it.

The 1982 FHWA study [9] designed piles based on the assumption that pile length is proportional to the applied load. Thus, pile length was reduced proportionally as the loading was reduced. The piers for the hypothetical bridges were assumed to have the same general configuration as the sample bridge. The stem of the pier and of abutment was varied according to the road width variation. The wing wall and width were maintained constant.

In the present study, individual cost responsibility factors were obtained for piles, piers and abutments. Other components of substructure, such as pile cap, were assumed to be non-attributable cost. The pile length was assumed directly proportional to the applied load. It was found that 75% of the total applied load was dead load and 25% was due to the live load. Hence, 75% of the cost was assumed to be non-attributable cost and the remaining 25% was distributed according to the live load. The cost responsibility factors for piles are shown in Table E.13. The stem of pier and abutment was varied according to the road



Table E.13. Pilling Cost Factors.

|                      | HS30 | 108        | .750                          | .375  | 1.125                                |
|----------------------|------|------------|-------------------------------|---|--------------------------------------|
|                      | HS20 | 72         | .750                          | .25   | .8129 .854 .875 .888 .937 1.00 1.125 |
|                      | HS15 | 54         | .750 .750 .750 .750 .750 .750 | .187  | .937                                 |
| AASHTO Loading Types | H20  | 07         | •750                          | .0207 .0345 .0623 .0629 .104 .125 .139 .187 | .888                                 |
|                      | HS10 | 36         | •750                          | .125  | .875                                 |
|                      | H15  | 30         | .750                          | .104  | .854                                 |
|                      | H10  | 20         | .750                          | .0629                                       | .8129                                |
|                      | HS5  | 18         | .750                          | .0623                                       | .7707 .7845 .8123                    |
|                      | H5   | 10 18      | .750                          | .0345                                       | .7845                                |
|                      | H3   | 9          | .750                          | .0207                                       | .7707                                |
|                      |      | GVW (KIPS) | 75% Common<br>Factor          | 25 % of GVW<br>Factor                       | Piling Cost<br>Factor                |



width variation. The cost responsibility factors for pier and abutment are shown in Table E.14.

## Excavation and Backfill Factors

The FHWA study [9] proportioned the cost of backfill and excavation according to the deck width. The smaller the width of the bridge, the lesser the amount of backfill and excavation. The same procedure was used in the present study and therefore the factors are the same as in the case of pier and abutment.

# Drainage Pipe Factors

Although most of the previous cost allocation studies assumed the cost of drainage pipes to be non-attributable cost, it can be argued that the size of drainage pipes is related to the quantity of runoff which in turn is related to the width of the deck surface. As the deck width can be related to vehicle width, drainage pipe can be considered to be an attributable cost. The same approach as that taken for pier and abutment can be applied here and therefore the drainage pipe cost factors are the same as in the case of pier and abutment.

## Railing Factors

According to AASHTO specification [3], the minimum railing height is 2'-3". Railing members are designed for a moment due to concentrated loads at the center of the panel and at the posts of the railing for PL/6 where P is the concentrated load and L is the post spacing. The common



Table E.14. Piers and Abutment Cost Factors

|                     |     |     | Cost | t Facto | rs by A | ASHTO Lo | Factors by AASHTO Loading Type | ype  |      |      |
|---------------------|-----|-----|------|---------|---------|----------|--------------------------------|------|------|------|
| Highway System      | 띰   | H5  | H10  | H15     | Н20     | HS5      | HS10                           | HS15 | HS20 | HS30 |
| Interstate<br>Rural | .82 | .82 | 06.  | 06.     | 1.0     | .82      | 06*                            | 06.  | 1.0  | 1.0  |
| Interstate<br>Urban | .86 | 98* | .95  | .95     | 1.0     | 98.      | .95                            | .95  | 1.0  | 1.0  |
| State<br>Primary    | .85 | .85 | 1.0  | 1.0     | 1.0     | \$85     | . 82                           | 1.0  | 1.0  | 1.0  |
| State<br>Secondary  | .75 | •75 | .85  | .85     | 1.0     | .75      | . 85                           | .85  | 1.0  | 1.0  |
| County<br>Road      | .82 | .82 | 88   | 88      | . 1.0   | .82      | 88                             | 88   | 1.0  | 1.0  |
| City<br>Street      | .83 | 83  | .92  | .92     | 1.0     | .92      | .92                            | .92  | 1.0  | 1.0  |



cost portion was determined by using the cost related to the smallest vehicle loading in the formula. This portion was found to be 25% of the total railing cost. The remaining 75% was distributed according to the gross vehicle weight. The cost responsibility factors for railing are shown in Table E.15.

## Miscellaneous Items

Miscellaneous items consist of those costs that are independent of vehicle size or weight and they include such items as engineering services, installation of traffic control devices, landscaping, and so on. These costs were thus considered to be non-attributable and distributed among all vehicles as common costs in proportion of their respective vehicle-miles of travel.

# Allocation of Cost-Responsibilities

Appropriate cost factors were developed for each of the structural cost components, and these cost factors were expressed in terms of AASHTO vehicle types. The next step was to combine these cost items and relate them to the appropriate respective vehicle classes considered in the present study. The steps involved in this procedure are listed below:

- 1. The VMT of each of the AASHTO vehicle types was obtained by using the correspondence matrix for matching AASHTO vehicle types with study vehicle classes shown in Table E.2.
- The common portion of the total cost was distributed among all AASHTO vehicles according to VMT.



Table E.15. Railing Cost Factors.

|                        |       |         | AAS  | AASHTO Loading Types | ding Ty      | /pes     |      |  |           |       |
|------------------------|-------|---------|------|----------------------|--------------|----------|------|--|-----------|-------|
|                        | H3    | HS HS5  | HS5  | H10                  | H10 H15 HS10 | HS10     | H20  | HS15   | HS15 HS20 | H830  |
| 3VW (KIPS)             | 9     | 6 10 18 | 18   | 20                   | 30           | 30 36 40 | 70   | 54   | 72        | 108   |
| 25% Common<br>Factor   | .250  | .250    | .250 | .250                 | .250         | .250     | .250 | .250 .250 .250 .250 .250 .250 .250 .250            | .250      | .250  |
| 75 % OF GVW<br>Factor  | .0623 | .103    | .186 | .207                 | .312         | .372     | .415 | .0623 .103 .186 .207 .312 .372 .415 .561 .75       | .75       | 1.125 |
| Railing Cost<br>Factor |       | .353    | .463 | .457                 | .562         | .622     | •665 | .312 .353 .463 .457 .562 .622 .665 .811 1.00 1.375 | 1.00      | 1.375 |



- Subsequent incremental costs were then allocated to appropriate AASHTO vehicle types.
- 4. The total allocated costs for each of the AASHTO vehicle types were assigned to the study vehicle classes using the correspondance matrix established in Table E.2.

## New Bridge Construction

If a bridge was constructed during the base period specifically on a new alignment, it was taken to be a new construction. All new construction costs within the base period were analyzed in terms of cost items and grouped into different highway classes. Table E.16 shows the percent distribution of new structure construction costs by cost item and by highway class.

# Bridge Replacement

Bridges are replaced due to the deficiencies of the original structures. Consequently, the FHWA study [9] treated bridge replacement costs differently from new bridge costs. A structural sufficiency rating was used to determine the relative contribution of each factors which were responsible. Costs were assigned to vehicles based on the sufficiency rating components. Deficiencies in original structures may include low load carrying capacity, inadequate lane width, fatigue worn components, and inadequate overhead clearances. However, the federal study simplified the allocation procedure by considering only load-deficiency related replacements. It further assumed that losses or inadequacies in load-bearing capacity are entirely attributable to heavy vehicle use. Because of the difficulty of determining age and environmental factors on load bearing capacity, it was decided in the present study to use the



Table E. 16. Percent Distribution of New Bridge Construction Cost by Cost Item and by Highway Class

|                         | Interstate<br>(Rural & Urban) | State<br>Primary | State<br>Secondary | Local<br>Roads |
|-------------------------|-------------------------------|------------------|--------------------|----------------|
| Superstructure          | 14%                           | 17%              | 26%                | 25.06          |
| Substructure            |                               |                  |                    |                |
| Piers and Abutm         | ents 1.9%                     | 8%               | 6.4%               | 6.29           |
| Piling                  | 0.3%                          | 1.8%             | 2.9%               | 2.87           |
| Excavation and Backfill | 0.7%                          | 6.6%             | 6.6%               | 9.43           |
| Drainage                | 0.02%                         | 0.01%            | 0.02%              | 0.05           |
| Railing                 | 0.41%                         | 0.46%            | 5.8%               | 5.59           |
| Miscellaneous           | 79%                           | 64%              | 48%                | 50.71          |
| Total                   | 100%                          | 100%             | 100%               | 100%           |



same approach as used in the new construction but with different distribution of cost components. A replacement project would not involve much excavation work, but it will require removal of the existing structure.

The percent distribution of component costs for replacement project was determined by analyzing the itemized cost files from the IDOH. The resulting cost distribution by cost item and by highway class is presented in Table E.17.

# Bridge Rehabilitation Cost

Bridge rehabilitation costs included cost of widening, deck repair and partial replacement of structural components. Bridge rehabilitation costs are different from bridge maintenance costs, because rehabitation work is not done routinely and it is normally more expensive than routine maintenance.

Many studies combined the rehabilitation costs with replacement costs. Other studies assumed rehabilitation costs to be common costs. In this study, the cost responsibility factors for bridge rehabilitation project were developed using the same approach as the new construction, but with different distribution of cost components. The cost distribution by cost item and by highway class is shown in Table E.18. It may be noted that a large percent of the rehabilitation cost is non-attributable cost.

## Culverts

In the base period, not too many box culverts were built. Most of the box culverts were replaced by metal pipes and structural plates. The size of the pipes is dependent mainly on the drainage requirement of the surrounding



Table E.17. Percent Distribution of Bridge Replacement Cost by Cost Item and by Highway Class

|                       | Interstate<br>(Rural & Urban) | State<br>Primary | State<br>Secondary | Local<br>Roads |
|-----------------------|-------------------------------|------------------|--------------------|----------------|
| Superstructure        | 28.5%                         | 29.5%            | 26.2%              | 27.00%         |
| Substructure          |                               |                  |                    |                |
| Piers & Abutme        | nts 7%                        | 2.6%             | 6.0%               | 5.74%          |
| Piling                | 0.01%                         | 0.6%             | 0.13%              | 1.37%          |
| Excavation & Backfill | 9.88%                         | 19.6%            | 18.6%              | 18.51%         |
| Drainage              | 0.01%                         | 0.10%            | 0.007%             | 0.12%          |
| Railing               | 5.7%                          | 3.2%             | 6.50%              | 6.08%          |
| Miscellaneous         | 48.9%                         | 44.4%            | 42.50%             | 41.18%         |
| Total                 | 100%                          | 100%             | 100%               | 100%           |



Table E.18. Percent Distribution of Bridge Rehabilitation Cost by Cost Item and by Highway Class

| (                | Interstate<br>(Rural & Urban) | State<br>Primary | State<br>Secondary | Local<br>Roads |
|------------------|-------------------------------|------------------|--------------------|----------------|
| Superstructure   | 7.60%                         | 5.72%            | 19.3%              | 14.82%         |
| Substructure     |                               |                  |                    |                |
| Piers & Abutment | cs 0.60%                      | 0.50%            | 1.9%               | 0.79%          |
| Piling           | 0.03%                         | 0.01%            | 0.9%               | 0.20%          |
| Excavation &     |                               | 0 70%            | F                  | 0.55%          |
| Backfill         | 0.10%                         | 2.79%            | 5.5%               | 0.55%          |
| Drainage         | 2.70%                         | 0.008%           | 0.004%             | 0.23%          |
| Railing          | 6.70%                         | 7.70%            | 5.70%              | 6.42%          |
| Miscellaneous    | 82.40%                        | 83.20%           | 66.70%             | 76.99%         |
|                  |                               |                  |                    |                |
| Total            | 100%                          | 100%             | 100%               | 100%           |



areas. Consequently, it was considered a common cost. Box culvert is largely related to the weight of overfill and the weight of overhead roadway slabs. Therefore, all future culvert costs were assigned to all vehicle classes as common cost.

## Sign Bridges

Sign bridges were singled out because their cost responsibility is vehicle-size related. For lighter and thus smaller vehicles, the horizontal and vertical clearances can be reduced appropriately. A typical sign bridge has a vehicle clearance of 18 feet and a span length of 80 feet. The procedure used by the Wisconsin study [48] was followed to allocate sign bridge costs.

For autos (H3) and light trucks (H5), the sign bridge geometry can be reduced as follows:

|        | Н3  | Н5          | HS5 | H10-H20 |
|--------|-----|-------------|-----|---------|
| Column | 11' | 13'         | 15′ | 18′     |
| Span   | 48′ | 68 <b>′</b> | 72" | 80′     |

Responsibility factors for sign bridges are then:

$$H3 \qquad \frac{48 + 11}{80 + 18} = 0.60$$

$$\frac{13 + 68}{80 + 18} = 0.82$$

$$HS5 \qquad \frac{72 + 15}{80 + 18} = 0.88$$



$$H10 - HS20 \qquad \frac{80 + 18}{80 + 18} = 1.00$$



#### APPENDIX F

#### MAINTENANCE COST ALLOCATION

#### General

A particular item of maintenance cost can be classified as a "common" or an "attributable" cost. A common cost is a cost that cannot be specifically allocated to a class or classes of vehicles, and is therefore distributed among all highway users. For example, mowing of grass or the pick up of litter within right-of-way can be considered as common cost. Common costs are to be borne by all users in direct proportion to the number of miles driven by each. Therefore, the common-cost allocator for each vehicle class is the VMT by that class as a percentage of the total VMT by all vehicle classes.

An attributable maintenance cost is a cost that can be directly allocated to a particular class or classes of vehicles. Attributable costs can be allocated on the basis of weight related allocators for those items that can be associated with vehicle weights. Some items can be allocated according to capacity related allocators when vehicle size affects the cost.

#### Previous Studies

Methodologies to allocate maintenance costs used by cost allocation studies by nine states were reviewed for comparison. These nine states are Connecticut, Florida, Maine, Maryland, North Carolina, Oregon, Washington, Wisconsin, and Virginia.

It was found from this comparison that there exists no universal method for the allocation of maintenance costs. This is especially true for the



costs (pavement, shoulders and bridges) that are related to the weight of vehicles. The selection of cost allocators is based on various assumptions and reasonings. A majority of these states used ESAL as the cost allocator of pavement related maintenance costs. It seems however that the use of vehicle-miles of travel (VMT) has been accepted in most of the allocation studies for allocation of the common costs.

# Allocation Methodology

Routine maintenance activities are classified into the following major groups:

- 1. Roadway and shoulder maintenance
- 2. Roadside
- 3. Drainage
- 4. Bridge
- 5. Traffic Control
- 6. Winter and Emergency
- 7. Public Service
- 8. Others

Roadway maintenance consists of activities such as patching, leveling, and sealing of cracks and joints. The associated pavement damages are considered to be caused either by climatic conditions or by the interaction of climate and the weight of vehicles.

For the purpose of allocating roadway maintenance costs due to traffic and its interaction with weather, a procedure was developed in the present study to separate the load-related and non-load-related effects, as discussed later in this section.



In the case of shoulder construction, use of capacity related cost allocators is justified; however, they may not be appropriate for the allocation of shoulder maintenance costs, because shoulder damages are more of a function of weather and traffic. The weather affects shoulder conditions more severely than pavements. Once constructed, functions of highway shoulders are to hold roadway pavement in place and strengthen it. Obviously the heavier trucks would cause more distress than the lighter vehicles. It was decided, therefore, to allocate the traffic-related component of shoulder maintenance costs in proportion to the costs assigned to vehicles for pavement maintenance. In this approach, assumption is made that the probability of using shoulders for emergency stops is equal for all vehicle classes.

All other maintenance costs, except bridge maintenance costs, were allocated as common costs to all vehicle classes because these costs cannot be directly related to the variation in highway use by different vehicle classes.

There are seven items under bridge maintenance of which bridge maintenance contract work can be judged partly to be the result of the interaction of traffic and weather. Consequently, this part of the maintenance cost was allocated using the approach used for pavement related maintenance costs. All other bridge maintenance costs were considered to be common costs.

Some of the activities in the "Other" category include operational overhead such as supervision and equipment repair and maintenance and therefore these operational overhead costs were grouped with administrative overhead.

Administrative and operational overhead costs were allocated to all vehicle classes in proportion to the sum of direct maintenance costs. These costs were first assigned percentwise to the three maintenance costs groups, then,



allocated to vehicle classes by the cost allocator(s) of each cost group.

# Data Base for Analysis

Routine maintenance costs for the state highway system were estimated using the Routine Maintenance Records and Construction Reports. As for cost items, Routine Maintenance Records contain only labor, production units, types and quantities of materials used. Maintenance costs for labor and material were computed by multiplying the labor and material units required for each activity by separately provided unit costs. Fuel consumption data are not found in Routine Maintenance Records, but are reported in lump sum for all maintenance works for each fiscal year. To distribute fuel costs to each activity, results of a previous study [36] concerning the fuel consumption rates of routine maintenance activities was used. Routine maintenance activities that have been done by contract are found in Construction Reports file.

# Procedure for Allocating Pavement Routine Maintenance Costs

The procedure for allocating pavement routine maintenance costs pursues the same concept adopted for allocating pavement rehabilitation costs. The maintenance expenditure items included in the computation of pavement routine maintenance costs are shown in Table F.1.

As explained earlier in the section on allocation of pavement rehabilitation costs, an actual field performance curve of a given pavement would lie between the no-loss line and the zero-maintenance curve. The higher the level of routine maintenance performed, the closer is the field performance curve to the no-loss line.



Table F.1. Pavement Routine Maintenance Activities

| IDOH Code No. | Activity Name                       |
|---------------|-------------------------------------|
| 201           | Shallow patching                    |
| 202           | Deep patching                       |
| 203           | Premix leveling                     |
| 204           | Full width shoulder seal            |
| 205           | Seal coating                        |
| 206           | Seal longitudinal cracks and joints |
| 207           | Sealing cracks                      |
| 209           | Cutting relief joints               |
| 219           | Others                              |



In Appendix H, a technique is described which enables the zeromaintenance curve to be derived by considering pavement performance curves and
their associated routine maintenance expenditure expressed in terms of average
annual routine maintenance expenditure per lane-mile. Also presented in
Appendix H is a proportionality rule by means of which the respective responsibility proportions of load-related and non-load-related effects of pavement
damage can be computed.

Since the effects of non-load-related factors may be different for different regions (northern and southern Indiana), and pavement types (overlay, rigid and flexible pavements), maintenance expenditure data were divided into six region-pavement type groups. In addition, six highway classes were used in the present study and each with a different vehicle composition. This means that 36 routine maintenance expenditure subgroups in total needed to be analysed in the cost-responsibility factor computation.



#### APPENDIX G

#### REVENUE ATTRIBUTION

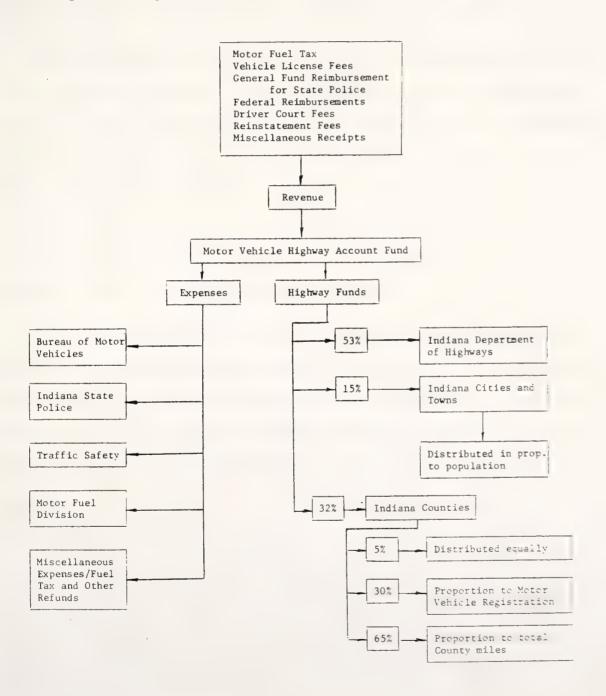
After cost responsibilities are identified it is necessary to examine revenue payment by vehicle class to provide a base for comparison. The apportionment was done of appropriate revenues paid by Indiana highway users to state, federal and local governments. In particular, the user revenues considered are those which went to support highway construction, operation and maintenance activities in Indiana.

# State Highway Revenues

The Indiana system of funding of highway activities includes two major accounts, Motor Vehicle Highway Account (MVHA) and Highway Road and Street Fund (HRSF). The sources of revenue consist primarily of the motor fuel taxes, registration fees, and motor carrier fees. In addition, miscellaneous revenues in the nature of fines and charges are collected and deposited in the Motor Vehicle Highway Account (MVHA). Furthermore, in recent years some user fees and taxes have been imposed by some local governments in the form of local option taxes. In Figure G.l is presented the current organization of the MVHA. The majority of highway revenues in Indiana is gathered in MVHA where fuel taxes and registration fees are the main sources of revenue. The other highway related fund is the Highway Road and Street Fund (HRSF). A part of the motor fuel tax and truck registration fee is gathered in the HRSF for use in two separate accounts, the Primary Highway Fund and the Local Road and Street Fund.



Figure G.1. Organization of the Motor Vehicle Highway Account (MVHA)





The motor fuel taxes are the major sources of highway revenues in Indiana and they consist of three items, motor fuel tax on gasoline, special fuel tax involving primarily diesel fuel, and motor carrier fuel tax imposed on interstate carriers.

## Federal Revenues

Federal funds available to Indiana are generated through Federal Trust

Fund. In 1983 the revenues included motor fuel tax, tax on new trucks and

trailers, parts and accessories tax, tires and tubes tax, tax on lubricating

oil and heavy vehicle use fee. The Surface Transportation Assistance Act of

1982 and its subsequent amendment resulted in several changes in federal tax

structure. For example, taxes on tread rubber, inner tubes, lubricating oil,

and truck parts were eliminated and new tax schedules were introduced for fuel

taxes and taxes on truck sales and heavy vehicle use.

It should be noted that only that portion of the federal revenues that was received by Indiana was considered in revenue analysis. For example, in 1983 the amount received by Indiana was \$155.56 million or about 75% of the revenues contributed by Indiana highway users to the Highway Trust Fund. The STAA of 1982 stipulated the percentage of return to be at least 85%.

#### Attribution of Revenue

Each of the state highway user charges were examined separately to attribute the shares of revenues to vehicle classes. In each case the revenues attributed were equal to the amount available for highway purposes. For example, the disbursements to the Bureau of Motor Vehicles from the Motor Vehicle



Highway Account were considered to be associated with the collection of state registration fees and were thus deducted from the gross amount. Similarly, the disbursements to the Motor Fuels Tax Division of the Department of Revenue were deducted from the total fuel taxes collected. However, these expenses of collecting and administering these taxes were not included in cost computation.

#### State Fuel Taxes

In FY83 total state fuel taxes collected in Indiana consisted of gasoline tax, special fuel tax (diesel) and motor carrier fuel use tax; and the total amount available for MVHA, HRSF and regular distribution was \$314.248 million with 81% from gasoline tax, 17% from special fuel tax and 2% from motor carrier fuel use tax. Considering the gasoline tax refunds and disbursements for the Motor Fuel Tax Division and other associated expenses, the net amount available for highway activities was \$305.175 million. This amount was shared by the IDOH, counties, cities, and the State Police. The corresponding amount for the biennial period of 1985-86 would be \$614 million.

Fuel taxes are dependent upon fuel consumption which in turn is related to vehicle-miles of travel and vehicle fuel efficiency. The VMT values by vehicle class for 1983 were available from the traffic count data. Fuel efficiency estimates by vehicle class for both 1983 and 1985-86 were generated by combining the figures from the FHWA Cost Allocation Study [9] with the findings of an earlier study performed for the IDOH [29]. To compute fuel consumption, annual VMT for a specific vehicle class was divided by its fuel efficiency value. Gallons of fuel consumed was then multiplied by the appropriate tax rate. It should be pointed out that percentage of vehicles powered by gasoline and diesel were estimated from the information available



in the National Truck Characteristics Report [23]. For example, 11.94% of 2-axle single-unit trucks was estimated to contain diesel engines, while 99.35% of combination trucks with 5 or more axles would have diesel engines. These estimates were made by vehicle type and by number of axles. Furthermore, while gasoline and special fuel taxes were attributed among all vehicle classes, motor carrier fuel use tax was distributed only among trucks with more than 2-axles.

The same procedure was used to attribute the state fuel tax revenues for the 1985-86 period on the basis of the estimated VMT and fuel efficiency rates for these years. The 1985-86 VMT projections were developed using the factors developed in connection with the Federal Cost-Allocation Study and factors used in the studies conducted by several midwestern states.

## State Registration Fees

A flat vehicle registration fee is charged to private automobiles in Indiana, while the fees schedules for commercial vehicles are graduated by registered weight. The total motor vehicle registration fees available for highway related activities in Indiana in FY83 were \$109.7 million, after deducting disbursements for the Bureau of Motor Vehicles, miscellaneous expenses and the amounts associated with dealer's fees, transfer fees and other fees, such as fees for amateur radio. The registration fees for 1985-86 were estimated on the basis of the information provided by the IDOR and the Bureau of Motor Vehicles. The net amount estimated to be available for highway purposes in the two-year period of 1985-86 is \$225.8 million.

Registration fees were attributed directly in proportion of the number of units of each vehicle class and associated registration fee rate. As men-



tioned earlier, a correspondence matrix was used to relate vehicles classified by gross operating weight with registered vehicle weight groups.

#### Other Taxes and Fees

Other taxes and fees at the state level were \$2.502 million in 1983 or about 0.4% of the total available revenues. The majority of these fees came from oversize and overweight permits. The rest of these fees came from vehicle identification stamp fees, reciprocity fees and others. These fees were distributed among commercial vehicles in proportion to number of units. In 1985-86 miscellaneous state fees are estimated to be \$5.35 million and the attribution would follow the same procedure as in 1983.

Local option taxes in 1983 amounted to \$1.058 million or about 0.2% of the total. In 1985-86, the estimated amount is \$5.5 million. Local option taxes are levied by counties and consist of an excise tax imposed on all motor vehicles and a wheel tax imposed on motor vehicles that are not subject to an excise tax. The attribution of these taxes was done by distributing the amount in proportion of registered units of all motor vehicles.

## Federal Taxes

All federal taxes were attributed according to the appropriate user charge schedules. The applicability of each type of tax or fee along with the effective date of implementation of each tax or fee type was considered for appropriate vehicle classes. The factor for distributing 1983 taxes on oil, tire, tubes, tread rubber and truck parts were obtained from the report [35] prepared for the Federal Highway Cost-Allocation Study. The 1983 factors were developed by interpolating the 1977 and 1985 factors given in the report. The rate of new truck sales and associated prices were also generated using the



information given in the report [35]. Heavy vehicle use fee was attributed in proportion of number of units in each commercial vehicle class of concern.

The rates and effective dates were carfully considered in estimating the amount of this fee.



#### APPENDIX H

Non-Load-Related Costs in Pavement Rehabilitation and Maintenance

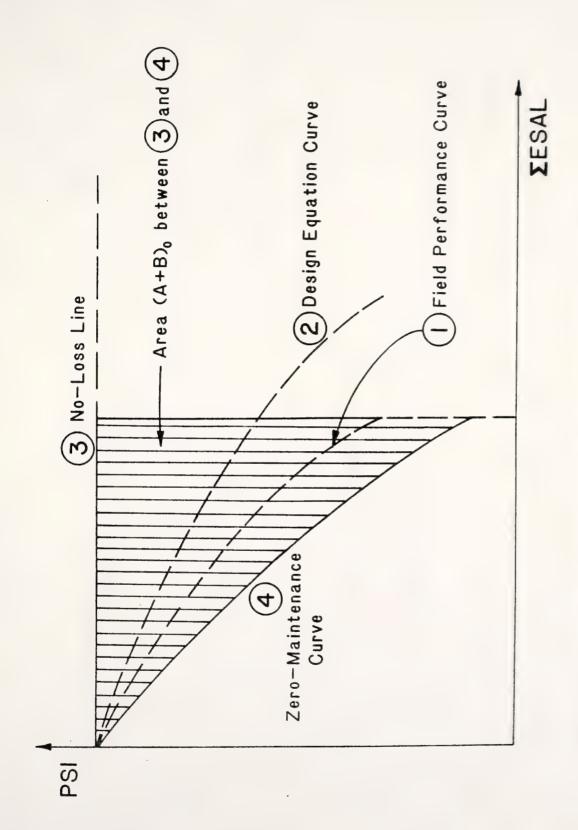
Cost Allocation

The procedure discussed herein follows a performance-based approach developed by Fwa and Sinha [13]. A summary of this approach is presented in this Appendix.

As discussed in the section on allocation procedure of pavement rehabilitation costs, pavement wear or damage may be represented by appropriate areas in a pavement performance (PSI vs.  $\Sigma$ ESAL) plot. In Figure H.l, the shaded area (A + B) between curves 3 and 4 represent the total pavement damage of a given stretch of pavement. Curve 3 is a hypothetical no-loss line and curve 4 is a hypothetical performance curve for the pavement concerned in a situation where no maintenance at all has been carried out.

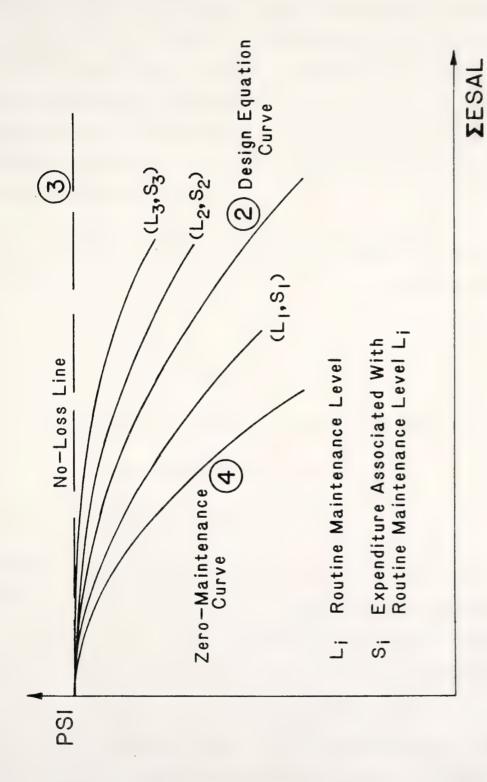
Consider a stretch of pavement which is maintained by a particular highway agency with known technology, facilities, and manpower, and assume that the efficiency of the working crew remain the same for the period of analysis. Under these conditions it is reasonable to say that the expenditure spent on maintaining the pavement would be positively related to the level of routine maintenance performed. That is, in terms of constant dollars higher expenditure is likely to be associated with higher levels of maintenance. In Figure H.2, one would expect the expenditure level  $S_3$  to be greater than  $S_2$ ,  $S_2$  greater than  $S_1$ , and so on.



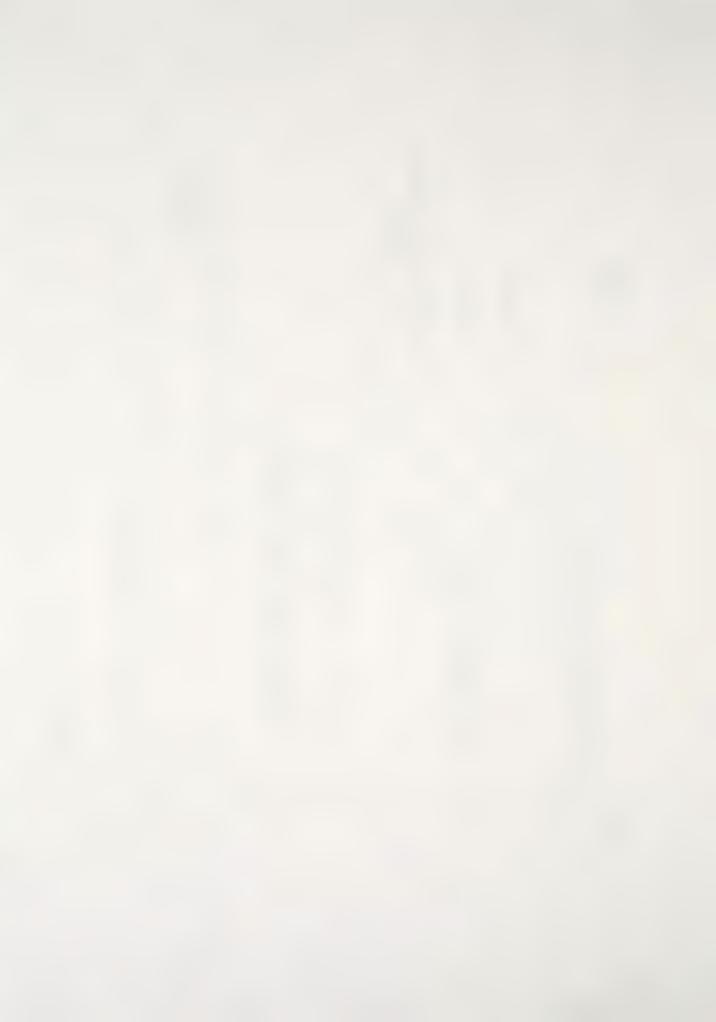


Total Pavement Damage as Defined by Zero-Maintenance Pavement Performance Curve Figure H.1.





Schematic Diagram Showing Pavement Performance Curves with their Associated Routine Expenditures. Figure H. 2.



Performance curves based on Indiana design equations vary with the following factors: type of pavement, region, terminal PSI, materials and traffic. Indiana material and regional factors estimated in an earlier work done at Purdue University [6] were used for this purpose. Cost-allocation analyses would be performed by highway class and type of pavement. For each pavement section on which a rehabilitation had been performed during the base period, performance curves corresponding to Indiana design equations and actual field performance were developed.

The Road-Life Records of the Indiana Department of Highways contain the following information for each route of the State Highway system:

- 1. Pavement type
- 2. Pavement thickness
- 3. Pavement age since the time of major improvement
- 4. Layer material characteristics, and
- Construction costs

Pavement roughness measurements on Indiana State Highways since 1979 are available from JHRP tapes at Purdue University. These roughness measurements can be related to PSI by using relationships established for Indiana in previous studies performed at Purdue University [30,31]. The relationships derived for different types of pavements are summarized in Table H.1.

For a given pavement, knowing a PSI value and the corresponding cumulative ESAL, a point on the actual performance curve of the pavement is obtained. This procedure may be repeated for other points of time at which



Table H.I. Relationship Between Present Serviceability Index (PSI) and Roughness Number (RN)

| Pavement                               | Relationship             |
|--|--------------------------|
| Asphalt                                | PSI = 3.94 - 0.00072(RN) |
| Overlay                                | PSI = 4.37 - 0.00174(RN) |
| Jointed Reinforced Concrete (JRC)      | PSI = 4.69 - 0.00141(RN) |
| Continuously Reinforced Concrete (CRC) | PSI = 4.40 - 0.00070(RN) |
| JRC & CRC (combined)                   | PSI = 4.58 - 0.00114(RN) |



data are available. Field performance curve of the pavement may then be plotted, and the area between this curve and the no-loss line, ie. area (A+B), may be computed.

The annual routine maintenance cost per lane-mile of a pavement section was obtained by dividing its annual routine maintenance expenditures by its total lane-miles. The annual routine maintenance expenditures over the base period were considered to compute the average maintenance cost for the highway section under consideration.

Routine maintenance information is documented by highway section which is defined as the portion of a highway that lies within the boundaries of a county. Highway section was therefore chosen as the basic unit of analysis in the present study. When a pavement section contains more than one roughness measurement, a weighted average of area (A+B) was calculated using the lanemile of each roughness measurement as the weighting factor.

For a stretch of pavement with more than one highway section, the zero-maintenance curve of the pavement was derived by plotting the areas (A+B) of these highway sections against their respective average annual routine maintenance expenditure per lane-mile. A least square line was then fitted to the data points. The intercept of this line with the (A+B) axis gives area (A+B) of the zero-maintenance curve of the pavement under consideration.

The next step involves the computation of load-related and non-load-related responsibility factors using proportionality assumption. Figure H.3 assumes that the interaction effects is composed of two components, namely the load-related and non-load-related parts. Proportion a is equal to  $\frac{A}{(A+B)_0}$  which could be computed for a given stretch of pavement with the procedure



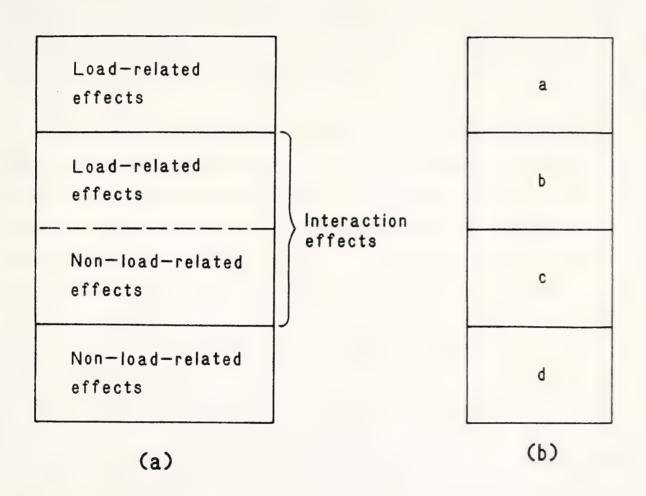


Figure H.3. Schematic Diagram Showing Load-related and Non-load-related Effects Responsible for Pavement Damage



described in preceding paragraphs.

Knowing proportion a, it is possible to calculate proportions b, c and d by making the following proportionality assumption:

$$\frac{b}{b+c+d} = \frac{a}{a+b+c+d} \tag{H.1}$$

$$\frac{c}{a+b+c} = \frac{d}{a+b+c+d}$$
 (H.2)

Equation (H.1) assumes that for a given 'pure' load-related effects (proportion a), the share of load-related effects in the remaining non-load-related and interaction effects is directly proportional to the share of 'pure' load-related effects in the overall effects (a+b+c+d). Similarly, equation (H.2) assumes that for a given 'pure' non-load-related effects (proportion d), the share of non-load-related effects in the remaining load-related and interaction effects is directly proportional to the share of the 'pure' non-load-related effects in the overall effects (a+b+c+d).

Solving for d using equations (H.1) and (H.2), it gives:

$$d = 1 - \sqrt{1 - (1 - a)^2}$$
 (H.3)

Proportions b and c may then be determined from solving equations (H.1) and (H.2). The total responsibility proportion of load-related effects is given by (a+b) and the total responsibility proportion of non-load-related effects by (c+d).

Applying the procedure described in this Appendix to Indiana highways, the resulted proportional responsibilities of load-related and non-load



related factors for different regions and pavement types are summarized in Table H.2.

The regional effect changes gradually from northern to southern Indiana and there exists no distinct boundary between them. For the present cost-allocation study, the two regions were defined as shown in Figure H.4.



Table H.2. Proportional Responsibilities of Load-Related and Non-load-related Factors in Indiana Pavement Rehabilitation and Maintenance Cost Allocation

|                  | Nor                  | tnern indi        | ana     | Sout                 | Southern Indiana |         |  |
|------------------|----------------------|-------------------|---------|----------------------|------------------|---------|--|
| Factor           | Flexible<br>Pavement | Rigid<br>Pavement | Overlay | Flexible<br>Pavement | -                | Overlay |  |
| Load-Related     | 0.87                 | 0.66              | 0.80    | 0.98                 | 0.70             | 0.98    |  |
| Non-Load-Related | 0.13                 | 0.34              | 0.20    | 0.02                 | 0.30             | 0.02    |  |



NORTHERN REGION SOUTHERN REGION

Figure H.4. Northern and Southern Regions for Pavement ost-Allocation



# APPENDIX I

#### TABLES OF COST-RESPONSIBILITY FACTORS



Table I.1. Pavement Construction Cost-Responsibility Factors

# (a) Pavement Construction Cost-Resp.(%) for 1983

| Vehicle<br>Class  | Int.<br>Rural  | Int.<br>Urban  | State<br>Primary   | State<br>Second.  | County<br>Roads  | City<br>Streets  |
|---|--|--|--|---|--|--|
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13 | 8.667<br>27.239<br>2.057<br>0.269<br>0.657<br>0.411<br>0.459<br>0.036<br>0.226<br>0.066<br>3.619<br>54.202<br>1.857<br>0.233 | 11.869<br>36.848<br>2.806<br>0.376<br>0.537<br>0.607<br>0.577<br>0.192<br>0.179<br>0.042<br>2.117<br>41.641<br>2.048 | 11.564<br>40.652<br>3.919<br>0.189<br>0.340<br>1.640<br>1.392<br>0.142<br>1.484<br>0.091<br>1.122<br>36.157<br>0.772 | 5.560<br>22.174<br>4.919<br>0.211<br>0.176<br>1.876<br>2.120<br>0.088<br>0.603<br>0.234<br>2.840<br>57.711<br>0.660 | 5.069<br>27.215<br>14.699<br>1.683<br>0.273<br>7.622<br>0.646<br>0.<br>0.019<br>0.<br>3.845<br>34.465<br>2.945 | 5.376 23.289 4.124 3.430 0.167 2.740 0.379 0. 0.015 0.120 2.785 56.600 0.721 |
| 14  | 0.233  | 0.160  | 0.537  | 0.829   | 1.520  | 0.252  |

# (b) Pavement Construction Cost-Resp.(%) for 1985/86

| Vehicle   | Int.   | Int.  | State   | State  | County  | City  |
|---|--|---|---|--|---|---|
| Class   | Rural  | Urban   | Primary   | Second.  | Roads   | Streets   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11 | 8.620<br>27.089<br>1.989<br>0.261<br>0.653<br>0.406<br>0.462<br>0.036<br>0.222<br>0.067<br>3.634<br>54.465 | 11.869<br>36.848<br>2.806<br>0.376<br>0.537<br>0.607<br>0.577<br>0.192<br>0.179<br>0.042<br>2.117<br>41.641 | 11.556<br>40.609<br>3.790<br>0.184<br>0.340<br>1.594<br>1.399<br>0.142<br>1.484<br>0.092<br>1.129<br>36.364 | 5.560<br>22.144<br>4.736<br>0.205<br>0.175<br>1.821<br>2.123<br>0.088<br>0.615<br>0.235<br>2.852<br>57.957 | 5.053<br>26.368<br>11.646<br>0.381<br>0.263<br>6.812<br>0.934<br>0.<br>2.473<br>0.<br>3.913<br>36.099 | 5.366<br>22.884<br>3.220<br>0.804<br>0.163<br>2.449<br>0.540<br>0.<br>1.025<br>0.182<br>2.824<br>59.317 |
| 13  | 1.861  | 2.048   | 0.775   | 0.659  | 3.028   | 0.744   |
| 14  | 0.234  | 0.160   | 0.541   | 0.832  | 3.030   | 0.481   |



Table I.2. Shoulder Construction Cost-Responsibility Factors

#### (a) Shoulder Construction Cost-Resp.(%) for 1983

| Vehicle   | Int.   | Int.  | State   | State  | County  | City  |
|---|--|---|---|--|---|---|
| Class   | Rural  | Urban   | Primary   | Second.  | Roads   | Streets   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11 | 7.202<br>22.647<br>1.790<br>0.462<br>0.590<br>0.415<br>0.522<br>0.032<br>0.229<br>0.070<br>4.099<br>59.353 | 10.217<br>31.726<br>2.379<br>0.834<br>0.502<br>0.627<br>0.666<br>0.179<br>0.174<br>0.044<br>2.434<br>47.430 | 10.432<br>36.701<br>4.491<br>0.523<br>0.330<br>1.795<br>1.020<br>0.138<br>1.637<br>0.077<br>1.346<br>38.908 | 5.467<br>22.494<br>6.011<br>0.851<br>0.181<br>2.123<br>1.597<br>0.094<br>0.011<br>0.172<br>2.901<br>56.953 | 3.162<br>16.977<br>12.393<br>1.788<br>0.230<br>9.770<br>0.828<br>0.<br>0.024<br>0.<br>4.928<br>44.177 | 3.647<br>15.799<br>3.306<br>3.172<br>0.134<br>2.535<br>0.537<br>0.<br>0.014<br>0.141<br>3.263<br>66.311 |
| 13  | 2.324  | 2.602   | 2.019   | 0.680  | 3.775   | 0.845   |
| 14  | 0.263  | 0.187   | 0.583   | 0.466  | 1.949   | 0.296   |

## (b) Shoulder Construction Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 5.368         | 8.035         | 8.055            | 3.258            | 3.258           | 3.722           |
| 2                | 16.868        | 24.946        | 28.306           | 12.974           | 12.974          | 14.822          |
| 3                | 1.542         | 2.459         | 3.412            | 3.724            | 3.724           | 3.744           |
| 4                | 0.242         | 0.405         | 0.202            | 0.202            | 0.202           | 0.186           |
| 5                | 0.506         | 0.471         | 0.306            | 0.138            | 0.138           | 0.139           |
| 6                | 0.402         | 0.814         | 2.190            | 2.161            | 2.161           | 1.659           |
| 7                | 0.569         | 0.774         | 1.921            | 2.520            | 2.520           | 2.963           |
| 8                | 0.028         | 0.168         | 0.128            | 0.069            | 0.069           | 0.069           |
| 9                | 0.220         | 0.241         | 2.038            | 0.729            | 0.729           | 0.560           |
| 10               | 0.082         | 0.056         | 0.127            | 0.279            | 0.279           | 0.271           |
| 11               | 4.478         | 2.838         | 1.551            | 3.385            | 3.385           | 3.289           |
| 12               | 67.114        | 55.834        | 49.957           | 68.794           | 68.794          | 66.856          |
| 13               | 2.293         | 2.745         | 1.064            | 0.782            | 0.782           | 0.760           |
| 14               | 0.289         | 0.215         | 0.743            | 0.987            | 0.987           | 0.959           |



Table I.3. Right-of-Way Construction Cost-Responsibility Factors

#### (a) Right-of-Way Cost-Resp.(%) for 1983

| Vehicle<br>Class      | Int.<br>Rural  | Int.<br>Urban  | State<br>Primary                                     | State<br>Second.                                     | County<br>Roads                                      | City<br>Streets                                      |
|-----------------------|--|--|--|--|--|--|
| 1<br>2<br>3<br>4<br>5 | 13.294<br>41.513<br>2.317<br>0.335<br>1.081<br>0.473 | 19.187<br>58.674<br>2.352<br>0.363<br>0.936<br>0.542 | 19.528<br>66.319<br>2.584<br>0.107<br>0.571<br>1.253 | 20.177<br>71.670<br>3.319<br>0.061<br>0.493<br>0.530 | 17.936<br>75.281<br>3.925<br>0.051<br>0.634<br>0.878 | 19.328<br>73.952<br>2.166<br>0.231<br>0.481<br>0.725 |
| 7                     | 0.472  | 0.381  | 0.440  | 0.275  | 0.051  | 0.061  |
| 8                     | 0.058  | 0.327  | 0.226  | 0.211  | 0.   | 0.   |
| 9                     | 0.192  | 0.103  | 0.253  | 0.031  | 0.051  | 0.050  |
| 10                    | 0.092  | 0.044  | 0.053  | 0.061  | 0.   | 0.046  |
| 11                    | 3.280  | 1.173  | 0.627  | 0.469  | 0.276  | 0.436  |
| 12                    | 35.686   | 15.245   | 7.692  | 2.549  | 0.643  | 2.393  |
| 13                    | 0.997  | 0.586  | 0.200  | 0.092  | 0.184  | 0.098  |
| 14                    | 0.210  | 0.088  | 0.147  | 0.061  | 0.092  | 0.032  |

#### (b) Right-of-Way Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 13.211        | 19.142        | 19.516           | 20.185           | 17.954          | 19.331          |
| 2                | 41.253        | 58.537        | 66.278           | 71.697           | 75.355          | 73.968          |
| 3                | 2.247         | 2.289         | 2.517            | 3.231            | 3.823           | 2.108           |
| 4                | 0.326         | 0.353         | 0.104            | 0.060            | 0.050           | 0.226           |
| 5                | 1.074         | 0.934         | 0.571            | 0.493            | 0.635           | 0.481           |
| 6                | 0.469         | 0.539         | 1.226            | 0.521            | 0.862           | 0.712           |
| 7                | 0.477         | 0.387         | 0.447            | 0.279            | 0.052           | 0.062           |
| 8                | 0.058         | 0.326         | 0.226            | 0.211            | 0.              | 0.              |
| 9                | 0.189         | 0.102         | 0.256            | 0.032            | 0.052           | 0.051           |
| 10               | 0.093         | 0.044         | 0.055            | 0.062            | 0.              | 0.047           |
| 11               | 3.309         | 1.187         | 0.636            | 0.477            | 0.281           | 0.443           |
| 12               | 36.077        | 15.475        | 7.816            | 2.596            | 0.655           | 2.436           |
| 13               | 1.006         | 0.594         | 0.203            | 0.093            | 0.187           | 0.100           |
| 14               | 0.212         | 0.089         | 0.149            | 0.062            | 0.094           | 0.033           |



Table I.4. Drainage & Erosion Control Cost-Responsibility Factors

#### (a) Drainage & Erosion Control Cost-Resp.(%) for 1983

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 13.985        | 19.633        | 19.778           | 20.183           | 17.939          | 19.330          |
| 2                | 43.672        | 60.038        | 67.168           | 71.689           | 75.295          | 73.963          |
| 3                | 2.342         | 2.295         | 2.515            | 3.315            | 3.919           | 2.165           |
| 4                | 0.328         | 0.341         | 0.100            | 0.061            | 0.051           | 0.231           |
| 5                | 1.093         | 0.914         | 0.555            | 0.492            | 0.633           | 0.481           |
| 6.               | 0.458         | 0.492         | 1.135            | 0.528            | 0.873           | 0.724           |
| 7                | 0.439         | 0.345         | 0.399            | 0.274            | 0.051           | 0.061           |
| 8                | 0.058         | 0.319         | 0,220            | 0.211            | 0.              | 0.              |
| 9                | 0.185         | 0.093         | 0.229            | 0.030            | 0.051           | 0.050           |
| 10               | 0.085         | 0.040         | 0.048            | 0.061            | 0.              | 0.045           |
| 11               | 3.050         | 1.063         | 0.568            | 0.467            | 0.274           | 0.434           |
| 12               | 33.183        | 13.816        | 6.969            | 2.537            | 0.640           | 2.385           |
| 13               | 0.927         | 0.531         | 0.181            | 0.091            | 0.183           | 0.098           |
| 14               | 0.195         | 0.080         | 0.133            | 0.061            | 0.091           | 0.032           |

#### (b) Drainage & Erosion Control Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 13.904        | 19.592        | 19.768           | 20.191           | 17.957          | 19.334          |
| 2                | 43.420        | 59.913        | 67.134           | 71.717           | 75.370          | 73.979          |
| 3                | 2.272         | 2.235         | 2.450            | 3.226            | 3.817           | 2.107           |
| 4                | 0.319         | 0.333         | 0.098            | 0.060            | 0.049           | 0.226           |
| 5                | 1.086         | 0.912         | 0.555            | 0.492            | 0.634           | 0.481           |
| 6                | 0.454         | 0.488         | 1.111            | 0.519            | 0.858           | 0.711           |
| 7                | 0.443         | 0.350         | 0.405            | 0.278            | 0.052           | 0.062           |
| 8                | 0.058         | 0.319         | 0.220            | 0.211            | 0.              | 0.              |
| 9                | 0.183         | 0.093         | 0.232            | 0.031            | 0.052           | 0.051           |
| 10               | 0.086         | 0.040         | 0.050            | 0.062            | 0.              | 0.046           |
| 11               | 3.078         | 1.076         | 0.576            | 0.475            | 0.279           | 0.442           |
| 12               | 33.563        | 14.029        | 7.082            | 2.584            | 0.652           | 2.428           |
| 13               | 0.936         | 0.539         | 0.184            | 0.092            | 0.186           | 0.100           |
| 14               | 0.197         | 0.081         | 0.135            | 0.062            | 0.093           | 0.033           |



Table I.5. Grading & Earthwork Cost-Responsibility Factors

#### (a) Grading & Earthwork Cost-Resp.(%) for 1983

| Vehicle | Int.   | Int.   | State           | State   | County | City    |
|---------|--------|--------|-----------------|---------|--------|---------|
| Class   | Rural  | Urban  | Primary         | Second. | Roads  | Streets |
|         |        |        |                 |         |        |         |
| 1       | 14.807 | 20.164 | 20.011          | 20.032  | 17.845 | 19.252  |
| 2       | 46.240 | 61.660 | 67 <b>.9</b> 58 | 71.154  | 74.901 | 73.663  |
| 3       | 2.371  | 2.228  | 2.450           | 3.443   | 4.083  | 2.208   |
| 4       | 0.319  | 0.316  | 0.095           | 0.066   | 0.055  | 0.241   |
| 5       | 1.106  | 0.887  | 0.541           | 0.511   | 0.660  | 0.491   |
| 6       | 0.439  | 0.431  | 1.026           | 0.596   | 0.991  | 0.755   |
| 7       | 0.400  | 0.303  | 0.360           | 0.310   | 0.058  | 0.069   |
| 8       | 0.059  | 0.309  | 0.214           | 0.219   | 0.     | 0.      |
| 9       | 0.178  | 0.082  | 0.207           | 0.034   | 0.058  | 0.052   |
| 10      | 0.078  | 0.035  | 0.044           | 0.069   | 0.     | 0.050   |
| 11      | 2.776  | 0.932  | 0.513           | 0.527   | 0.311  | 0.474   |
| 12      | 30.206 | 12.118 | 6.297           | 2.867   | 0.726  | 2.602   |
| 13      | 0.844  | 0.466  | 0.164           | 0.103   | 0.207  | 0.107   |
| 14      | 0.178  | 0.070  | 0.120           | 0.069   | 0.104  | 0.035   |
|         |        |        |                 |         |        |         |

# (b) Grading & Earthwork Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 14.729        | 20.127        | 20.011           | 20.039           | 17.864          | 19.255          |
| 2                | 45.995        | 61.549        | 67.958           | 71.179           | 74.978          | 73.677          |
| 3                | 2.301         | 2.170         | 2.450            | 3.351            | 3.978           | 2.149           |
| 4                | 0.310         | 0.308         | 0.095            | 0.065            | 0.054           | 0.236           |
| 5                | 1.100         | 0.886         | 0.541            | 0.511            | 0.661           | 0.491           |
| 6                | 0.436         | 0.429         | 1.026            | 0.586            | 0.974           | 0.742           |
| 7                | 0.404         | 0.307         | 0.360            | 0.314            | 0.059           | 0.071           |
| 8                | 0.059         | 0.309         | 0.214            | 0.219            | 0.              | 0.              |
| 9                | 0.175         | 0.082         | 0.207            | 0.036            | 0.059           | 0.053           |
| 10               | 0.079         | 0.035         | 0.044            | 0.070            | 0.              | 0.051           |
| 11               | 2.804         | 0.944         | 0.513            | 0.537            | 0.317           | 0.482           |
| 12               | 30.575        | 12.309        | 6.297            | 2.919            | 0.740           | 2.649           |
| 13               | 0.852         | 0.473         | 0.164            | 0.104            | 0.211           | 0.109           |
| 14               | 0.180         | 0.071         | 0.120            | 0.070            | 0.106           | 0.036           |



Table I.6. Common Costs Cost-Responsibility Factors

# (a) Common Costs Cost-Resp.(%) for 1983

| Vehicle   | Int.  | Int.  | State  | State   | County  | City   |
|---|---|---|--|---|---|--|
| Class   | Rural   | Urban   | Primary  | Second.   | Roads   | Streets  |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13 | 15.640<br>48.840<br>2.400<br>0.310<br>1.120<br>0.420<br>0.360<br>0.060<br>0.170<br>0.070<br>2.500<br>27.200<br>0.760<br>0.160 | 20.700<br>63.300<br>2.160<br>0.290<br>0.860<br>0.370<br>0.260<br>0.300<br>0.070<br>0.030<br>0.800<br>10.400<br>0.400<br>0.060 | 20.200<br>68.600<br>2.400<br>0.090<br>0.530<br>0.940<br>0.330<br>0.210<br>0.190<br>0.040<br>0.470<br>5.770<br>0.150<br>0.110 | 20.200 71.750 3.300 0.060 0.490 0.520 0.270 0.210 0.030 0.060 0.460 2.500 0.090 0.060 | 17.950 75.340 3.900 0.050 0.630 0.860 0.050 0. 0.050 0. 0.270 0.630 0.180 0.090 | 19.340 74.000 2.160 0.230 0.480 0.720 0.060 0. 0.050 0.045 0.430 2.360 0.097 0.032 |

# (b) Common Costs Cost-Resp.(%) for 1985/86

| Vehicle<br>Class  | Int.<br>Rural   | Int.<br>Urban  | State<br>Primary   | State<br>Second.  | County<br>Roads   | City<br>Streets  |
|---|---|--|--|---|---|--|
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13 | 15.563<br>48.599<br>2.331<br>0.302<br>1.114<br>0.417<br>0.364<br>0.060<br>0.168<br>0.071<br>2.527<br>27.554<br>0.768<br>0.162 | 20.668 63.203 2.105 0.283 0.859 0.368 0.264 0.300 0.070 0.030 0.811 10.571 0.406 0.061 | 20.187<br>68.556<br>2.338<br>0.088<br>0.530<br>0.920<br>0.335<br>0.210<br>0.192<br>0.041<br>0.477<br>5.863<br>0.152<br>0.112 | 20.208 71.778 3.212 0.059 0.490 0.511 0.274 0.210 0.031 0.061 0.468 2.546 0.091 0.061 | 17.968 75.415 3.799 0.049 0.631 0.845 0.051 0. 0.051 0. 0.275 0.642 0.183 0.092 | 19.344 74.013 2.102 0.225 0.480 0.707 0.061 0. 0.051 0.046 0.437 2.403 0.099 0.033 |
| * 4   | 0   |  |  |   |   |  |



Table I.7. Truck-Only Common Costs Cost-Responsibility Factors

#### (a) Truck-Only Common Costs Cost-Resp.(%) for 1983

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1 2              | 0.            | 0.            | 0.<br>0.         | 0.<br>0.         | 0.<br>0.        | 0.              |
| 3                | 7.051         | 14.845        | 23.077           | 45.268           | 64.677          | 36.278          |
| 4                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 5.               | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 6                | 1.234         | 2.543         | 9.038            | 7.133            | 14.262          | 12.093          |
| 7                | 1.058         | 1.787         | 3.173            | 3.704            | 0.829           | 1.008           |
| 8                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 9                | 0.499         | 0.481         | 1.827            | 0.412            | 0.829           | 0.840           |
| 10               | 0.206         | 0.206         | 0.385            | 0.823            | 0.              | 0.756           |
| 11               | 7.344         | 5.498         | 4.519            | 6.310            | 4.478           | 7.222           |
| 12               | 79.906        | 71.478        | 55.481           | 34.294           | 10.448          | 39.637          |
| 13               | 2.233         | 2.749         | 1.442            | 1.235            | 2.985           | 1.629           |
| 14               | 0.470         | 0.412         | 1.058            | 0.823            | 1.493           | 0.537           |

#### Truck-Only Common Costs Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 2                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 3                | 6.785         | 14.335        | 22.414           | 44.276           | 63.984          | 35.403          |
| 4                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 5                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 6                | 1.213         | 2.509         | 8.822            | 7.038            | 14.233          | 11.905          |
| 7                | 1.059         | 1.796         | 3.210            | 3.783            | 0.857           | 1.027           |
| 8                | 0.            | 0.            | 0.               | 0.               | 0.              | 0.              |
| 9                | 0.490         | 0.474         | 1.841            | 0.421            | 0.858           | 0.857           |
| 10               | 0.206         | 0.207         | 0.389            | 0.841            | 0.              | 0.770           |
| 11               | 7.354         | 5.525         | 4.576            | 6.447            | 4.627           | 7.362           |
| 12               | 80.186        | 71.978        | 56.215           | 35.092           | 10.813          | 40.468          |
| 13               | 2.234         | 2.761         | 1.459            | 1.260            | 3.082           | 1.659           |
| 14               | 0.472         | 0.416         | 1.074            | 0.843            | 1.546           | 0.549           |



Table I.8. Pavement Construction Cost-Responsibility of Vehicle Classes on Rural Interstate (1983)

|       |       |           |           | ** 1  | 0 1   |     |       |           |
|-------|-------|-----------|-----------|-------|-------|-----|-------|-----------|
| Veh   | Sub-  |           | nsibility | Veh   | Sub-  |     |       | sibility  |
| Class | Group | Veh Class | Sub-Group | Class | Group | ven | Class | Sub-Group |
|       | 1     | 8.667     | 8.667     | 11    | 6     |     |       | 0.250     |
| 1     | ı     | 0.007     | 0.007     | 11    | 7     |     |       | 0.229     |
|       |       |           | 07.000    |       |       |     |       | 0.243     |
| 2     | 1     | 27.239    | 27.239    | 11    | 8     |     |       |           |
|       |       |           |           | 11    | 9     |     |       | 0.331     |
| 3     | 1     | 2.057     | 0.032     | 11    | 10    |     |       | 0.392     |
| 3     | 2     |           | 0.109     | 11    | 11    |     |       | 0.433     |
| 3     | 3     |           | 0.137     | 11    | 12    |     |       | 0.422     |
| 3     | 4     |           | 0.415     | 11    | 13    |     |       | 0.472     |
| 3     | 5     |           | 0.354     |       |       |     |       |           |
| 3     | 6     |           | 0.301     | 12    | 1     | 54  | .202  | 0.040     |
| 3     | 7     |           | 0.199     | 12    | 2     |     |       | 0.206     |
| 3     | 8     |           | 0.172     | 12    | 3     |     |       | 0.735     |
| 3     | 9     |           | 0.338     | 12    | 4     |     |       | 2.160     |
| 2     | 7     |           | 0.550     | 12    | 5     |     |       | 1.834     |
| ,     |       | 0.000     | 0.000     | 12    | 6     |     |       | 1.182     |
| 4     | 1     | 0.269     | 0.269     |       |       |     |       |           |
|       |       |           |           | 12    | 7     |     |       | 1.033     |
| 5     | 1     | 0.657     | 0.657     | 12    | 8     |     |       | 0.960     |
|       |       |           |           | 12    | 9     |     |       | 0.925     |
| 6     | 1     | 0.411     | 0.035     | 12    | 10    |     |       | 0.922     |
| 6     | 2     |           | 0.018     | 12    | 11    |     |       | 0.951     |
| 6     | 3     |           | 0.029     | 12    | 12    |     |       | 0.996     |
| 6     | 4     |           | 0.062     | 12    | 13    |     |       | 0.961     |
| 6     | 5     |           | 0.059     | 12    | 14    |     |       | 1.242     |
| 6     | 6     |           | 0.039     | 12    | 15    |     |       | 1.479     |
| 6     | 7     |           | 0.042     | 12    | 16    |     |       | 2.062     |
|       | 8     |           | 0.034     | 12    | 17    |     |       | 2.040     |
| 6     |       |           |           | 12    | 18    |     |       | 2.156     |
| 6     | 9     |           | 0.092     |       |       |     |       | 2.712     |
|       |       |           |           | 12    | 19    |     |       |           |
| 7     | 1     | 0.459     | 0.009     | 12    | 20    |     |       | 4.440     |
| 7     | 2     |           | 0.020     | 12    | 21    |     |       | 7.672     |
| 7     | 3     |           | 0.043     | 12    | 22    |     |       | 9.102     |
| 7     | 4     |           | 0.072     | 12    | 23    |     |       | 4.976     |
| 7     | 5     |           | 0.040     | 12    | 24    |     |       | 2.627     |
| 7     | 6     |           | 0.018     | 12    | 25    |     |       | 0.224     |
| 7     | 7     |           | 0.166     | 12    | 26    |     |       | 0.570     |
| 7     | 8     |           | 0.066     |       |       |     |       |           |
| 7     | 9     |           | 0.025     | 13    | 1     | 1   | .857  | 0.108     |
| •     | -     |           |           | 13    | 2     |     |       | 0.182     |
| 8     | 1     | 0.036     | 0.036     | 13    | 3     |     |       | 0.043     |
| 0     | 1     | 0.000     | 0.030     | 13    | 4     |     |       | 0.090     |
| 9     | 1     | 0.226     | 0.058     | 13    | 5     |     |       | 0.053     |
| 9     |       | 0.220     |           | 13    | 6     |     |       | 0.063     |
| 9     | 2     |           | 0.169     |       | 7     |     |       | 0.152     |
|       |       | 0.000     | 0.012     | 13    |       |     |       | 0.071     |
| 10    | 1     | 0.066     | 0.013     | 13    | 8     |     |       |           |
| 10    | 2     |           | 0.013     | 13    | 9     |     |       | 0.085     |
| 10    | 3     |           | 0.026     | 13    | 10    |     |       | 0.177     |
| 10    | 4     |           | 0.015     | 13    | 11    |     |       | 0.094     |
|       |       |           |           | 13    | 12    |     |       | 0.329     |
| 11    | 1     | 3.619     | 0.036     | 13    | 13    |     |       | 0.410     |
| 11    | 2     |           | 0.078     |       |       |     |       |           |
| 11 -  | 3     |           | 0.308     | 14    | 1     | 0   | .233  | 0.049     |
| 11    | 4     |           | 0.145     | 14    | 2     |     |       | 0.066     |
| 11    | 5     |           | 0.281     | 14    | 3     |     |       | 0.119     |
| 1.1   | )     |           | 0.201     | 7.4   | -     |     |       |           |



Table I.9. Pavement Rehabilitation Cost-Responsibility Factors for Rural Interstate

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.323            | 3.136            | 4.697          | 5.322          |                   |                   |
| 2                | 1.270            | 10.007           | 14.793         | 16.738         |                   |                   |
| 3                | 1.784            | 1.897            | 1.461          | 1.515          |                   |                   |
| 4                | 0.193            | 0.215            | 0.172          | 0.180          |                   |                   |
| 5                | 0.031            | 0.231            | 0.340          | 0.385          |                   |                   |
| 6                | 0.361            | 0.372            | 0.320          | 0.326          |                   |                   |
| 7                | 0.529            | 0.498            | 0.327          | 0.329          |                   |                   |
| 8                | 0.002            | 0.013            | 0.018          | 0.021          |                   |                   |
| 9                | 0.313            | 0.286            | 0.219          | 0.217          |                   |                   |
| 10               | 0.042            | 0.047            | 0.040          | 0.041          |                   |                   |
| 11               | 4.785            | 4.365            | 3.020          | 2.990          |                   |                   |
| 12               | 86.643           | 75.723           | 72.667         | 70.068         | and the same      |                   |
| 13               | 3.439            | 2.947            | 1.691          | 1.638          |                   |                   |
| 14               | 0.286            | 0.263            | 0.235          | 0.230          |                   |                   |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.321            | 3.121            | 4.674          | 5.296          |                   |                   |
| 2                | 1.260            | 9.955            | 14.718         | 16.655         |                   |                   |
| 3                | 1.713            | 1.827            | 1.410          | 1.463          |                   |                   |
| 4                | 0.186            | 0.207            | 0.166          | 0.174          |                   |                   |
| 5                | 0.031            | 0.230            | 0.338          | 0.383          |                   |                   |
| 6                | 0.354            | 0.366            | 0.316          | 0.321          |                   |                   |
| 7                | 0.528            | 0.498            | 0.328          | 0.330          |                   |                   |
| 8                | 0.002            | 0.013            | 0.018          | 0.021          |                   |                   |
| 9                | 0.305            | 0.280            | 0.215          | 0.212          |                   |                   |
| 10               | 0.042            | 0.047            | 0.040          | 0.042          |                   |                   |
| 11               | 4.781            | 4.367            | 3.025          | 2.997          |                   |                   |
| 12 .             | 86.754           | 75.881           | 72.824         | 70.237         |                   |                   |
| 13               | 3.435            | 2.945            | 1.691          | 1.638          |                   |                   |
| 14               | 0.286            | 0.263            | 0.235          | 0.231          |                   |                   |
|                  |                  |                  |                |                |                   |                   |

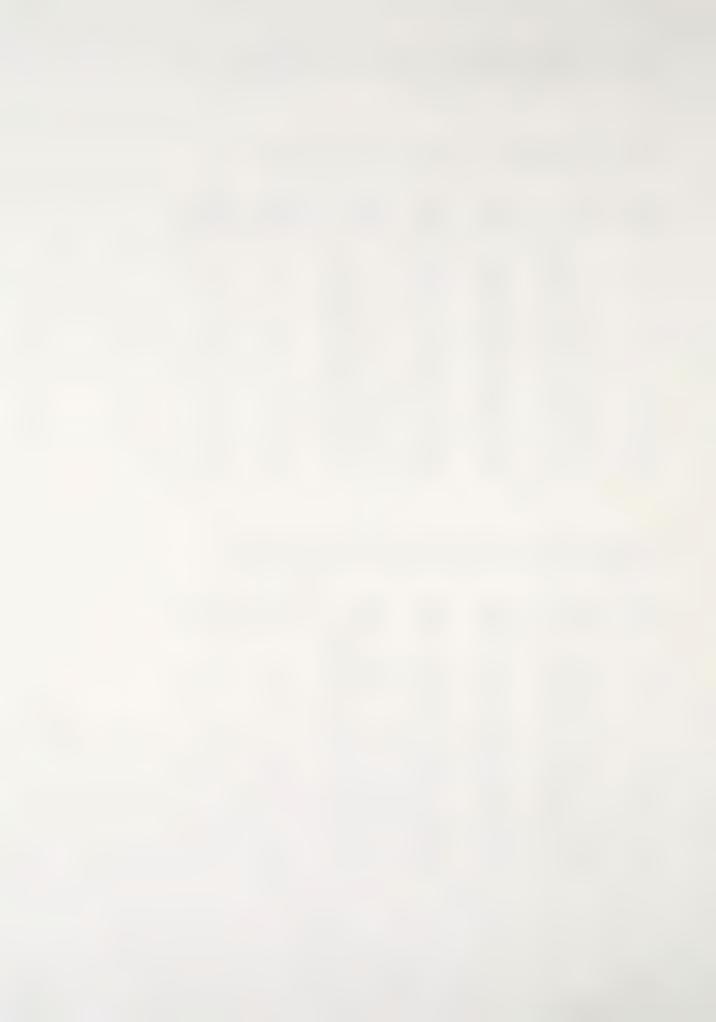


Table I.10. Pavement Rehabilitation Cost-Responsibility Factors for Urban Interstate

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.446            | 4.166            | 6.227          | 7.054          |                   |                   |
| 2                | 2.194            | 13.418           | 19.453         | 21.961         |                   |                   |
| 3                | 3.858            | 3.546            | 2.333          | 2.330          |                   |                   |
| 4.               | 1.720            | 1.458            | 0.841          | 0.813          |                   |                   |
| 5                | 0.034            | 0.186            | 0.266          | 0.300          |                   |                   |
| 6                | 0.766            | 0.693            | 0.541          | 0.532          |                   |                   |
| 7                | 0.925            | 0.803            | 0.479          | 0.469          |                   |                   |
| 8                | 0.019            | 0.071            | 0.096          | 0.108          |                   |                   |
| 9                | 0.312            | 0.268            | 0.088          | 0.041          |                   |                   |
| 10               | 0.034            | 0.033            | 0.023          | 0.023          |                   |                   |
| 11               | 3.721            | 3.185            | 2.050          | 1.971          |                   |                   |
| 12               | 80.796           | 67.866           | 65.066         | 61.968         |                   |                   |
| 13               | 4.907            | 4.079            | 2.336          | 2.237          |                   |                   |
| 14               | 0.267            | 0.229            | 0.200          | 0.193          |                   |                   |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.446            | 4.160            | 6.217          | 7.043          |                   |                   |
| 2                | 2.197            | 13.402           | 19.418         | 21.920         |                   |                   |
| 3                | 3.785            | 3.476            | 2.257          | 2.249          |                   |                   |
| 4                | 0.426            | 0.399            | 0.265          | 0.266          |                   |                   |
| 5                | 0.034            | 0.186            | 0.266          | 0.300          |                   |                   |
| 6                | 0.767            | 0.693            | 0.536          | 0.527          |                   |                   |
| 7                | 0.945            | 0.820            | 0.481          | 0.469          |                   |                   |
| 8                | 0.019            | 0.071            | 0.096          | 0.108          |                   |                   |
| 9                | 0.314            | 0.269            | 0.194          | 0.187          |                   |                   |
| 10               | 0.043            | 0.041            | 0.029          | 0.029          |                   |                   |
| 11               | 3.792            | 3.244            | 2.085          | 2.013          |                   |                   |
| 12               | 82.463           | 69.258           | 65.882         | 62.721         |                   |                   |
| 13               | 4.504            | 3.751            | 2.077          | 1.981          |                   |                   |
| 14               | 0.266            | 0.229            | 0.196          | 0.189          |                   |                   |
|                  |                  |                  |                |                |                   |                   |



Table I.11. Pavement Rehabilitation Cost-Responsibility Factors for State Routes Primary

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid  | North<br>Rigid  | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|-----------------|-----------------|-------------------|-------------------|
| 1<br>2           | 0.479<br>3.781   | 4.101<br>15.705  | 6.096<br>21.655 | 6.901<br>24.337 | 0.502<br>4.464    | 2.703<br>11.370   |
| 3                | 6.039            | 5.391            | 3.251           | 3.203           | 6.114             | 5.675             |
| 4 °<br>5         | 0.302<br>0.035   | 0.265<br>0.126   | 0.151<br>0.170  | 0.148<br>0.191  | 0.308<br>0.042    | 0.282<br>0.094    |
| 6                | 2.046            | 1.854            | 1.341           | 1.318           | 2.127             | 1.961             |
| 7<br>8           | 2.728<br>0.026   | 2.294<br>0.060   | 1.264<br>0.072  | 1.211<br>0.080  | 2.706             | 2.454             |
| 9                | 3.315            | 2.744            | 1.735           | 1.646           | 0.031<br>3.239    | 0.049<br>2.936    |
| 10               | 0.128            | 0.112            | 0.071           | 0.069           | 0.134             | 0.121             |
| 11<br>12         | 1.666<br>76.940  | 1.453<br>63.786  | 0.911<br>61.898 | 0.886<br>58.690 | 1.725             | 1.560             |
| 13               | 1.472            | 1.235            | 0.657           | 0.628           | 76.066<br>1.493   | 68.518<br>1.336   |
| 14               | 1.042            | 0.873            | 0.728           | 0.693           | 1.049             | 0.941             |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.480            | 4.101            | 6.094          | 6.899          | 0.504             | 2.704             |
| 2                | 3.837            | 15.743           | 21.694         | 24.372         | 4.535             | 11.422            |
| 3                | 6.531            | 5.772            | 3.554          | 3.484          | 6.592             | 6.092             |
| 4                | 1.133            | 0.940            | 0.540          | 0.514          | 1.110             | 1.005             |
| 5                | 0.036            | 0.127            | 0.171          | 0.191          | 0.043             | 0.095             |
| 6                | 1.902            | 1.731            | 1.345          | 1.321          | 1.980             | 1.829             |
| 7                | 1.505            | 1.297            | 0.735          | 0.712          | 1.530             | 1.388             |
| 8                | 0.026            | 0.060            | 0.073          | 0.081          | 0.032             | 0.050             |
| 9                | 3.249            | 2.684            | 2.535          | 2.401          | 3.194             | 2.880             |
| 10               | 0.077            | 0.071            | 0.048          | 0.048          | 0.084             | 0.076             |
| 11               | 1.882            | 1.630            | 1.040          | 1.008          | 1.937             | 1.750             |
| 12               | 74.198           | 61.609           | 59.611         | 56.540         | 73.356            | 66.141            |
| 13               | 4.134            | 3.389            | 1.974          | 1.870          | 4.084             | 3.655             |
| 14               | 1.009            | 0.847            | 0.586          | 0,350          | 1.018             | 0.914             |



Table I.12. Pavement Rehabilitation Cost-Responsibility Factors for State Routes Secondary

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid  | North<br>Rigid  | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|-----------------|-----------------|-------------------|-------------------|
| 1 2              | 0.550<br>6.337   | 4.159<br>18.368  | 6.134<br>23.824 | 6.938<br>26.578 | 0.560<br>6.666    | 2.772<br>14.228   |
| 3                | 8.389            | 7.469            | 4.641           | 4.585           | 8.564             | 8.097             |
| 4                | 0.392            | 0.332            | 0.187           | 0.180           | 0.402             | 0.370             |
| 5                | 0.054            | 0.134            | 0.168           | 0.186           | 0.057             | 0.108             |
| 6                | 2.697            | 2.302            | 1.672           | 1.614           | 2.754             | 2.543             |
| 7                | 3.907            | 3.243            | 1.815           | 1.736           | 3.935             | 3.540             |
| 8                | 0.046            | 0.077            | 0.082           | 0.090           | 0.049             | 0.069             |
| 9                | 1.025            | 0.842            | 0.548           | 0.521           | 1.021             | 0.906             |
| 10               | 0.373            | 0.316            | 0.198           | 0.191           | 0.385             | 0.358             |
| 11               | 4.713            | 3.936            | 2.474           | 2.370           | 4.762             | 4.314             |
| 12               | 69.197           | 56.895           | 56.928          | 53.744          | 68.474            | 60.539            |
| 13               | 1.209            | 1.007            | 0.543           | 0.521           | 1.250             | 1.148             |
| 14               | 1.111            | 0.919            | 0.787           | 0.746           | 1.120             | 1.007             |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.548            | 4.160            | 6.135          | 6.940          | 0.558             | 2.771             |
| 2                | 6.280            | 18.326           | 23.801         | 26.557         | 6.606             | 14.176            |
| 3                | 8.066            | 7.189            | 4.466          | 4.415          | 8.236             | 7.792             |
| 4                | 0.381            | 0.323            | 0.181          | 0.175          | 0.391             | 0.360             |
| 5                | 0.054            | 0.134            | 0.167          | 0.186          | 0.057             | 0.108             |
| 6                | 2.618            | 2.236            | 1.622          | 1.566          | 2.674             | 2.470             |
| 7                | 3.916            | 3.251            | 1.817          | 1.738          | 3.945             | 3.551             |
| 8                | 0.046            | 0.076            | 0.082          | 0.089          | 0.049             | 0.069             |
| 9                | 1.046            | 0.860            | 0.559          | 0.531          | 1.042             | 0.925             |
| 10               | 0.374            | 0.318            | 0.198          | 0.192          | 0.387             | 0.360             |
| 11               | 4.736            | 3.956            | 2.483          | 2.379          | 4.787             | 4.337             |
| 12               | 69.611           | 57.242           | 57.158         | 53.965         | 68.895            | 60.923            |
| 13               | 1.208            | 1.006            | 0.542          | 0.520          | 1.249             | 1.148             |
| 14               | 1.116            | 0.923            | 0.789          | 0.748          | 1.125             | 1.011             |



Table I.13. Pavement Rehabilitation Cost-Responsibility Factors for County Roads

| Vehicle | South   | North   | South  | North  | South    | North    |
|---------|---------|---------|--------|--------|----------|----------|
| Class   | Overlay | Overlay | Rigid  | Rigid  | Flexible | Flexible |
|         |         |         |        |        |          |          |
| 1       | 0.609   | 3.795   | 5.545  | 6.255  | 0.615    | 2.566    |
| 2       | 11.474  | 23.217  | 28.510 | 31.198 | 11.711   | 19.037   |
| 3 ·     | 20.327  | 17.318  | 11.741 | 11.310 | 20.407   | 18.608   |
| 4       | 0.665   | 0.553   | 0.359  | 0.342  | 0.669    | 0.602    |
| 5       | 0.123   | 0.216   | 0.254  | 0.276  | 0.126    | 0.184    |
| 6       | 9.145   | 7.627   | 6.404  | 6.096  | 9.183    | 8.274    |
| 7       | 1.522   | 1.251   | 0.802  | 0.760  | 1.519    | 1.351    |
| 8       | 0.      | 0.      | 0.     | 0.     | 0.       | 0.       |
| 9       | 3.660   | 2.996   | 2.221  | 2.099  | 3.636    | 3.215    |
| 10      | 0.      | 0.      | 0.     | 0.     | 0.       | 0.       |
| 11      | 5.824   | 4.804   | 3.444  | 3.267  | 5.819    | 5.192    |
| 12      | 38.269  | 31.326  | 35.267 | 33,236 | 37.891   | 33.436   |
| 13      | 4.864   | 4.007   | 2.583  | 2.450  | 4.911    | 4.413    |
| 14      | 3.519   | 2.889   | 2.870  | 2.711  | 3.512    | 3.122    |
| _ ,     |         |         |        | _ ,,   |          |          |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.609            | 3.798            | 5.550          | 6.260          | 0.615             | 2.568             |
| 2                | 11.443           | 23.206           | 28.495         | 31.188         | 11.681            | 19.019            |
| 3                | 19.718           | 16.802           | 11.362         | 10.947         | 19.798            | 18.055            |
| 4                | 0.649            | 0.539            | 0.350          | 0.333          | 0.653             | 0.588             |
| 5                | 0.123            | 0.216            | 0.254          | 0.276          | 0.126             | 0.184             |
| 6                | 8.947            | 7.464            | 6.248          | 5.948          | 8.986             | 8.097             |
| 7                | 1.546            | 1.271            | 0.812          | 0.770          | 1.543             | 1.373             |
| 8                | 0.               | 0.               | 0.             | 0.             | 0.                | 0.                |
| 9                | 3.717            | 3.043            | 2.249          | 2.126          | 3.694             | 3.266             |
| 10               | 0.               | 0.               | 0.             | 0.             | 0.                | 0.                |
| 11               | 5.907            | 4.873            | 3.483          | 3.304          | 5.902             | 5.267             |
| 12               | 38.834           | 31.790           | 35.678         | 33.625         | 38.455            | 33.937            |
| 13               | 4.924            | 4.057            | 2.607          | 2.473          | 4.973             | 4.469             |
| 14               | 3.582            | 2.941            | 2.913          | 2.751          | 3.575             | 3.179             |



Table I.14. Pavement Rehabilitation Cost-Responsibility Factors for City Streets

#### (a) Pavement Rehabilitation Cost-Resp.(%) for 1983

| Vehicle<br>Class  | South<br>Overlay  | North<br>Overlay   | South<br>Rigid   | North<br>Rigid   | South<br>Flexible   | North<br>Flexible  |
|---|---|--|--|--|---|--|
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12 | 0.523<br>6.412<br>5.693<br>1.544<br>0.052<br>3.864<br>0.920<br>0.<br>1.844<br>0.284<br>4.677<br>72.236<br>1.321 | 3.979 18.834 5.049 1.304 0.131 3.290 0.763 0. 1.515 0.240 3.899 59.378 1.098 | 5.877<br>24.719<br>3.190<br>0.756<br>0.166<br>2.450<br>0.428<br>0.<br>0.973<br>0.157<br>2.454<br>57.761<br>0.621 | 6.647<br>27.542<br>3.138<br>0.728<br>0.184<br>2.357<br>0.408<br>0.<br>0.922<br>0.151<br>2.344<br>54.563<br>0.593 | 0.527<br>6.558<br>5.747<br>1.562<br>0.053<br>3.902<br>0.924<br>0.<br>1.842<br>0.288<br>4.699<br>71.923<br>1.342 | 2.642<br>14.241<br>5.383<br>1.425<br>0.102<br>3.571<br>0.829<br>0.<br>1.639<br>0.264<br>4.235<br>63.887<br>1.217 |
| 14  | 0.631   | 0.521  | 0.449  | 0.425  | 0.633   | 0.567  |

# (b) Pavement Rehabilitation Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.521            | 3 <b>.9</b> 78   | 5.877          | 6.647          | 0.525             | 2.640             |
| 2                | 6.351            | 18.787           | 24.688         | 27.514         | 6.496             | 14.186            |
| 3                | 5.471            | 4.857            | 3.069          | 3.020          | 5.524             | 5.176             |
| 4                | 1.492            | 1.261            | 0.730          | 0.703          | 1.509             | 1.377             |
| 5                | 0.052            | 0.130            | 0.165          | 0.183          | 0.053             | 0.102             |
| 6                | 3.747            | 3.192            | 2.375          | 2.285          | 3.784             | 3.464             |
| 7                | 0.924            | 0.766            | 0.429          | 0.409          | 0.928             | 0.832             |
| 8                | 0.               | 0.               | 0.             | 0.             | 0.                | 0.                |
| 9                | 1.857            | 1.526            | 0.978          | 0.927          | 1.856             | 1.651             |
| 10               | 0.286            | 0.243            | 0.158          | 0.152          | 0.291             | 0.266             |
| 11               | 4.694            | 3.914            | 2.461          | 2.350          | 4.716             | 4.251             |
| 12               | 72.632           | 59.710           | 57.988         | 54.780         | 72.322            | 64.249            |
| 13               | 1.332            | 1.107            | 0.625          | 0.597          | 1.352             | 1.226             |
| 14               | 0.642            | 0.530            | 0.456          | 0.432          | 0.645             | 0.577             |



Table I.15. Pavement Maintenance Cost-Responsibility Factors for Rural Interstate

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.480            | 3.136            | 4.697          | 5.322          |                   |                   |
| 2                | 1.792            | 10.017           | 14.794         | 16.739         |                   |                   |
| 3                | 1.825            | 1.906            | 1.464          | 1.518          |                   |                   |
| 4                | 0.207            | 0.218            | 0.172          | 0.180          |                   |                   |
| 5                | 0.044            | 0.232            | 0.340          | 0.385          |                   |                   |
| 6                | 0.380            | 0.377            | 0.321          | 0.327          |                   |                   |
| 7                | 0.548            | 0.504            | 0.328          | 0.330          |                   |                   |
| 8                | 0.003            | 0.013            | 0.018          | 0.021          |                   |                   |
| 9                | 0.320            | 0.289            | 0.220          | 0.217          |                   |                   |
| 10               | 0.045            | 0.048            | 0.040          | 0.041          |                   |                   |
| 11               | 4.780            | 4.367            | 3.029          | 2.999          |                   |                   |
| 12               | 85.864           | 75.681           | 72.644         | 70.047         |                   |                   |
| 13               | 3.417            | 2.948            | 1.697          | 1.643          |                   |                   |
| 14               | 0.294            | 0.266            | 0.235          | 0.231          |                   | -                 |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.478            | 3.121            | 4.674          | 5.296          |                   |                   |
| 2                | 1.780            | 9.964            | 14.719         | 16.655         |                   |                   |
| 3                | 1.752            | 1.835            | 1.414          | 1.466          |                   |                   |
| 4                | 0.200            | 0.211            | 0.167          | 0.174          |                   |                   |
| 5                | 0.043            | 0.230            | 0.338          | 0.383          |                   | -                 |
| 6                | 0.374            | 0.371            | 0.317          | 0.322          |                   |                   |
| 7                | 0.548            | 0.504            | 0.329          | 0.331          |                   |                   |
| 8                | 0.003            | 0.013            | 0.018          | 0.021          |                   |                   |
| 9                | 0.312            | 0.283            | 0.215          | 0.213          |                   |                   |
| 10               | 0.045            | 0.048            | 0.040          | 0.042          |                   |                   |
| 11               | 4.777            | 4.369            | 3.034          | 3.005          |                   |                   |
| 12               | 85.981           | 75.839           | 72.802         | 70.216         |                   |                   |
| 13               | 3.413            | 2.946            | 1.697          | 1.644          |                   |                   |
| 14               | 0.294            | 0.266            | 0.236          | 0.231          |                   |                   |



Table I.16. Pavement Maintenance Cost-Responsibility Factors for Urban Interstate

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.657            | 4.168            | 6.227          | 7.054          |                   |                   |
| 2                | 2.954            | 13.463           | 19.457         | 21.962         |                   |                   |
| 3                | 3.988            | 3.629            | 2.348          | 2.338          |                   |                   |
| 4                | 0.469            | 0.422            | 0.275          | 0.276          |                   |                   |
| 5                | 0.045            | 0.186            | 0.266          | 0.300          |                   |                   |
| 6                | 0.817            | 0.717            | 0.548          | 0.537          |                   |                   |
| 7                | 0.973            | 0.829            | 0.482          | 0.469          |                   |                   |
| 8                | 0.024            | 0.071            | 0.096          | 0.108          |                   |                   |
| 9                | 0.324            | 0.276            | 0.198          | 0.190          |                   |                   |
| 10               | 0.047            | 0.042            | 0.029          | 0.029          |                   |                   |
| 11               | 3.769            | 3.242            | 2.091          | 2.017          |                   |                   |
| 12               | 81.204           | 68.979           | 65.703         | 62.543         |                   |                   |
| 13               | 4.456            | 3.745            | 2.082          | 1.986          |                   |                   |
| 14               | 0.272            | 0.230            | 0.196          | 0.188          |                   |                   |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.656            | 4.161            | 6.218          | 7.043          |                   |                   |
| 2                | 2.935            | 13.431           | 19.421         | 21.923         |                   |                   |
| 3                | 3.834            | 3.494            | 2.264          | 2.255          |                   |                   |
| 4                | 0.452            | 0.407            | 0.266          | 0.267          |                   |                   |
| 5                | 0.044            | 0.186            | 0.266          | 0.300          |                   |                   |
| 6                | 0.802            | 0.705            | 0.538          | 0.529          |                   |                   |
| 7                | 0.975            | 0.831            | 0.484          | 0.471          |                   |                   |
| 8                | 0.023            | 0.071            | 0.096          | 0.108          |                   |                   |
| 9                | 0.320            | 0.272            | 0.195          | 0.188          |                   |                   |
| 10               | 0.046            | 0.042            | 0.029          | 0.029          |                   |                   |
| 11               | 3.769            | 3.244            | 2.092          | 2.019          |                   |                   |
| 12               | 81.410           | 69.176           | 65.851         | 62.692         |                   |                   |
| 13               | 4.461            | 3.750            | 2.084          | 1.988          |                   |                   |
| 14               | 0.272            | 0.231            | 0.197          | 0.189          |                   |                   |



Table I.17. Pavement Maintenance Cost-Responsibility Factors for State Routes Primary

| Vehicle<br>Class | South<br>Overlay        | North<br>Overlay        | South<br>Rigid          | North<br>Rigid          | South<br>Flexible       | North<br>Flexible        |
|------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|--------------------------|
| 1<br>2<br>3      | 0.681<br>4.483          | 4.100<br>15.664         | 6.096<br>21.673         | 6.901<br>24.339         | 0.477<br>3.711<br>5.991 | 2.692<br>11.056<br>5.628 |
| 3<br>4<br>5      | 6.032<br>0.302<br>0.041 | 5.361<br>0.262<br>0.126 | 3.288<br>0.153<br>0.170 | 3.207<br>0.148<br>0.191 | 0.298                   | 0.278                    |
| 6<br>7           | 2.052                   | 1.836<br>2.287          | 1.357<br>1.280<br>0.073 | 1.320<br>1.212<br>0.080 | 2.018<br>2.718<br>0.025 | 1.921<br>2.458<br>0.047  |
| 8<br>9<br>10     | 0.028<br>3.284<br>0.128 | 0.059<br>2.743<br>0.111 | 1.755<br>0.072          | 1.649<br>0.069          | 3.315<br>0.126          | 2.964<br>0.118           |
| 11<br>12         | 1.665<br>76.088         | 1.441<br>63.912         | 0.922<br>61.762         | 0.887<br>58.674         | 1.646<br>77.147         | 1.531 68.956             |
| 13<br>14         | 1.468<br>1.036          | 1.226<br>0.870          | 0.667<br>0.731          | 0.629<br>0.693          | 1.456<br>1.037          | 1.323<br>0.937           |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.680            | 4.097            | 6.092          | 6.897          | 0.475             | 2.690             |
| 2                | 4.452            | 15.632           | 21.647         | 24.312         | 3.681             | 11.024            |
| 3                | 5.808            | 5.167            | 3.170          | 3.093          | 5.767             | 5.422             |
| 4                | 0.292            | 0.254            | 0.148          | 0.143          | 0.288             | 0.269             |
| 5                | 0.040            | 0.126            | 0.170          | 0.190          | 0.034             | 0.091             |
| 6                | 1.985            | 1.778            | 1.314          | 1.279          | 1.952             | 1.860             |
| 7                | 2.719            | 2.295            | 1.284          | 1.216          | 2.726             | 2.467             |
| 8                | 0.028            | 0.059            | 0.072          | 0.080          | 0.025             | 0.046             |
| 9                | 3.280            | 2.740            | 1.751          | 1.645          | 3.310             | 2.960             |
| 10               | 0.130            | 0.113            | 0.073          | 0.070          | 0.127             | 0.119             |
| 11               | 1.670            | 1.447            | 0.925          | 0.890          | 1.651             | 1.536             |
| 12               | 76.404           | 64.190           | 61.951         | 58.856         | 77.460            | 69.249            |
| 13               | 1.470            | 1.228            | 0.667          | 0.630          | 1.458             | 1.325             |
| 14               | 1.042            | 0.876            | 0.735          | 0.697          | 1.044             | 0.943             |



Table I.18. Pavement Maintenance Cost-Responsibility Factors for State Routes Secondary

| Vehicle   | South   | North  | South  | North  | South   | North  |
|---|---|--|--|--|---|--|
| Class   | Overlay   | Overlay  | Rigid  | Rigid  | Flexible  | Flexible   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10 | 0.758 7.272 8.502 0.398 0.061 2.729 3.902 0.050 1.013 0.381 4.716 | 4.168<br>18.653<br>7.620<br>0.341<br>0.137<br>2.351<br>3.267<br>0.079<br>0.839<br>0.327<br>3.978 | 6.134<br>23.846<br>4.671<br>0.188<br>0.168<br>1.683<br>1.828<br>0.082<br>0.552<br>0.199<br>2.490 | 6.937<br>26.546<br>4.542<br>0.178<br>0.186<br>1.597<br>1.717<br>0.089<br>0.516<br>0.189<br>2.346 | 0.542<br>6.086<br>8.230<br>0.383<br>0.052<br>2.644<br>3.875<br>0.044<br>1.025<br>0.362<br>4.668 | 2.745<br>13.324<br>7.579<br>0.341<br>0.100<br>2.372<br>3.447<br>0.062<br>0.913<br>0.322<br>4.169 |
| 12  | 67.872  | 56.272   | 56.821   | 53.899   | 69.813  | 62.616   |
| 13  | 1.235   | 1.042  | 0.548  | 0.514  | 1.174   | 1.031  |
| 14  | 1.109   | 0.926  | 0.788  | 0.744  | 1.103   | 0.980  |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.757            | 4.168            | 6.136          | 6.939          | 0.541             | 2.744             |
| 2                | 7.213            | 18.609           | 23.822         | 26.526         | 6.031             | 13.280            |
| 3                | 8.177            | 7.335            | 4.495          | 4.373          | 7.912             | 7.290             |
| 4                | 0.387            | 0.331            | 0.183          | 0.173          | 0.372             | 0.332             |
| 5                | 0.061            | 0.136            | 0.168          | 0.186          | 0.051             | 0.099             |
| 6                | 2.650            | 2.284            | 1.633          | 1.550          | 2.566             | 2.303             |
| 7                | 3.912            | 3.276            | 1.830          | 1.718          | 3.884             | 3.455             |
| 8                | 0.050            | 0.078            | 0.082          | 0.089          | 0.044             | 0.061             |
| 9                | 1.034            | 0.857            | 0.562          | 0.526          | 1.046             | 0.931             |
| 10               | 0.383            | 0.329            | 0.200          | 0.189          | 0.363             | 0.323             |
| 11               | 4.740            | 4.000            | 2.500          | 2.355          | 4.690             | 4.189             |
| 12               | 68.288           | 56.625           | 57.053         | 54.118         | 70.220            | 62.978            |
| 13               | 1.234            | 1.041            | 0.547          | 0.513          | 1.172             | 1.029             |
| 14               | 1.114            | 0.931            | 0.790          | 0.746          | 1.107             | 0.984             |



Table I.19. Pavement Maintenance Cost-Responsibility Factors for County Roads

| Vehicle                              | South   | North  | South   | North  | South  | North  |
|--------------------------------------|---|--|---|--|--|--|
| Class                                | Overlay   | Overlay  | Rigid   | Rigid  | Flexible   | Flexible   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 | 0.791<br>12.321<br>20.240<br>0.663<br>0.130<br>9.100<br>1.505<br>0. | 3.800<br>23.422<br>17.387<br>0.556<br>0.219<br>7.660<br>1.249<br>0.<br>2.975 | 5.546<br>28.527<br>11.766<br>0.360<br>0.254<br>6.417<br>0.804<br>0. | 6.254 31.173 11.273 0.341 0.276 6.077 0.758 0. 2.094 | 0.605<br>11.289<br>20.248<br>0.661<br>0.121<br>9.106<br>1.523<br>0.<br>3.677 | 2.549<br>18.380<br>18.361<br>0.590<br>0.177<br>8.154<br>1.358<br>0.<br>3.278 |
| 10                                   | 0.  | 0.   | 0.  | 0.   | 0.   | 0.   |
| 11                                   | 5.764   | 4.799  | 3.450   | 3.258  | 5.828  | 5.206  |
| 12                                   | 37.541  | 31.002   | 35.192  | 33.345   | 38.598   | 34.532   |
| 13                                   | 4.861   | 4.048  | 2.590   | 2.440  | 4.821  | 4.274  |
| 14                                   | 3.479   | 2.883  | 2.869   | 2.712  | 3.523  | 3.140  |

| Vehicle | South   | North   | South  | North  | South    | North    |
|---------|---------|---------|--------|--------|----------|----------|
| Class   | Overlay | Overlay | Rigid  | Rigid  | Flexible | Flexible |
|         | •       | -       | J      | Ü      |          |          |
| 1       | 0.757   | 4.168   | 6.136  | 6.939  | 0.541    | 2.551    |
| 2       | 7.213   | 18.609  | 23.822 | 26.526 | 6.031    | 18.361   |
| 3       | 8.177   | 7.335   | 4.495  | 4.373  | 7.912    | 17.810   |
| 4       | 0.387   | 0.331   | 0.183  | 0.173  | 0.372    | 0.576    |
| 5       | 0.061   | 0.136   | 0.168  | 0.186  | 0.051    | 0.177    |
| 6       | 2.650   | 2.284   | 1.633  | 1.550  | 2.566    | 7.978    |
| 7       | 3.912   | 3.276   | 1.830  | 1.718  | 3.884    | 1.379    |
| 8       | 0.050   | 0.078   | 0.082  | 0.089  | 0.044    | 0.       |
| 9       | 1.034   | 0.857   | 0.562  | 0.526  | 1.046    | 3.329    |
| 10      | 0.383   | 0.329   | 0.200  | 0.189  | 0.363    | 0.       |
| 11      | 4.740   | 4.000   | 2.500  | 2.355  | 4.690    | 5.279    |
| 12      | 68.288  | 56.625  | 57.053 | 54.118 | 70.220   | 35.038   |
| 13      | 1.234   | 1.041   | 0.547  | 0.513  | 1.172    | 4.326    |
| 14      | 1.114   | 0.931   | 0.790  | 0.746  | 1.107    | 3.196    |
|         |         |         |        |        |          |          |



Table I. 20. Pavement Maintenance Cost-Responsibility Factors for City Streets

| Vehicle<br>Class | South<br>Overlay         | North<br>Overlay         | South<br>Rigid           | North<br>Rigid           | South<br>Flexible        | North<br>Flexible        |
|------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| 1 2              | 0.718<br>7.224           | 3.983<br>18.961          | 5.877<br>24.730          | 6.646<br>27.527          | 0.519<br>6.297           | 2.630<br>13.834          |
| 2<br>3<br>4      | 5.708<br>1.548           | 5.095<br>1.320           | 3.199<br>0.759           | 3.124<br>0.724           | 5.643<br>1.528           | 5.222<br>1.372           |
| 5                | 0.057<br>3.868           | 0.132                    | 0.166<br>2.458           | 0.183                    | 0.051                    | 0.099                    |
| 7<br>8           | 0.915                    | 0.766                    | 0.430                    | 0.406                    | 0.917                    | 0.818                    |
| 9<br>10          | 1.826<br>0.285           | 1.513                    | 0.976<br>0.157           | 0.918<br>0.150           | 1.844<br>0.280           | 1.641<br>0.251           |
| 11               | 4.654                    | 3.917                    | 2.462                    | 2.333                    | 4.657                    | 4.171                    |
| 12<br>13<br>14   | 71.242<br>1.328<br>0.627 | 59.109<br>1.116<br>0.523 | 57.714<br>0.623<br>0.449 | 54.630<br>0.589<br>0.424 | 72.505<br>1.303<br>0.628 | 64.789<br>1.157<br>0.560 |
|                  |                          |                          |                          |                          |                          |                          |

| Vehicle<br>Class | South<br>Overlay | North<br>Overlay | South<br>Rigid | North<br>Rigid | South<br>Flexible | North<br>Flexible |
|------------------|------------------|------------------|----------------|----------------|-------------------|-------------------|
| 1                | 0.757            | 4.168            | 6.136          | 6.939          | 0.541             | 2.629             |
| 2                | 7.213            | 18.609           | 23.822         | 26.526         | 6.031             | 13.783            |
| 3                | 8.177            | 7.335            | 4.495          | 4.373          | 7.912             | 5.021             |
| 4                | 0.387            | 0.331            | 0.183          | 0.173          | 0.372             | 1.325             |
| 5                | 0.061            | 0.136            | 0.168          | 0.186          | 0.051             | 0.098             |
| 6                | 2.650            | 2.284            | 1.633          | 1.550          | 2.566             | 3.354             |
| 7                | 3.912            | 3.276            | 1.830          | 1.718          | 3.884             | 0.821             |
| 8                | 0.050            | 0.078            | 0.082          | 0.089          | 0.044             | 0.                |
| 9                | 1.034            | 0.857            | 0.562          | 0.526          | 1.046             | 1.653             |
| 10               | 0.383            | 0.329            | 0.200          | 0.189          | 0.363             | 0.254             |
| 11               | 4.740            | 4.000            | 2.500          | 2.355          | 4.690             | 4.186             |
| 12               | 68.288           | 56.625           | 57.053         | 54.118         | 70.220            | 65.140            |
| 13               | 1.234            | 1.041            | 0.547          | 0.513          | 1.172             | 1.166             |
| 14               | 1.114            | 0.931            | 0.790          | 0.746          | 1.107             | 0.570             |



Table I.21. Bridge Superstructure Cost-Responsibility Factors

## (a)Bridge Superstructure Cost-Resp.(%) for 1983

| Vehicle                                   | Int.  | Int.   | State  | State  | County  | City  |
|---|---|--|--|--|---|---|
| Class                                     | Rural   | Urban  | Primary  | Second.  | Roads   | Streets   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9 | 7.615<br>23.779<br>2.565<br>0.445<br>0.693<br>0.504<br>0.377<br>0.044<br>3.723<br>0.084 | 10.080<br>30.823<br>3.973<br>0.794<br>0.670<br>0.799<br>0.463<br>0.312<br>3.820<br>0.065 | 11.137<br>37.821<br>5.136<br>0.349<br>0.485<br>2.075<br>0.749<br>0.260<br>6.692<br>0.114 | 11.337<br>40.269<br>8.073<br>0.396<br>0.519<br>1.842<br>0.862<br>0.316<br>3.928<br>0.266 | 10.701<br>44.914<br>11.421<br>0.483<br>0.727<br>4.152<br>0.209<br>0.<br>5.506 | 11.520<br>44.079<br>5.490<br>1.447<br>0.553<br>2.612<br>0.205<br>0.<br>5.394<br>0.208 |
| 11  | 3.301   | 1.967  | 1.233  | 2.063  | 1.771   | 1.995   |
| 12  | 49.177  | 38.579   | 28.243   | 23.210   | 10.399  | 21.743  |
| 13  | 1.539   | 1.700  | 0.718  | 0.594  | 1.806   | 0.634   |
| 14  | 6.153   | 5.954  | 4.986  | 6.326  | 7.915   | 4.125   |

### (b)Bridge Superstructure Cost-Resp.(%) for 1985/86

| Vehicle  | Int.   | Int.            | State           | State           | County          | City    |
|----------|--------|-----------------|-----------------|-----------------|-----------------|---------|
| Class    | Rural  | Urban           | Primary         | Second.         | Roads           | Streets |
| 1 2      | 7.578  | 10.064          | 11.133          | 11.342          | 10.701          | 11.520  |
|          | 23.665 | 30.777          | 37.809          | 40.286          | 44.914          | 44.079  |
| 3        | 2.482  | 3.854           | 4.991           | 7.870           | 11.421          | 5.490   |
| 4        | 0.430  | 0.768           | 0.339           | 0.385           | 0.483           | 1.447   |
| 5        | 0.688  | 0.667           | 0.485           | 0.520           | 0.727           | 0.553   |
| 6        | 0.499  | 0.794           | 2.033           | 1.822           | 4.152           | 2.612   |
| 7<br>8   | 0.379  | 0.467           | 0.758           | 0.876           | 0.209           | 0.205   |
| 9        | 0.044  | 0.310           | 0.259           | 0.317           | 0.              | 0.      |
|          | 3.856  | 3.797           | 6.674           | 3.913           | 5.506           | 5.394   |
| 10       | 0.084  | 0.065           | 0.116           | 0.269           | 0.              | 0.208   |
| 11       | 3.316  | 1.977           | 1.246           | 2.086           | 1.771           | 1.995   |
| 12<br>13 | 49.484 | 38.794<br>1.700 | 28.441<br>0.720 | 23.377<br>0.599 | 10.399<br>1.806 | 21.743  |
| 14       | 5.957  | 5.962           | 4.996           | 6.339           | 7.915           | 4.125   |



Table I. 22. Bridge Pier Cost-Responsibility Factors

### (a)Bridge Pier Cost-Resp.(%) for 1983

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 12.823        | 16.974        | 17.165           | 15.150           | 15.273          | 16.442          |
| 2                | 40.043        | 51.905        | 58.292           | 53.811           | 64.103          | 62.911          |
| 3                | 2.773         | 3.492         | 3.992            | 7.527            | 8.200           | 3.434           |
| 4                | 0.421         | 0.611         | 0.251            | 0.448            | 0.369           | 1.075           |
| 5                | 0.921         | 0.711         | 0.455            | 0.374            | 0.546           | 0.415           |
| 6                | 0.486         | 0.600         | 1.098            | 1.358            | 1.958           | 1.216           |
| 7                | 0.402         | 0.396         | 0.583            | 0.775            | 0.177           | 0.147           |
| 8                | 0.055         | 0.309         | 0.182            | 0.302            | 0.              | 0.              |
| 9                | 0.323         | 0.244         | 0.753            | 0.358            | 0.602           | 0.450           |
| 10               | 0.094         | 0.062         | 0.109            | 0.300            | 0.              | 0.214           |
| 11               | 3.322         | 1.629         | 1.095            | 2.119            | 1.555           | 1.609           |
| 12               | 36.880        | 21.889        | 15.113           | 16.120           | 4.819           | 11.288          |
| 13               | 1.050         | 0.867         | 0.424            | 0.672            | 1.381           | 0.471           |
| 14               | 0.404         | 0.310         | 0.488            | 0.687            | 1.018           | 0.327           |

# (b)Bridge Pier Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 12.761        | 16.948        | 17.159           | 15.156           | 15.273          | 16.442          |
| 2                | 39.851        | 51.826        | 58.273           | 53.833           | 64.103          | 62.911          |
| 3                | 2.687         | 3.389         | 3.874            | 7.319            | 8.200           | 3.434           |
| 4                | 0.408         | 0.593         | 0.243            | 0.435            | 0.369           | 1.075           |
| 5                | 0.917         | 0.709         | 0.455            | 0.374            | 0.546           | 0.415           |
| 6                | 0.483         | 0.598         | 1.082            | 1.350            | 1.958           | 1.216           |
| 7                | 0.406         | 0.400         | 0.589            | 0.785            | 0.177           | 0.147           |
| 8                | 0.054         | 0.308         | 0.182            | 0.303            | 0.              | 0.              |
| 9                | 0.323         | 0.242         | 0.754            | 0.360            | 0.602           | 0.450           |
| 10               | 0.095         | 0.063         | 0.110            | 0.303            | 0.              | 0.214           |
| 11               | 3.345         | 1.642         | 1.105            | 2.140            | 1.555           | 1.609           |
| 12               | 37.212        | 22.097        | 15.254           | 16.274           | 4.819           | 11.288          |
| 13               | 1.056         | 0.873         | 0.427            | 0.677            | 1.381           | 0.471           |
| 14               | 0.400         | 0.311         | 0.491            | 0.691            | 1.018           | 0.327           |



Table I.23. Bridge Excavation & Backfill Cost-Responsibility Factors

## (a)Bridge Excavation & Backfill Cost-Resp.(%) for 1983

| Vehicle  | Int.           | Int.           | State          | State          | County         | City           |
|----------|----------------|----------------|----------------|----------------|----------------|----------------|
| Class    | Rural          | Urban          | Primary        | Second.        | Roads          | Streets        |
| 1        | 12.823         | 16.974         | 17.165         | 15.150         | 15.273         | 16.442         |
| 2        | 40.043         | 51.905         | 58.292         | 53.811         | 64.103         | 62.911         |
| 3        | 2.773          | 3.492          | 3.992          | 7.527          | 8.200          | 3.434          |
| 4 ·<br>5 | 0.421          | 0.611          | 0.251          | 0.448          | 0.369          | 1.075<br>0.415 |
| 6        | 0.486<br>0.402 | 0.600<br>0.396 | 1.098<br>0.583 | 1.358<br>0.775 | 1.958<br>0.177 | 1.216          |
| 8        | 0.055          | 0.309          | 0.182          | 0.302          | 0.             | 0.             |
| 9        | 0.323          | 0.244          | 0.753          | 0.358          | 0.602          | 0.450          |
| 10       | 0.094          | 0.062          | 0.109          | 0.300          | 0.             | 0.214          |
| 11       | 3.322          | 1.629          | 1.095          | 2.119          | 1.555          |                |
| 12       | 36.880         | 21.889         | 15.113         | 16.120         | 4.819          | 11.288         |
| 13       | 1.050          | 0.867          | 0.424          | 0.672          | 1.381          | 0.471          |
| 14       | 0.404          | 0.310          | 0.488          | 0.687          | 1.018          | 0.327          |

## (b)Bridge Excavation & Backfill Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 12.761        | 16.948        | 17.159           | 15.156           | 15.273          | 16.442          |
| 2                | 39.851        | 51.826        | 58.273           | 53.833           | 64.103          | 62.911          |
| 3                | 2.687         | 3.389         | 3.874            | 7.319            | 8.200           | 3.434           |
| 4                | 0.408         | 0.593         | 0.243            | 0.435            | 0.369           | 1.075           |
| 5                | 0.917         | 0.709         | 0.455            | 0.374            | 0.546           | 0.415           |
| 6                | 0.483         | 0.598         | 1.082            | 1.350            | 1.958           | 1.216           |
| 7                | 0.406         | 0.400         | 0.589            | 0.785            | 0.177           | 0.147           |
| 8                | 0.054         | 0.308         | 0.182            | 0.303            | 0.              | 0.              |
| 9                | 0.323         | 0.242         | 0.754            | 0.360            | 0.602           | 0.450           |
| 10               | 0.095         | 0.063         | 0.110            | 0.303            | 0.              | 0.214           |
| 11               | 3.345         | 1.642         | 1.105            | 2.140            | 1.555           | 1.609           |
| 12               | 37.212        | 22.097        | 15.254           | 16.274           | 4.819           | 11.288          |
| 13               | 1.056         | 0.873         | 0.427            | 0.677            | 1.381           | 0.471           |
| 14               | 0.400         | 0.311         | 0.491            | 0.691            | 1.018           | 0.327           |



Table I.24. Bridge Drainage Cost-Responsibility Factors

### (a)Bridge Drainage Cost-Resp.(%) for 1983

| Vehicle   | Int.  | Int.   | State  | State   | County   | City  |
|---|---|--|--|---|--|---|
| Class   | Rural   | Urban  | Primary  | Second.   | Roads  | Streets   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11 | 12.823<br>40.043<br>2.773<br>0.421<br>0.921<br>0.486<br>0.402<br>0.055<br>0.323<br>0.094<br>3.322<br>36.880 | 16.974 51.905 3.492 0.611 0.711 0.600 0.396 0.309 0.244 0.062 1.629 21.889 | 17.165 58.292 3.992 0.251 0.455 1.098 0.583 0.182 0.753 0.109 1.095 15.113 | 15.150<br>53.811<br>7.527<br>0.448<br>0.374<br>1.358<br>0.775<br>0.302<br>0.358<br>0.300<br>2.119<br>16.120 | 15.273<br>64.103<br>8.200<br>0.369<br>0.546<br>1.958<br>0.177<br>0.<br>0.602<br>0.<br>1.555<br>4.819 | 16.442 62.911 3.434 1.075 0.415 1.216 0.147 0. 0.450 0.214 1.609 11.288 |
| 13  | 1.050   | 0.867  | 0.424  | 0.672   | 1.381  | 0.471   |
| 14  | 0.404   | 0.310  | 0.488  | 0.687   | 1.018  | 0.327   |

## (b)Bridge Drainage Cost-Resp.(%) for 1985/86

| Vehicle                              | Int.  | Int.  | State   | State   | County  | City  |
|--------------------------------------|---|---|---|---|---|---|
| Class                                | Rural   | Urban   | Primary   | Second.   | Roads   | Streets   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 | 12.761<br>39.851<br>2.687<br>0.408<br>0.917<br>0.483<br>0.406<br>0.054<br>0.323 | 16.948<br>51.826<br>3.389<br>0.593<br>0.709<br>0.598<br>0.400<br>0.308<br>0.242 | 17.159 58.273 3.874 0.243 0.455 1.082 0.589 0.182 0.754 | 15.156<br>53.833<br>7.319<br>0.435<br>0.374<br>1.350<br>0.785<br>0.303<br>0.360 | 15.273<br>64.103<br>8.200<br>0.369<br>0.546<br>1.958<br>0.177<br>0. | 16.442<br>62.911<br>3.434<br>1.075<br>0.415<br>1.216<br>0.147<br>0. |
| 10                                   | 0.095   | 0.063   | 0.110   | 0.303   | 0.  | 0.214   |
| 11                                   | 3.345   | 1.642   | 1.105   | 2.140   | 1.555   | 1.609   |
| 12                                   | 37.212  | 22.097  | 15.254  | 16.274  | 4.819   | 11.288  |
| 13                                   | 1.056   | 0.873   | 0.427   | 0.677   | 1.381   | 0.471   |
| 14                                   | 0.400   | 0.311   | 0.491   | 0.691   | 1.018   | 0.327   |



Table I.25. Bridge Pile Cost-Responsibility Factors

# (a)Bridge Pile Cost-Resp.(%) for 1983

| Vehicle                         | Int.   | Int.   | State   | State   | County | City    |
|---------------------------------|--------|--------|---------|---------|--------|---------|
| Class                           | Rural  | Urban  | Primary | Second. | Roads  | Streets |
| 1 . 2 3 4 5 6 7 8 9 10 11 12 13 | 12.041 | 15.939 | 15.549  | 15.554  | 13.835 | 14.894  |
|                                 | 37.602 | 48.740 | 52.806  | 55.246  | 58.070 | 56.990  |
|                                 | 2.387  | 2.828  | 3.572   | 4.855   | 7.245  | 3.206   |
|                                 | 0.394  | 0.574  | 0.270   | 0.308   | 0.407  | 1.163   |
|                                 | 0.862  | 0.662  | 0.408   | 0.377   | 0.486  | 0.370   |
|                                 | 0.449  | 0.551  | 1.277   | 1.140   | 2.781  | 1.624   |
|                                 | 0.330  | 0.291  | 0.440   | 0.453   | 0.111  | 0.108   |
|                                 | 0.046  | 0.231  | 0.162   | 0.162   | 0.     | 0.      |
|                                 | 0.398  | 0.333  | 2.145   | 0.816   | 2.306  | 1.397   |
|                                 | 0.069  | 0.038  | 0.065   | 0.138   | 0.     | 0.111   |
|                                 | 2.914  | 1.383  | 0.778   | 1.321   | 1.219  | 1.299   |
|                                 | 39.917 | 26.035 | 19.988  | 16.980  | 7.992  | 16.674  |
|                                 | 1.155  | 1.048  | 0.516   | 0.461   | 1.522  | 0.509   |
| 14                              | 1.437  | 1.347  | 2.025   | 2.190   | 4.027  | 1.653   |

## (b)Bridge Pile Cost-Resp.(%) for 1985/86

| Vehicle | Int.   | Int.   | State   | State   | County | City    |
|---------|--------|--------|---------|---------|--------|---------|
| Class   | Rural  | Urban  | Primary | Second. | Roads  | Streets |
| 1       | 11.983 | 15.915 | 15.544  | 15.560  | 13.835 | 14.894  |
| 2       | 37.421 | 48.666 | 52.788  | 55.269  | 58.070 | 56.990  |
| 3       | 2.316  | 2.751  | 3.473   | 4.721   | 7.245  | 3.206   |
| 4       | 0.381  | 0.556  | 0.262   | 0.298   | 0.407  | 1.163   |
| 5       | 0.858  | 0.661  | 0.408   | 0.377   | 0.486  | 0.370   |
| 6       | 0.446  | 0.550  | 1.256   | 1.130   | 2.781  | 1.624   |
| 7       | 0.333  | 0.294  | 0.445   | 0.459   | 0.111  | 0.108   |
| 8       | 0.046  | 0.231  | 0.162   | 0.162   | 0.     | 0.      |
| 9       | 0.393  | 0.328  | 2.137   | 0.812   | 2.306  | 1.397   |
| 10      | 0.070  | 0.039  | 0.065   | 0.140   | 0.     | 0.111   |
| 11      | 2.935  | 1.393  | 0.787   | 1.333   | 1.219  | 1.299   |
| 12      | 40.245 | 26.218 | 20.129  | 17.084  | 7.992  | 16.674  |
| 13      | 1.160  | 1.052  | 0.519   | 0.465   | 1.522  | 0.509   |
| 14      | 1.413  | 1.346  | 2.026   | 2.189   | 4.027  | 1.653   |



Table I.26. Bridge Railing Cost-Responsibility Factors

## (a)Bridge Railing Cost-Resp.(%) for 1983

| Vehicle                                   | Int.   | Int.   | State   | State  | County   | City   |
|---|--|--|---|--|--|--|
| Class                                     | Rural  | Urban  | Primary   | Second.  | Roads  | Streets  |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9 | 5.473<br>17.092<br>2.333<br>0.441<br>0.392<br>0.466<br>0.310<br>0.030<br>6.640<br>0.066<br>3.255 | 7.245 22.155 3.924 0.844 0.301 0.797 0.401 0.204 6.866 0.052 2.104 | 7.068 24.003 5.552 0.433 0.185 2.129 0.708 0.172 13.744 0.100 1.255 | 7.070<br>25.112<br>8.603<br>0.519<br>0.171<br>2.138<br>0.855<br>0.212<br>8.242<br>0.237<br>2.518 | 6.289<br>26.395<br>13.723<br>0.689<br>0.221<br>5.339<br>0.220<br>0.<br>12.373<br>0.<br>2.496 | 6.770<br>25.905<br>6.121<br>2.016<br>0.168<br>3.210<br>0.218<br>0.<br>12.074<br>0.202<br>2.577 |
| 12  | 56.891   | 48.551   | 39.350  | 36.383   | 18.077   | 36.339   |
| 13  | 1.525  | 1.767  | 0.867   | 0.779  | 2.575  | 0.883  |
| 14  | 5.085  | 4.791  | 4.434   | 7.162  | 11.603   | 3.518  |

# (b)Bridge Railing Cost-Resp.(%) for 1985/86

| Vehicle<br>Class | Int.<br>Rural | Int.<br>Urban | State<br>Primary | State<br>Second. | County<br>Roads | City<br>Streets |
|------------------|---------------|---------------|------------------|------------------|-----------------|-----------------|
| 1                | 5.447         | 7.234         | 7.065            | 7.073            | 6.289           | 6.770           |
| 2                | 17.010        | 22.121        | 23.995           | 25.122           | 26.395          | 25.905          |
| 3                | 2.258         | 3.805         | 5.393            | 8.382            | 13.723          | 6.121           |
| 4                | 0.425         | 0.815         | 0.419            | 0.504            | 0.689           | 2.016           |
| 5                | 0.390         | 0.301         | 0.185            | 0.172            | 0.221           | 0.168           |
| 6                | 0.462         | 0.792         | 2.090            | 2.119            | 5.339           | 3.210           |
| 7                | 0.312         | 0.404         | 0.716            | 0.869            | 0.220           | 0.218           |
| 8                | 0.029         | 0.203         | 0.171            | 0.213            | 0.              | 0.              |
| 9                | 6.889         | 6.827         | 13.701           | 8.204            | 12.373          | 12.074          |
| 10               | 0.067         | 0.053         | 0.101            | 0.240            | 0.              | 0.202           |
| 11               | 3.264         | 2.112         | 1.267            | 2.542            | 2.496           | 2.577           |
| 12               | 57.173        | 48.751        | 39.575           | 36.596           | 18.077          | 36.339          |
| 13               | 1.526         | 1.768         | 0.871            | 0.785            | 2.575           | 0.883           |
| 14               | 4.750         | 4.813         | 4.450            | 7.183            | 11.603          | 3.518           |



Table I.27. Cost-Responsibility for State Highways (1983)\*

|             |       |           |           |       | C . I | * P       | -42414    |
|-------------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh         | Sub-  |           | nsibility | Veh   | Sub-  |           | Sub-Crown |
| Class       | Group | Veh Class | Sub-Group | CIASS | Group | Veh Class | Sub-Group |
|             |       | 202       | 11 202    | 11    | 6     |           | 0.336     |
| 1           | 1     | 11.303    | 11.303    | 11    | 7     |           | 0.121     |
|             |       |           |           |       |       |           |           |
| 2           | 1     | 40.460    | 40.460    | 11    | 8     |           | 0.153     |
|             |       |           |           | 11    | 9     |           | 0.126     |
| 3           | 1     | 4.591     | 0.377     | 11    | 10    |           | 0.153     |
| 3           | 2     |           | 0.214     | 11    | 11    |           | 0.180     |
| 3<br>3<br>3 | 3     |           | 0.641     | 11    | 12    |           | 0.203     |
| 3           | 4     |           | 0.651     | 11    | 13    |           | 0.403     |
| 3           | 5     |           | 0.352     |       |       |           |           |
| 3           | 6     |           | 0.982     | 12    | 1     | 36.035    | 0.022     |
| 3           | 7     |           | 0.709     | 12    | 2     |           | 0.086     |
| 3           | 8     |           | 0.280     | 12    | 3     |           | 0.327     |
| 3           | 9     |           | 0.385     | 12    | 4     |           | 1.093     |
|             |       |           |           | 12    | 5     |           | 0.560     |
| 4           | 1     | 0.223     | 0.223     | 12    | 6     |           | 0.586     |
|             |       |           |           | 12    | 7     |           | 0.248     |
| 5           | 1     | 0.384     | 0.384     | 12    | 8     |           | 0.373     |
| -           | -     | 0400.     |           | 12    | 9     |           | 0.616     |
| 6           | 1     | 1.267     | 0.207     | 12    | 10    |           | 0.667     |
| 6           | 2     | 1.207     | 0.144     | 12    | 11    |           | 0.363     |
|             | 3     |           | 0.105     | 12    | 12    |           | 0.469     |
| 6           | 4     |           |           | 12    | 13    |           | 0.622     |
| 6           |       |           | 0.129     |       |       |           |           |
| 6           | 5     |           | 0.051     | 12    | 14    |           | 0.680     |
| 6           | 6     |           | 0.058     | 12    | 15    |           | 0.756     |
| 6           | 7     |           | 0.071     | 12    | 16    |           | 0.968     |
| 6           | 8     |           | 0.103     | 12    | 17    |           | 1.240     |
| 6           | 9     |           | 0.401     | 12    | 18    |           | 3.402     |
|             |       |           |           | 12    | 19    |           | 2.177     |
| 7           | 1     | 1.486     | 0.041     | 12    | 20    |           | 4.024     |
| 7           | 2     |           | 0.049     | 12    | 21    |           | 6.224     |
| 7           | 3     |           | 0.072     | 12    | 22    |           | 4.882     |
| 7           | 4     |           | 0.106     | 12    | 23    |           | 4.310     |
| 7           | 5     |           | 0.116     | 12    | 24    |           | 0.917     |
| 7           |       |           |           | 12    | 25    |           | 0.174     |
|             | 6     |           | 0.211     |       |       |           | 0.249     |
| 7           | 7     |           | 0.239     | 12    | 26    |           | 0.249     |
| 7           | 8     |           | 0.297     |       |       |           | 0 115     |
| 7           | 9     |           | 0.356     | 13    | 1     | 0.741     | 0.115     |
|             |       |           |           | 13    | 2     |           | 0.142     |
| 8           | 1     | 0.119     | 0.119     | 13    | 3     |           | 0.110     |
|             |       |           |           | 13    | 4     |           | 0.078     |
| 9           | 1     | 0.527     | 0.017     | 13    | 5     |           | 0.078     |
| 9           | 2     |           | 0.510     | 13    | 6     |           | 0.016     |
|             |       |           |           | 13    | 7     |           | 0.028     |
| 10          | 1     | 0.153     | 0.027     | 13    | 8     |           | 0.015     |
| 10          | 2     | 01133     | 0.033     | 13    | 9     |           | 0.015     |
| 10          | 3     |           | 0.040     | 13    | 10    |           | 0.027     |
| 10          | 4     |           | 0.052     | 13    | 11    |           | 0.017     |
| 10          | 4     |           | 0.052     | 13    | 12    |           | 0.044     |
|             |       | 0.054     | 0.053     |       |       |           | 0.054     |
| 11          | 1     | 2.256     | 0.053     | 13    | 13    |           | 0.034     |
| 11          | 2     |           | 0.099     |       |       | 0 /50     | 0.056     |
| 11          | 3     |           | 0.205     | 14    | 1     | 0.458     | 0.056     |
| 11          | 4     |           | 0.118     | 14    | 2     |           | 0.109     |
| 11          | 5     |           | 0.108     | 14    | 3     |           | 0.294     |

\*Costs do not include structure and enforcement costs



Table I.28. Cost-Responsibility for County Roads (1983)\*

|       |       |           | 41.484    |       |       | ~   | _     |           |
|-------|-------|-----------|-----------|-------|-------|-----|-------|-----------|
| Veh   | Sub-  |           | nsibility | Veh   | Sub-  |     |       | nsibility |
| CLASS | Group | ven Class | Sub-Group | Class | Group | Ven | Class | Sub-Group |
| 1     | 1     | 5.806     | 5.806     | 11    | 6     |     |       | 0.733     |
| •     | *     | 3.000     | 3.000     | 11    | 7     |     |       | 0.226     |
| 2     | 1     | 30.494    | 30.494    | 11    | 8     |     |       | 0.317     |
| ~     |       | 30.434    | 30.434    | 11    | 9     |     |       | 0.205     |
| 3     | 1     | 15.174    | 0.457     | 11    |       |     |       |           |
|       |       | 15.1/4    |           |       | 10    |     |       | 0.262     |
| 3     | 2     |           | 0.884     | 11    | 11    |     |       | 0.331     |
| 3     | 3     |           | 1.535     | 11    | 12    |     |       | 0.363     |
| 3     | 4     |           | 1.772     | 11    | 13    |     |       | 0.888     |
| 3     | 5     |           | 0.868     |       |       |     |       |           |
| 3     | 6     |           | 4.098     | 12    | 1     | 27  | .767  | 0.008     |
| 3     | 7     |           | 3.139     | 12    | 2     |     |       | 0.025     |
| 3     | 8     |           | 0.946     | 12    | 3     |     |       | 0.089     |
| 3     | 9     |           | 1.476     | 12    | 4     |     |       | 0.526     |
|       |       |           |           | 12    | 5     |     |       | 0.150     |
| 4     | 1     | 0.589     | 0.589     | 12    | 6     |     |       | 0.322     |
|       |       |           |           | 12    | 7     |     |       | 0.034     |
| 5     | 1     | 0.277     | 0.277     | 12    | 8     |     |       | 0.170     |
|       |       |           |           | 12    | 9     |     |       | 0.446     |
| 6     | 1     | 6.703     | 0.791     | 12    | 10    |     |       | 0.500     |
| 6     | 2     |           | 0.609     | 12    | 11    |     |       | 0.151     |
| 6     | 3     |           | 0.391     | 12    | 12    |     |       | 0.275     |
| 6     | 4     |           | 0.572     | 12    | 13    |     |       | 0.449     |
| 6     | 5     |           | 0.227     | 12    | 14    |     |       | 0.390     |
| 6     | 6     |           | 0.299     | 12    | 15    |     |       | 0.500     |
| 6     | 7     |           | 0.378     | 12    | 16    |     |       | 0.388     |
| 6     | 8     |           | 0.614     | 12    | 17    |     |       | 0.775     |
| 6     | 9     |           |           |       |       |     |       |           |
| О     | 9     |           | 2.823     | 12    | 18    |     |       | 3.352     |
| -     | ,     | 1 007     | 0.016     | 12    | 19    |     |       | 1.817     |
| 7     | 1     | 1.027     | 0.016     | 12    | 20    |     |       | 3.785     |
| 7     | 2     |           | 0.027     | 12    | 21    |     |       | 5.396     |
| 7     | 3     |           | 0.042     | 12    | 22    |     |       | 3.449     |
| 7     | 4     |           | 0.064     | 12    | 23    |     |       | 3.974     |
| 7     | 5     |           | 0.078     | 12    | 24    |     |       | 0.547     |
| 7     | 6     |           | 0.155     | 12    | 25    |     |       | 0.125     |
| 7     | 7     |           | 0.160     | 12    | 26    |     |       | 0.124     |
| 7     | 8     |           | 0.217     |       |       |     |       |           |
| 7     | 9     |           | 0.268     | 13    | 1     | 3   | .363  | 0.721     |
|       |       |           |           | 13    | 2     |     |       | 0.896     |
| 8     | 1     | 0.        | 0.        | 13    | 3     |     |       | 0.739     |
|       |       |           |           | 13    | 4     |     |       | 0.454     |
| 9     | 1     | 2.315     | 0.011     | 13    | 5     |     |       | 0.554     |
| 9     | 2     |           | 2.304     | 13    | 6     |     |       | 0.        |
|       |       |           |           | 13    | 7     |     |       | 0.        |
| 10    | 1     | 0.        | 0.        | 13    | 8     |     |       | 0.        |
| 10    | 2     |           | 0.        | 13    | 9     |     |       | 0.        |
| 10    | 3     |           | 0.        | 13    | 10    |     |       | 0.        |
| 10    | 4     |           | 0.        | 13    | 11    |     |       | 0.        |
|       |       |           |           | 13    | 12    |     |       | 0.        |
| 1.1   | 1     | 4.092     | 0.060     | 13    | 13    |     |       | 0.        |
| 11    | 2     |           | 0.136     |       |       |     |       |           |
| 11    | 3     |           | 0.284     | 14    | 1     | 2   | .392  | 0.227     |
| 11    | 4     |           | 0.173     | 14    | 2     |     |       | 0.545     |
| 11    | 5     |           | 0.115     | 14    | 3     |     |       | 1.620     |
|       | _     |           |           |       |       |     |       |           |

<sup>\*</sup>Costs do not include structure and enforcement costs



Table I.29. Cost-Responsibility for City Streets (1983)\*

|       |       |           |           | 67 1  | C     | *       | Page  | neibility |
|-------|-------|-----------|-----------|-------|-------|---------|-------|-----------|
| Veh   | Sub-  | % Respon  | neibility | Veh   | Sub-  | 17 n ln | Class | Sub-Group |
| Class | Group | Veh Class | Sub-Group | CTSBB | Group | v∈u.    | Class | Sub-Group |
|       | ,     | 10.266    | 10 266    | 11    | 6     |         |       | 0.414     |
| 1     | 1     | 10.366    | 10.366    | 11    | 7     |         |       | 0.126     |
|       |       |           |           |       | 8     |         |       | 0.172     |
| 2     | 1     | 41.629    | 41.629    | 11    |       |         |       | 0.109     |
|       |       |           |           | 11    | 9     |         |       |           |
| 3     | 1     | 3.619     | 0.338     | 11    | 10    |         |       | 0.139     |
| 3     | 2     |           | 0.287     | 11    | 11    |         |       | 0.174     |
| 3     | 3     |           | 0.527     | 11    | 12    |         |       | 0.184     |
| 3     | 4     |           | 0.458     | 11    | 13    |         |       | 0.447     |
| 3     | 5     |           | 0.188     |       |       |         |       |           |
| 3     | 6     |           | 0.804     | 12    | 1     | 36      | .485  | 0.017     |
| 3     | 7     |           | 0.578     | 12    | 2     |         |       | 0.045     |
| 3     | 8     |           | 0.174     | 12    | 3     |         |       | 0.151     |
| 3     | 9     |           | 0.266     | 12    | 4     |         |       | 0.838     |
|       | ,     |           |           | 12    | 5     |         |       | 0.227     |
| 4     | 1     | 0.999     | 0.999     | 12    | 6     |         |       | 0.478     |
| 4     |       | 0.337     | 0.,,,     | 12    | 7     |         |       | 0.050     |
| 5     | 1     | 0.276     | 0.276     | 12    | 8     |         |       | 0.242     |
| )     | 1     | 0.270     | 0.270     | 12    | 9     |         |       | 0.625     |
| ,     |       | 0.126     | 0.322     | 12    | 10    |         |       | 0.688     |
| 6     | 1     | 2.136     |           | 12    | 11    |         |       | 0.206     |
| 6     | 2     |           | 0.244     | 12    | 12    |         |       | 0.371     |
| 6     | . 3   |           | 0.137     | 12    | 13    |         |       | 0.603     |
| 6     | 4     |           | 0.188     | 12    | 14    |         |       | 0.519     |
| 6     | 5     |           | 0.069     |       | 15    |         |       | 0.663     |
| 6     | 6     |           | 0.089     | 12    |       |         |       | 0.509     |
| 6     | 7     |           | 0.111     | 12    | 16    |         |       | 1.016     |
| 6     | 8     |           | 0.173     | 12    | 17    |         |       |           |
| 6     | 9     |           | 0.802     | 12    | 18    |         |       | 4.376     |
|       |       |           |           | 12    | 19    |         |       | 2.363     |
| 7     | 1     | 0.414     | 0.009     | 12    | 20    |         |       | 4.913     |
| 7     | 2     |           | 0.014     | 12    | 21    |         |       | 6.985     |
| 7     | 3     |           | 0.019     | 12    | 22    |         |       | 4.456     |
| 7     | 4     |           | 0.028     | 12    | 23    |         |       | 5.125     |
| 7     | 5     |           | 0.033     | 12    | 24    |         |       | 0.705     |
| 7     | 6     |           | 0.061     | 12    | 25    |         |       | 0.161     |
| 7     | 7     |           | 0.063     | 12    | 26    |         |       | 0.156     |
| 7     | 8     |           | 0.084     |       |       |         |       |           |
| 7     | 9     |           | 0.103     | 13    | 1     | (       | .618  | 0.137     |
| ,     | ,     |           | 0.100     | 13    | 2     |         |       | 0.167     |
| 8     | 1     | 0.        | 0.        | 13    | 3     |         |       | 0.135     |
| 0     |       | •         | •         | 13    | 4     |         |       | 0.081     |
| 9     | 1     | 0.747     | 0.007     | 13    | 5     |         |       | 0.098     |
| 9     | 2     | 0.747     | 0.740     | 13    | 6     |         |       | 0.        |
| ,     | 4     |           | 0.740     | 13    | 7     |         |       | 0.        |
| 10    | ,     | 0.144     | 0.026     | 13    | 8     |         |       | 0.        |
| 10    | 1     | 0.144     |           | 13    | 9     |         |       | 0.        |
| 10    | 2     |           | 0.032     | 13    | 10    |         |       | 0.        |
| 10    |       |           |           | 13    | 11    |         |       | 0.        |
| 10    | 4     |           | 0.050     | 13    | 12    |         |       | 0.        |
|       |       | 0.071     | 0.057     | 13    | 13    |         |       | 0.        |
| 11    | 1     | 2.271     | 0.056     | 13    | 13    |         |       |           |
| 11    | 2     |           | 0.094     | 14    | 1     |         | 0.297 | 0.031     |
| 11    | 3     |           | 0.180     |       | 2     |         | 0.471 | 0.069     |
| 11    | 4     |           | 0.107     | 14    |       |         |       | 0.009     |
| 11    | 5     |           | 0.069     | 14    | 3     |         |       | U . 1 7 / |

<sup>\*</sup>Costs do not include structure and enforcement costs.



Table I.30. Cost-Responsibility for Bridges on State Highways (1983)

| Veh   | Sub-  | % Respon  | nsibility |   | Veh   | Sub-  | 7 Kes   | ponsibility<br>ss Sub-Group |
|-------|-------|-----------|-----------|---|-------|-------|---------|-----------------------------|
| Class | Group | Veh Class | Sub-Group |   | Class | Group | AGU CIS | iss Sub-Group               |
|       |       |           |           |   | 11    | 6     |         | 0.210                       |
| 1     | 1     | 15.468    | 15.468    |   | 11    | 7     |         | 0.112                       |
|       |       |           |           |   |       | 8     |         | 0.107                       |
| 2     | 1     | 53.114    | 53.114    |   | 11    |       |         | 0.093                       |
|       |       |           |           |   | 11    | 9     |         |                             |
| 3     | 1     | 4.165     | 0.629     |   | 11    | 10    |         | 0.088                       |
| 3     | 2     |           | 0.295     |   | 11    | 11    |         | 0.107                       |
| 3     | 3     |           | 0.840     |   | 11    | 12    |         | 0.102                       |
| 3     | 4     |           | 0.631     |   | 11    | 13    |         | 0.151                       |
| 3     | 5     |           | 0.374     |   |       |       |         |                             |
| 3     | 6     |           | 0.619     |   | 12    | 1     | 19.62   |                             |
| 3     | 7     |           | 0.415     |   | 12    | 2     |         | 0.118                       |
| 3     | 8     |           | 0.150     |   | 12    | 3     |         | 0.408                       |
| 3     | 9     |           | 0.213     |   | 12    | 4     |         | 1.504                       |
| 3     | 7     |           | 0.213     |   | 12    | 5     |         | 0.770                       |
| ,     | 1     | 0.277     | 0.277     |   | 12    | 6     |         | 0.707                       |
| 4     | 1     | 0.2//     | 0.277     |   | 12    | 7     |         | 0.343                       |
| _     |       | 0 500     | 0.500     |   | 12    | 8     |         | 0.399                       |
| 5     | 1     | 0.598     | 0.598     |   | 12    | 9     |         | 0.692                       |
|       |       |           | 0 107     |   | 12    | 10    |         | 0.631                       |
| 6     | 1     | 0.950     | 0.197     |   | 12    | 11    |         | 0.363                       |
| 6     | 2     |           | 0.128     |   | 12    | 12    |         | 0.396                       |
| 6     | 3     |           | 0.085     |   | 12    | 13    |         | 0.535                       |
| 6     | 4     |           | 0.090     |   |       | 14    |         | 0.512                       |
| 6     | 5     |           | 0.039     |   | 12    | _     |         | 0.544                       |
| 6     | 6     |           | 0.049     |   | 12    | 15    |         | 0.587                       |
| 6     | 7     |           | 0.050     |   | 12    | 16    |         | 0.628                       |
| 6     | 8     |           | 0.050     |   | 12    | 17    |         | 1.278                       |
| 6     | 9     |           | 0.261     |   | 12    | 18    |         | 0.847                       |
|       |       |           |           |   | 12    | 19    |         |                             |
| 7     | 1     | 0.453     | 0.038     |   | 12    | 20    |         | 1.358<br>2.743              |
| 7     | 2     |           | 0.036     |   | 12    | 21    |         |                             |
| 7     | 3     |           | 0.042     |   | 12    | 22    |         | 1.998                       |
| 7     | 4     |           | 0.056     |   | 12    | 23    |         | 1.674                       |
| 7     | 5     |           | 0.042     |   | 12    | 24    |         | 0.378                       |
| 7     | 6     |           | 0.050     |   | 12    | 25    |         | 0.071                       |
| 7     | 7     |           | 0.075     |   | 12    | 26    |         | 0.106                       |
| 7     | 8     |           | 0.061     |   |       |       |         |                             |
| 7     | 9     |           | 0.054     |   | 13    | 1     | 0.54    | 49 0.111                    |
| •     | -     |           |           |   | 13    | 2     |         | 0.125                       |
| 8     | 1     | 0.175     | 0.175     |   | 13    | 3     |         | 0.064                       |
| 0     | -     |           |           |   | 13    | 4     |         | 0.045                       |
| 9     | 1     | 1.154     | 0.033     |   | 13    | 5     |         | 0.036                       |
| ģ     | 2     |           | 1.121     |   | 13    | 6     |         | 0.010                       |
| ,     | _     |           |           |   | 13    | 7     |         | 0.026                       |
| 10    | 1     | 0.126     | 0.036     |   | 13    | 8     |         | 0.013                       |
| 10    | 2     | 0.110     | 0.036     |   | 13    | 9     |         | 0.013                       |
| 10    | 3     |           | 0.029     |   | 13    | 10    |         | 0.024                       |
| 10    | 4     |           | 0.025     |   | 13    | 11    |         | 0.013                       |
| 10    | 4     |           | 0.023     |   | 13    | 12    |         | 0.036                       |
| 11    | 1     | 1.627     | 0.082     |   | 13    | 13    |         | 0.036                       |
|       | 2     | 1.02/     | 0.099     |   | -     |       |         |                             |
| 11    | 3     |           | 0.237     |   | 14    | 1     | 1.7     | 39 0.075                    |
| 11    |       |           | 0.237     | - | 14    | 2     |         | 0.343                       |
| 11    | 4     |           |           |   | 14    | 3     |         | 1.321                       |
| 11    | 5     |           | 0.121     |   | 7-4   | ,     |         |                             |



Table L.31. Cost-Responsibility for Bridges on County Roads (1983)

| Veh    | Sub-   |           | onsibility     | Veh      | Sub-     | I Respon  | sibility  |
|--------|--------|-----------|----------------|----------|----------|-----------|-----------|
| Class  | Group  | Veh Class | Sub-Group      | Class    | Group    | Ven Class | Jub Group |
| 1      | 1      | 14.537    | 14.537         | 11       | 6        |           | 0.178     |
| •      | -      |           |                | 11       | 7        |           | 0.069     |
| 2      | 1      | 61.016    | 61.016         | 11       | 8        |           | 0.069     |
| -      | -      |           |                | 11       | 9        |           | 0.039     |
| 3      | 1      | 7.126     | 1.174          | 11       | 10       |           | 0.039     |
| 3      | 2      | ,         | 0.419          | 11       | 11       |           | 0.063     |
| 3      | 3      |           | 1.491          | 11       | 12       |           | 0.063     |
| 3      | 4      |           | 0.853          | 11       | 13       |           | 0.154     |
| 3      | 5      |           | 0.486          |          |          |           |           |
| 3      | 6      |           | 1.222          | 12       | 1        | 6.303     | 0.008     |
| 3      | 7      |           | 0.864          | 12       | 2        |           | 0.017     |
| 3      | 8      |           | 0.222          | 12       | 3        |           | 0.050     |
| 3      | 9      |           | 0.396          | 12       | 4        |           | 0.379     |
| _      |        |           |                | 12       | 5        |           | 0.084     |
| 4      | 1      | 0.314     | 0.314          | 12       | 6        |           | 0.174     |
|        |        |           |                | 12       | 7        |           | 0.016     |
| 5      | 1      | 0.603     | 0.603          | 12       | 8        |           | 0.064     |
|        |        |           |                | 12       | 9        |           | 0.224     |
| 6      | 1      | 2.460     | 0.419          | 12       | 10       |           | 0.200     |
| 6      | 2      |           | 0.299          | 12       | 11       |           | 0.055     |
| 6      | 3      |           | 0.165          | 12       | 12       |           | 0.083     |
| 6      | 4      |           | 0.165          | 12       | 13       |           | 0.179     |
| 6      | 5      |           | 0.069          | 12       | 14       |           | 0.134     |
| 6      | 6      |           | 0.122          | 12       | 15       |           | 0.148     |
| 6      | 7      |           | 0.122          | 12       | 16       |           | 0.099     |
| 6      | 8      |           | 0.135          | 12       | 17       |           | 0.166     |
| 6      | 9      |           | 0.963          | 12       | 18       |           | 0.602     |
|        |        |           |                | 12       | 19       |           | 0.557     |
| 7      | 1      | 0.116     | 0.009          | 12       | 20       |           | 1.211     |
| 7      | 2      |           | 0.009          | 12       | 21<br>22 |           | 0.664     |
| 7      | 3      |           | 0.009          | 12<br>12 | 23       |           | 0.747     |
| 7      | 4      |           | 0.012          | 12       | 24       |           | 0.090     |
| 7      | 5      |           | 0.010          | 12       | 25       |           | 0.020     |
| 7      | 6      |           | 0.016<br>0.016 | 12       | 26       |           | 0.020     |
| 7      | 7      |           | 0.018          | 12       | 20       |           |           |
| 7<br>7 | 8<br>9 |           | 0.018          | 13       | 1        | 1.132     | 0.340     |
| /      | ,      |           | 0.010          | 13       | 2        |           | 0.340     |
| 8      | 1      | 0.        | 0.             | 13       | 3        |           | 0.226     |
| 0      |        | 0.        | •              | 13       | 4        |           | 0.113     |
| 9      | 1      | 2.076     | 0.078          | 13       | 5        |           | 0.113     |
| 9      | 2      | 2.0.0     | 1.998          | 13       | 6        |           | 0.        |
| ,      | _      |           |                | 13       | 7        |           | 0.        |
| 10     | 1      | 0.        | 0.             | 13       | 8        |           | 0.        |
| 10     | 2      |           | 0.             | 13       | 9        |           | 0.        |
| 10     | 3      |           | 0.             | 13       | 10       |           | 0.        |
| 10     | 4      |           | 0.             | 13       | 11       |           | 0.        |
|        |        |           |                | 13       | 12       |           | 0.        |
| 11     | 1      | 1.096     | 0.070          | 13       | 13       |           | 0.        |
| 11     | 2      |           | 0.070          |          |          |           | 0.100     |
| 11     | 3      |           | 0.157          | 14       | 1        | 3.229     | 0.189     |
| 11     | 4      |           | 0.079          | 14       | 2        |           | 0.971     |
| 11     | 5      |           | 0.045          | 14       | 3        |           | 2.009     |
|        |        |           |                |          |          |           |           |



Table I.32. Cost-Responsibility for Bridges on City Streets (1983)

| Veh   | Sub-  | % Respo   | nsibility | Veh | Sub-     | % Respon  | nsibility |
|-------|-------|-----------|-----------|-----|----------|-----------|-----------|
| Class | Group | Veh Class | Sub-Group | C1a | ss Group | Veh Class | Sub-Group |
|       |       |           |           |     |          |           |           |
| 1     | 1     | 15.405    | 15.405    | 11  |          |           | 0.215     |
|       |       |           |           | 11  | 7        |           | 0.079     |
| 2     | 1     | 58.942    | 58.942    | 11  | 8        |           | 0.079     |
|       |       |           |           | 11  | 9        |           | 0.043     |
| 3     | 1     | 3.428     | 0.641     | 11  |          |           | 0.043     |
| 3     | 2     | 34120     | 0.229     | 11  |          |           | 0.062     |
| 3     | 3     |           | 0.791     | 11  |          |           | 0.062     |
| 3     | 4     |           | 0.452     | 11  |          |           | 0.142     |
| 2     | 5     |           | 0.432     | 11  | 13       |           | 0.142     |
| 3     | )     |           |           | 1.0 |          | 1/ 100    | 0.020     |
| 3     | 6     |           | 0.535     | 12  |          | 14.198    | 0.028     |
| 3     | 7     |           | 0.343     | 12  |          |           | 0.056     |
| 3     | 8     |           | 0.088     | 12  |          |           | 0.166     |
| 3     | 9     |           | 0.136     | 12  |          |           | 1.121     |
|       |       |           |           | 12  |          |           | 0.249     |
| 4     | 1     | 1.006     | 1.006     | 12  |          |           | 0.493     |
|       |       |           |           | 12  | . 7      |           | 0.045     |
| 5     | 1     | 0.453     | 0.453     | 12  |          |           | 0.181     |
|       | _     |           |           | 12  |          |           | 0.600     |
| 6     | I     | 1.576     | 0.336     | 12  |          |           | 0.538     |
| 6     | 2     | 1.570     | 0.240     | 12  |          |           | 0.144     |
| 6     | 3     |           | 0.121     | 12  |          |           | 0.217     |
|       | 4     |           | 0.121     | 12  |          |           | 0.417     |
| 6     | 4     |           |           | 12  |          |           |           |
| 6     | 5     |           | 0.045     |     |          |           | 0.313     |
| 6     | 6     |           | 0.073     | 12  |          |           | 0.335     |
| 6     | 7     |           | 0.073     | 12  |          |           | 0.223     |
| 6     | 8     |           | 0.079     | 12  |          |           | 0.359     |
| 6     | 9     |           | 0.486     | 12  |          |           | 1.300     |
|       |       |           |           | 12  |          |           | 0.647     |
| 7     | I     | 0.116     | 0.010     | 12  | 20       |           | 1.156     |
| 7     | 2     |           | 0.010     | 12  | 21       |           | 2.433     |
| 7     | 3     |           | 0.010     | 12  | 22       |           | 1.335     |
| 7     | 4     |           | 0.013     | 12  | 23       |           | 1.555     |
| 7     | 5     |           | 0.010     | 12  | 24       |           | 0.186     |
| 7     | 6     |           | 0.015     | 12  | 25       |           | 0.050     |
| 7     | 7     |           | 0.015     | 12  | 26       |           | 0.050     |
| 7     | 8     |           | 0.016     |     |          |           |           |
| 7     | 9     |           | 0.016     | 13  | 1        | 0.424     | 0.127     |
| ,     | ,     |           | 0.010     | 13  | _        | 0 4 1 2 1 | 0.127     |
| 8     | 1     | 0.        | 0.        | 13  |          |           | 0.085     |
| 0     | 1     | 0.        | 0.        | 13  |          |           | 0.042     |
|       |       | 1 000     | 0         |     |          |           | 0.042     |
| 9     | 1     | 1.903     | 0.        | 13  |          |           |           |
| 9     | 2     |           | 1.903     | 13  |          |           | 0.        |
|       |       |           |           | 13  |          |           | 0.        |
| 10    | 1     | 0.124     | 0.037     | 13  |          |           | 0.        |
| 10    | 2     |           | 0.037     | 13  |          |           | 0.        |
| 10    | 3     |           | 0.025     | 13  |          |           | 0.        |
| 10    | 4     |           | 0.025     | 13  |          |           | 0.        |
|       |       |           |           | 13  |          |           | 0.        |
| 11    | 1     | 1.274     | 0.099     | 13  | 13       |           | 0.        |
| 11    | 2     |           | 0.099     |     |          |           |           |
| 11    | 3     |           | 0.198     | 14  | 1        | 1.351     | 0.047     |
| 11    | 4     |           | 0.099     | 14  | . 2      |           | 0.226     |
| 11    | 5     |           | 0.054     | 14  |          |           | 1.078     |
|       |       |           |           | •   |          |           |           |



Table L-33. Cost-Responsibility for Sign Bridges (1983)

| Veh         Sub-         X         Responsibility         Veh         Sub-         X         Responsibility           1         1         1.1.475         11.475         11.6         6         9.245           2         1         41.353         41.353         11.7         9         0.158           3         1         5.732         0.795         11.1         10         0.138           3         2         0.437         11.1         11         0.249           3         3         0.920         11.1         12         0.233           3         4         0.775         11.1         13         0.233           3         5         0.686         3         0.293         12         1         33.029         0.055           3         7         0.517         12         2         0.228         0.228           3         8         0.293         12         3         3.029         0.055           3         7         0.519         12         4         1         0.650         0.650         12         6         0.228           3         8         0.293         12         3   |       |       |           |           | ** 1  | C 1   | * n       |           |
|---|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| 1         1         11.475         11.475         11         6         0.245           2         1         41.353         41.353         11         8         0.150           3         1         5.732         0.795         11         10         0.138           3         2         0.437         11         11         0.249           3         3         0.920         11         12         0.233           3         4         0.775         11         13         0.238           3         5         0.686         3         6         0.791         12         1         33.029         0.055           3         7         0.517         12         2         0.228         3         0.238         3         0.0293         12         3         0.850         0.228         3         9         0.519         12         4         1.287         0.228         3         9         0.519         12         4         1.287         0.286         12         6         0.9956         0.228         12         12         3         0.850         12         12         6         0.9956         0.286         12  | Veh   | Sub-  |           |           | Veh   | Sub-  |           |           |
| 2 1 41.353 41.353 11 7 0.158 2 1 41.353 41.353 11 8 0.150 3 1 5.732 0.795 11 10 0.138 3 2 0.437 11 11 11 0.249 3 3 3 0.920 11 12 0.233 3 4 0.775 11 13 0.233 3 5 0.686 3 6 0.791 12 1 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.956 5 1 0.374 0.374 12 8 0.605 5 1 0.374 0.374 12 8 0.605 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 23 1.865 7 5 0.096 12 16 1.867 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 23 1.865 7 5 0.099 12 24 0.666 7 7 0.096 12 16 1.867 7 1 0.472 0.037 12 20 2.386 7 7 0.096 12 15 1.322 6 7 0.096 12 15 1.322 6 7 0.096 12 15 1.322 7 1 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.099 12 24 0.666 7 7 0.096 12 15 1.322 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.666 7 7 0.095 12 26 0.666 7 7 0.096 13 1 1.103 0.175 7 8 0.059 7 9 0.046 13 1 1.103 0.175 7 8 0.059 7 9 0.046 13 1 1.103 0.175 9 1 0.661 0.133 13 5 0.092 10 1 0.113 0.027 13 8 0 0.039 10 2 0.033 13 10 0.007 11 1 2 0.580 0.039 10 1 0.113 0.027 13 8 0 0.039 10 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.0092 11 1 1 2.540 0.126 13 13 11 0.039 11 1 1 0.0175 14 2 0.035 | Class | Group | Veh Class | Sub-Group | Class | Group | ven Class | 300-G100p |
| 2 1 41.353 41.353 11 7 0.158 2 1 41.353 41.353 11 8 0.150 3 1 5.732 0.795 11 10 0.138 3 2 0.437 11 11 11 0.249 3 3 3 0.920 11 12 0.233 3 4 0.775 11 13 0.233 3 5 0.686 3 6 0.791 12 1 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.956 5 1 0.374 0.374 12 8 0.605 5 1 0.374 0.374 12 8 0.605 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 23 1.865 7 5 0.096 12 16 1.867 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 23 1.865 7 5 0.099 12 24 0.666 7 7 0.096 12 16 1.867 7 1 0.472 0.037 12 20 2.386 7 7 0.096 12 15 1.322 6 7 0.096 12 15 1.322 6 7 0.096 12 15 1.322 7 1 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.099 12 24 0.666 7 7 0.096 12 15 1.322 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.666 7 7 0.095 12 26 0.666 7 7 0.096 13 1 1.103 0.175 7 8 0.059 7 9 0.046 13 1 1.103 0.175 7 8 0.059 7 9 0.046 13 1 1.103 0.175 9 1 0.661 0.133 13 5 0.092 10 1 0.113 0.027 13 8 0 0.039 10 2 0.033 13 10 0.007 11 1 2 0.580 0.039 10 1 0.113 0.027 13 8 0 0.039 10 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.007 11 1 2 0.033 13 10 0.0092 11 1 1 2.540 0.126 13 13 11 0.039 11 1 1 0.0175 14 2 0.035 | ,     | ,     | 11 475    | 11 475    | 1.1   | 6     |           | 0.245     |
| 2 1 41.353 41.353 11 8 0.150 3 1 5.732 0.795 11 10 0.138 3 2 0.437 11 11 0.249 3 3 3 0.920 11 12 0.233 3 4 0.775 11 13 0.238 3 5 0.686 3 6 0.791 12 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.956 5 1 0.374 0.374 12 8 0.665 5 1 0.374 0.374 12 8 0.665 6 2 0.217 12 10 0.865 6 2 0.217 12 11 0.686 6 3 0.245 12 10 0.865 6 4 0.240 12 13 1.173 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.842 0.661 6 8 0.066 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 2 18 2.030 7 2 0.046 12 18 2.039 7 3 0.033 12 22 3.391 7 4 0.071 12 22 3.391 7 5 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.391 7 4 0.071 12 22 3.391 7 5 0.099 12 24 0.666 7 7 0.096 12 16 1.867 7 8 0.099 12 24 0.666 7 7 0.096 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.391 7 4 0.071 12 23 3.391 7 4 0.071 12 23 3.869 7 7 9 0.046 12 18 2.030 8 1 0.168 0.168 13 3 0.092 7 8 0.099 12 24 0.666 7 7 0.095 12 26 0.081 7 7 9 0.046 13 1 1.103 0.175 9 2 0.528 13 6 0.092 10 3 0.033 13 10 0.077 9 1 0.661 0.133 13 5 0.092 10 3 0.033 13 10 0.077 11 2 0.528 13 6 0.092 11 1 2.540 0.126 13 13 1 0.0039 10 2 0.528 13 6 0.0039 11 1 2.540 0.126 13 13 10 0.0074 11 1 2.5540 0.126 13 13 10 0.0092 11 1 2 0.106   | 1     | i     | 11.4/5    | 11.473    |       |       |           |           |
| 1   |       |       | / 1 252   | (1 252    |       |       |           |           |
| 3         1         5.732         0.795         11         10         0.138           3         2         0.437         11         11         12         0.239           3         3         0.920         11         12         0.238           3         4         0.775         11         13         0.238           3         5         0.686         3         6         0.791         12         1         33.029         0.055           3         6         0.791         12         2         0.228         0.228           3         8         0.293         12         3         0.850         0.228           3         8         0.293         12         4         2.132         0.850           3         9         0.519         12         4         2.132         0.286           4         1         0.650         0.650         12         6         0.7956           5         1         0.374         0.374         12         8         0.655           5         1         0.374         0.351         12         10         0.865           6         1 <th>2</th> <th>1</th> <th>41.353</th> <td>41.333</td> <td></td> <td></td> <td></td> <td></td>   | 2     | 1     | 41.353    | 41.333    |       |       |           |           |
| 3 2 0.437 11 11 12 0.243 3 3 0.920 11 12 0.233 3 4 0.775 11 13 0.238 3 5 0.686 3 6 0.791 12 1 2 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.955 5 1 0.374 0.374 12 8 0.655 5 1 0.374 0.374 12 8 0.665 6 2 0.217 12 12 10 0.865 6 2 0.217 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 4 0.240 12 13 1.173 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.842 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.036 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 11 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 7 0.095 12 24 0.666 7 7 0.095 12 25 0.081 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.0072 11 1 2.540 0.126 13 13 11 0.0486 0.095 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.0074 11 1 2.540 0.126 13 13 11 0.486 0.095 11 1 1 2.540 0.126 13 13 13 0.106   |       |       |           |           |       | -     |           |           |
| 3 3 0.920 11 12 0.233 3 4 0.775 11 13 0.238 3 5 0.686 3 6 0.791 12 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.956 5 1 0.374 0.374 12 8 0.605 5 1 0.374 0.374 12 8 0.665 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.865 6 3 0.245 12 12 0.661 6 4 0.240 12 13 0.689 6 5 0.078 12 14 1.11 0.668 6 6 0.090 12 15 1.332 6 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 12 13 1.610 6 9 0.046 12 18 2.030 7 8 0.059 7 9 0.046 12 12 23 1.865 7 6 0.095 12 24 0.666 7 7 6 0.095 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 8 0.059 12 24 0.666 7 9 0.046 13 1 0.103 0.175 8 1 0.113 0.027 13 8 0.039 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.007 11 1 2.540 0.126 13 13 1 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 0.106   |       |       | 5.732     |           |       |       |           |           |
| 3 4 0.775 11 13 0.238 3 5 0.686 3 6 0.791 12 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.956 5 1 0.374 0.374 12 8 0.667 5 1 0.374 0.374 12 8 0.668 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.090 12 15 1.322 6 7 0.096 12 16 1.867 7 0.096 12 16 1.867 7 0.096 12 17 1.610 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.661 7 7 0.095 12 24 0.661 7 7 0.095 12 24 0.668 7 6 0.046 12 25 0.081 7 7 1 0.472 0.037 12 20 2.386 7 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.0143 7 8 0.059 7 9 1 0.661 0.133 13 5 0.200 8 1 0.113 0.027 13 8 0.039 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.092 11 1 2.540 0.126 13 13 1 0.0486 0.099 11 1 1 2.540 0.126 13 13 10 0.0099 11 1 2.540 0.126 13 13 10 0.0099 11 1 2.540 0.126 13 13 10 0.0099 11 1 2.540 0.126 13 13 10 0.0099 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.175 14 2 0.0995  |       |       |           |           |       |       |           |           |
| 3 5 0.686 3 3 6 0.791 12 1 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 7.956 5 1 0.374 0.374 12 8 0.605 5 1 0.374 0.374 12 8 0.605 6 2 0.217 12 11 0.685 6 2 0.217 12 11 0.685 6 3 0.245 12 12 0.666 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 1 0.472 0.037 12 20 2.386 7 1 0.472 0.037 12 20 2.386 7 7 2 0.026 12 15 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 9 0.046 12 25 0.081 7 8 0.059 7 9 1 0.661 0.133 13 5 0.290 9 1 0.661 0.133 13 5 0.092 9 1 0.661 0.133 13 5 0.092 10 1 0.113 0.027 13 8 0.092 10 1 0.113 0.027 13 8 0.093 10 2 0.027 13 9 0.039 10 2 0.033 13 10 0.097 11 1 2.540 0.126 13 13 10 0.095 11 1 2.540 0.126 13 13 10 0.095 11 2 19 0.486 0.095 11 2 19 0.486 0.095 11 2 10 0.486 0.095 11 2 10 0.486 0.095 11 2 10 0.486 0.095   | 3     |       |           |           |       |       |           |           |
| 3         5         0.686           3         6         0.791         12         1         33.029         0.055           3         7         0.517         12         2         0.228           3         8         0.293         12         3         0.850           3         9         0.519         12         4         2.132           4         1         0.650         0.650         12         6         7.956           5         1         0.374         0.374         12         8         0.605           5         1         0.374         0.374         12         9         0.924           6         1         1.842         0.351         12         10         0.865           6         2         0.217         12         11         0.689           6         3         0.245         12         12         0.661           6         2         0.278         12         12         0.661           6         4         0.240         12         13         1.173           6         5         0.078         12         14         1.343 </th <th>3</th> <th>4</th> <th></th> <th>0.775</th> <th>11</th> <th>13</th> <th></th> <th>0.238</th>  | 3     | 4     |           | 0.775     | 11    | 13    |           | 0.238     |
| 3 6 0.791 12 13 33.029 0.055 3 7 0.517 12 2 0.228 3 8 0.293 12 3 0.850 3 9 0.519 12 4 2.132 4 1 0.650 0.650 12 6 0.587 5 1 0.374 0.374 12 8 0.605 5 1 0.374 0.374 12 9 0.924 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 10 0.865 6 4 0.240 12 11 0.689 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 12 13 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 24 0.666 7 7 0.095 12 24 0.666 7 7 0.095 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 9 1 0.661 0.133 13 5 0.092 10 1 0.168 0.168 13 3 3 0.092 11 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.071 11 1 2.540 0.126 13 13 10 0.039 10 3 0.033 13 10 0.097 11 1 2.540 0.126 13 13 10 0.039 10 3 0.033 13 10 0.007 11 1 2.540 0.126 13 13 10 0.007 11 1 2.540 0.126 13 13 10 0.007 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.007 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 3 0.330 14 1 0.486 0.095 11 1 4 0.175 14 2  | 3     | 5     |           | 0.686     |       |       |           |           |
| 3       7       0.517       12       2       0.228         3       8       0.293       12       3       0.850         3       9       0.519       12       4       2.132         4       1       0.650       0.650       12       5       1.287         5       1       0.374       0.374       12       8       0.605         5       1       0.374       12       8       0.605         6       1       1.842       0.351       12       10       0.865         6       2       0.217       12       11       0.689         6       3       0.245       12       12       0.661         6       4       0.240       12       13       1.173         6       5       0.078       12       14       1.343         6       6       0.090       12       15       1.322         6       7       0.096       12       16       1.867         6       8       0.086       12       17       1.610         8       0.440       12       18       2.030         9   | 3     | 6     |           | 0.791     | 12    |       | 33.029    |           |
| 3       8       0.293       12       3       0.850         3       9       0.519       12       4       2.132         4       1       0.650       0.650       12       6       0.996         5       1       0.374       0.374       12       8       0.605         6       1       1.842       0.351       12       10       0.865         6       2       0.217       12       11       0.689         6       3       0.245       12       12       0.661         6       4       0.240       12       13       1.173         6       5       0.078       12       14       1.343         6       6       0.090       12       15       1.322         6       7       0.096       12       16       1.867         6       8       0.086       12       17       1.610         6       9       0.440       12       18       2.030         12       19       1.684       1.684       1.610       1.687         7       2       0.026       12       21       3.391       1.  |       | 7     |           | 0.517     | 12    | 2     |           | 0.228     |
| 1   |       | 8     |           | 0.293     | 12    | 3     |           | 0.850     |
| 12 5 1.287 4 1 0.650 0.650 12 6 7.956 5 1 0.374 0.374 12 8 0.605 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 12 0.661 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 17 1.610 6 9 0.440 12 18 2.030 17 4 0.037 12 20 2.386 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 8 0.059 12 24 0.666 7 7 7 0.095 12 24 0.666 7 7 8 0.059 12 24 0.666 7 7 9 0.046 12 25 0.081 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 1 0.661 0.133 13 5 0.055 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.077 10 4 0.037 13 9 0.039 10 3 0.033 13 10 0.0052 11 1 2.540 0.126 13 13 10 0.0093 11 1 2.5540 0.126 13 13 12 0.106 11 2 0.170 11 2 13 11 0.486 0.095 11 1 1 0.475 0.330 14 1 0.486 0.095 11 1 1 0.475 0.175   |       |       |           |           | 12    | 4     |           | 2.132     |
| 4         1         0.650         0.650         12         6         0.587           5         1         0.374         0.374         12         8         0.605           5         1         0.374         12         8         0.605           6         1         1.842         0.351         12         10         0.865           6         2         0.217         12         11         0.669           6         3         0.245         12         12         0.661           6         4         0.240         12         13         1.173           6         5         0.078         12         14         1.343           6         6         0.090         12         15         1.322           6         7         0.096         12         16         1.867           6         8         0.086         12         17         1.610           6         9         0.440         12         18         2.030           12         19         1.684         2.030         12         18         2.030           7         1         0.472         0.037  | -     |       |           |           | 12    | 5     |           | 1.287     |
| 5         1         0.374         0.374         12         8         0.605           6         1         1.842         0.351         12         10         0.865           6         2         0.217         12         11         0.689           6         3         0.245         12         12         0.6661           6         4         0.240         12         13         1.173           6         5         0.078         12         14         1.343           6         6         0.090         12         15         1.322           6         7         0.096         12         16         1.867           6         8         0.096         12         17         1.610           6         9         0.440         12         18         2.030           7         1         0.472         0.037         12         20         2.386           7         2         0.026         12         21         19         1.684           7         1         0.472         0.037         12         20         2.386           7         2         0.026  | /.    | 1     | 0.650     | 0.650     |       |       |           |           |
| 5         1         0.374         0.374         12         8         0.605           6         1         1.842         0.351         12         10         0.865           6         2         0.217         12         11         0.689           6         3         0.245         12         12         0.661           6         4         0.240         12         13         1.173           6         5         0.078         12         14         1.343           6         6         0.090         12         15         1.322           6         7         0.096         12         16         1.867           6         8         0.086         12         17         1.610           6         9         0.440         12         18         2.030           12         19         1.684         1         2.07         1         1.610         1         1.610         1         1         1.610         1         1         1.610         1         1         1.610         1         1         1.610         1         1         1.610         1         1         1.610   | -4    | 1     | 0.030     | 0.030     |       |       |           |           |
| 12   9   0.924  | -     | 1     | 0.374     | 0.37/     |       |       |           |           |
| 6 1 1.842 0.351 12 10 0.865 6 2 0.217 12 11 0.689 6 3 0.245 12 12 12 0.661 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 3.629 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 7 0.095 12 26 0.081 7 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.200 9 1 0.661 0.133 13 5 0.0052 9 2 0.528 13 6 0.0052 9 2 0.528 13 6 0.0052 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.007 11 1 2.540 0.126 13 13 10 0.039 10 2 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 8 0.039 10 2 0.033 13 10 0.095 11 1 2.540 0.126 13 13 13 0.0066 11 1 0.175 13 12 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095 11 1 2.540 0.126 13 13 10 0.0095   | )     | 1     | 0.3/4     | 0.374     |       |       |           |           |
| 6 2 0.217 12 11 0.689 6 3 0.245 12 12 12 0.661 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 24 0.666 7 7 0.095 12 25 0.081 7 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 1 0.661 0.133 13 5 0.092 10 1 0.113 0.027 13 8 0.092 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 2 0.027 13 10 0.039 11 1 2.540 0.126 13 11 0.486 0.095 11 1 0.175 14 2 0.196  |       |       |           | 0.251     |       |       |           |           |
| 6 3 0.245 12 12 0.661 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 24 0.666 7 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 8 1 0.168 0.168 13 3 0.092 9 2 0.528 13 6 0.095 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.027 11 1 2.540 0.126 13 11 0.486 0.095 11 1 2.540 0.126 13 13 1 0.0095 11 1 0.175 14 2 0.095   |       |       | 1.842     |           |       |       |           |           |
| 6 4 0.240 12 13 1.173 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 24 0.666 7 7 8 0.095 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.200 9 1 0.661 0.133 13 5 0.092 10 1 0.113 0.027 13 8 0.039 10 2 0.025 10 3 0.033 13 10 0.039 10 4 0.027 13 18 0.039 10 2 0.027 13 18 0.039 10 1 0.113 0.027 13 18 0.039 10 1 0.113 0.027 13 10 0.039 10 2 0.027 13 11 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 13 0.106 11 1 2.540 0.126 13 13 13 0.106 11 1 0.330 14 1 0.486 0.995 11 1 1 0.330 14 1 0.486 0.995 11 1 1 0.330 14 1 0.486 0.995 11 1 1 0.175 14 2  |       |       |           |           |       |       |           |           |
| 6 5 0.078 12 14 1.343 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.0959 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.200 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.077 10 4 0.027 13 9 0.039 10 1 2.540 0.126 13 13 1 0.009 11 1 2.540 0.126 13 13 10 0.072 11 1 2.540 0.126 13 13 10 0.095 11 1 4 0.330 14 1 0.486 0.095 11 1 1 0.330 14 1 0.486 0.095 11 1 1 0.330 14 1 0.486 0.095   |       |       |           |           |       |       |           |           |
| 6 6 6 0.090 12 15 1.322 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 24 0.666 7 8 0.059 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 2 0.528 13 6 0.025 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.077 11 1 2.540 0.126 13 13 10 0.073 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2 0.175 14 2 0.486 0.095 11 1 4 0.175 14 2  | 6     |       |           |           |       |       |           |           |
| 6 7 0.096 12 16 1.867 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 18 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.007 11 1 0.330 14 1 0.486 0.095 11 1 4 0.175 14 2  | 6     | 5     |           | 0.078     |       |       |           |           |
| 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.200 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.027 10 4 0.027 13 11 0.039 10 3 0.033 13 10 0.039 11 1 2.540 0.126 13 11 0.039 11 1 2.540 0.126 13 13 10 0.039 11 2 0.330 14 1 0.486 0.095 11 1 0.330 14 1 0.486 0.095 11 1 2 0.330 14 1 0.486 0.095 11 1 4 0.330 14 1 0.486 0.095   | 6     | 6     |           | 0.090     |       | 15    |           |           |
| 6 8 0.086 12 17 1.610 6 9 0.440 12 18 2.030 12 19 1.684 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.033 13 10 0.025 10 3 0.033 13 10 0.039 10 2 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 12 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095  | 6     | 7     |           | 0.096     | 12    | 16    |           | 1.867     |
| 6       9       0.440       12       18       2.030         7       1       0.472       0.037       12       20       2.386         7       2       0.026       12       21       3.629         7       3       0.033       12       22       3.391         7       4       0.071       12       23       1.865         7       5       0.059       12       24       0.666         7       6       0.046       12       25       0.081         7       7       0.095       12       26       0.143         7       8       0.059       12       26       0.143         7       9       0.046       13       1       1.103       0.175         8       1       0.168       13       3       0.092         9       2       0.528       13       4       0.077         9       1       0.661       0.133       13       5       0.052         9       2       0.528       13       6       0.052         10       1       0.113       0.027       13       8       0.039  |       |       |           | 0.086     | 12    | 17    |           | 1.610     |
| 7       1       0.472       0.037       12       20       2.386         7       2       0.026       12       21       3.629         7       3       0.033       12       22       3.391         7       4       0.071       12       23       1.865         7       5       0.059       12       24       0.666         7       6       0.046       12       25       0.081         7       7       0.095       12       26       0.143         7       8       0.059       12       26       0.143         7       9       0.046       13       1       1.103       0.175         8       1       0.168       13       3       0.200         8       1       0.168       13       3       0.092         9       2       0.661       0.133       13       4       0.077         9       1       0.661       0.133       13       5       0.052         9       2       0.528       13       6       0.025         13       7       0.080         10       2   |       |       |           |           | 12    | 18    |           | 2.030     |
| 7 1 0.472 0.037 12 20 2.386 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 3 0.092 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.0095 11 2 0.330 14 1 0.466 0.095 11 1 0.330 14 1 0.466 0.095 11 1 0.330 14 1 0.466 0.095 11 1 0.175   | U     | ,     |           | 0         |       | 19    |           | 1.684     |
| 7 2 0.026 12 21 3.629 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 12 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 1 4 0.330 14 1 0.486 0.095   | 7     | 1     | 0 472     | 0.037     |       |       |           |           |
| 7 3 0.033 12 22 3.391 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 2 0.528 13 6 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 12 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 1 4 0.330 14 1 0.486 0.095 11 1 4 0.330 14 1 0.486 0.095   | 7     |       | 0.4/2     |           |       |       |           |           |
| 7 4 0.071 12 23 1.865 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.092 9 2 0.528 13 6 0.055 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 0.330 14 1 0.486 0.095 11 1 0.330 14 1 0.486 0.095 11 1 0.330 14 1 0.486 0.095  | 7     |       |           |           |       |       |           |           |
| 7 5 0.059 12 24 0.666 7 6 0.046 12 25 0.081 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 2 0.200 8 1 0.661 0.133 13 4 0.077 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.052 9 2 0.528 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 0.170 11 0.170 11 2 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 4 0.376   |       |       |           |           |       |       |           |           |
| 7 6 0.046 12 25 0.081 7 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 8 1 0.168 0.168 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.052 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 10 0.039 11 1 0.170 11 2 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 4 0.175  |       |       |           |           |       |       |           |           |
| 7 7 7 0.095 12 26 0.143 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 4 0.077 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.330 14 1 0.486 0.095 11 4 0.175 14 2 0.196  | /     |       |           |           |       |       |           |           |
| 7 8 0.059 7 9 0.046 13 1 1.103 0.175 13 2 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 8 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.375 14 2 0.196   |       |       |           |           |       |       |           |           |
| 7 9 0.046 13 1 1.103 0.175 0.200 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.074 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.376   |       |       |           |           | 12    | 20    |           | 0.143     |
| 8 1 0.168 0.168 13 3 0.092 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.039 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 1 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.175 14 2 0.196  |       |       |           |           |       | ,     | 1 102     | 0.175     |
| 8     1     0.168     0.168     13     3     0.092       9     1     0.661     0.133     13     5     0.052       9     2     0.528     13     6     0.025       10     1     0.113     0.027     13     8     0.039       10     2     0.027     13     9     0.039       10     3     0.033     13     10     0.07-       10     4     0.027     13     11     0.039       10     4     0.027     13     11     0.039       11     1     2.540     0.126     13     13     0.106       11     2     0.170     11     0.330     14     1     0.486     0.095       11     4     0.175     14     2     0.196   | 7     | 9     |           | 0.046     |       |       | 1.103     |           |
| 13 4 0.077 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.07- 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.466 0.095 11 4 0.175 14 2 0.196   |       |       |           |           |       |       |           |           |
| 9 1 0.661 0.133 13 5 0.052 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.074 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.175 14 2 0.196  | 8     | 1     | 0.168     | 0.168     |       |       |           |           |
| 9 2 0.528 13 6 0.025 13 7 0.080 10 1 0.113 0.027 13 8 0.039 10 2 0.027 13 9 0.039 10 3 0.033 13 10 0.07- 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.175 14 2 0.196   |       |       |           |           |       |       |           |           |
| 13 7 0.080  10 1 0.113 0.027 13 8 0.039  10 2 0.027 13 9 0.039  10 3 0.033 13 10 0.074  10 4 0.027 13 11 0.039  11 1 2.540 0.126 13 13 0.106  11 2 0.170  11 3 0.330 14 1 0.486 0.095  11 4 0.175 14 2 0.196  | 9     | 1     | 0.661     | 0.133     | 13    |       |           |           |
| 10     1     0.113     0.027     13     8     0.039       10     2     0.027     13     9     0.039       10     3     0.033     13     10     0.07.4       10     4     0.027     13     11     0.039       11     1     2.540     0.126     13     13     0.106       11     2     0.170     11     0.486     0.095       11     3     0.330     14     1     0.486     0.095       11     4     0.175     14     2     0.196   | 9     | 2     |           | 0.528     | 13    |       |           |           |
| 10 2 0.027 13 9 0.039<br>10 3 0.033 13 10 0.07-<br>10 4 0.027 13 11 0.039<br>11 1 2.540 0.126 13 13 0.106<br>11 2 0.170<br>11 3 0.330 14 1 0.466 0.095<br>11 4 0.175 14 2 0.196   |       |       |           |           | 13    | 7     |           | 0.080     |
| 10 2 0.027 13 9 0.039<br>10 3 0.033 13 10 0.07-<br>10 4 0.027 13 11 0.039<br>11 1 2.540 0.126 13 13 0.106<br>11 2 0.170<br>11 3 0.330 14 1 0.486 0.095<br>11 4 0.175 14 2 0.196   | 10    | 1     | 0.113     | 0.027     | 13    | 8     |           |           |
| 10 3 0.033 13 10 0.07- 10 4 0.027 13 11 0.039 11 1 2.540 0.126 13 13 0.106 11 2 0.170 11 3 0.330 14 1 0.486 0.095 11 4 0.175 14 2 0.196   |       |       |           |           | 13    | 9     |           | 0.039     |
| 10 4 0.027 13 11 0.039<br>11 1 2.540 0.126 13 13 0.106<br>11 2 0.170<br>11 3 0.330 14 1 0.486 0.095<br>11 4 0.175 14 2 0.196  |       |       |           |           |       |       |           | 0.07-     |
| 13 12 0.106<br>11 1 2.540 0.126 13 13 0.106<br>11 2 0.170<br>11 3 0.330 14 1 0.486 0.095<br>11 4 0.175 14 2 0.196   |       |       |           |           |       |       |           | 0.039     |
| 11     1     2.540     0.126     13     13     0.106       11     2     0.170       11     3     0.330     14     1     0.486     0.095       11     4     0.175     14     2     0.196   | 10    | *1    |           | 0.021     |       |       |           |           |
| 11 2 0.170<br>11 3 0.330 14 1 0.486 0.095<br>11 4 0.175 14 2 0.196  | 1.1   | 1     | 2 540     | 0 126     |       |       |           |           |
| 11 3 0.330 14 1 0.486 0.095<br>11 4 0.175 14 2 0.196  |       |       | 2.340     |           | 13    | 4.5   |           |           |
| 11 4 0.175 14 2 0.196   |       |       |           |           | 1.1   | 1     | 0.486     | 0.095     |
| 11 4 0.175  |       |       |           |           |       |       | U.400     |           |
| 11 5 0.182 14 3 0.196   |       |       |           |           |       |       |           |           |
|   | 11    | 5     |           | 0.182     | 14    | 3     |           | 0.170     |



Table 1.34. Cost-Responsibility for Police Enforcement (1983)

|       |       |           |           |       |       | # D       |           |
|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh   | Sub-  |           | nsibility | Veh   | Sub-  |           | nsibility |
| Class | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
|       |       | 10 13/    | 19.124    | 11    | 6     |           | 0.087     |
| 1     | 1     | 19.124    | 19.124    | 11    | 7     |           | 0.040     |
|       |       |           |           |       | 8     |           | 0.038     |
| 2     | 1     | 68.921    | 68.921    | 11    |       |           |           |
|       |       |           |           | 11    | 19    |           | 0.037     |
| 3     | 1     | 2.666     | 0.506     | 11    | 10    |           | 0.035     |
| 3     | 2     |           | 0.278     | 11    | 11    |           | 0.034     |
| 3     | 3     |           | 0.585     | 11    | 12    |           | 0.032     |
| 3     | 4     |           | 0.493     | 11    | 13    |           | 0.033     |
| 3     | 5     |           | 0.245     |       |       |           |           |
| 3     | 6     |           | 0.282     | 12    | 1     | 6.385     | 0.020     |
| 3     | 7     |           | 0.131     | 12    | 2     |           | 0.081     |
| 3     | 8     |           | 0.074     | 12    | 3     |           | 0.303     |
| 3     | 9     |           | 0.072     | 12    | 4     |           | 0.761     |
| 3     | 9     |           | 0.072     | 12    | 5     |           | 0.459     |
|       |       | 0.167     | 0.167     | 12    | 6     |           | 0.341     |
| 4     | 1     | 0.164     | 0.164     | 12    | 7     |           | 0.210     |
|       |       |           |           |       |       |           | 0.216     |
| 5     | 1     | 0.623     | 0.623     | 12    | 8     |           |           |
|       |       |           |           | 12    | 9     |           | 0.234     |
| 6     | 1     | 0.692     | 0.223     | 12    | 10    |           | 0.219     |
| 6     | 2     |           | 0.138     | 12    | 11    |           | 0.174     |
| 6     | 3     |           | 0.088     | 12    | 12    |           | 0.167     |
| 6     | 4     |           | 0.086     | 12    | 13    |           | 0.162     |
| 6     | 5     |           | 0.028     | 12    | 14    |           | 0.185     |
| 6     | 6     |           | 0.023     | 12    | 15    |           | 0.182     |
| 6     | 7     |           | 0.024     | 12    | 16    |           | 0.258     |
|       | 8     |           | 0.022     | 12    | 17    |           | 0.222     |
| 6     |       |           |           | 12    | 18    |           | 0.280     |
| 6     | 9     |           | 0.061     |       | 19    |           | 0.232     |
|       |       |           |           | 12    |       |           | 0.329     |
| 7     | 1     | 0.196     | 0.024     | 12    | 20    |           |           |
| 7     | 2     |           | 0.017     | 12    | 21    |           | 0.501     |
| 7     | 3     |           | 0.021     | 12    | 22    |           | 0.468     |
| 7     | 4     |           | 0.025     | 12    | 23    |           | 0.257     |
| 7     | 5     |           | 0.021     | 12    | 24    |           | 0.092     |
| 7     | 6     |           | 0.017     | 12    | 25    |           | 0.011     |
| 7     | 7     |           | 0.034     | 12    | 26    |           | 0.020     |
| 7     | 8     |           | 0.021     |       |       |           |           |
| 7     | 9     |           | 0.017     | 13    | 1     | 0.22-     | 0.044     |
| •     |       |           |           | 13    | 2     |           | 0.051     |
| 8     | 1     | 0.107     | 0.107     | 13    | 3     |           | 0.023     |
| ()    | •     | .,        | 0         | 13    | 4     |           | 0.020     |
| 9     | 1     | 0.091     | 0.018     | 13    | 5     |           | 0.013     |
| 9     | 2     | 0.071     | 0.073     | 13    | 6     |           | 0.006     |
| 7     | 4     |           | 0.073     | 13    | 7     |           | 0.011     |
|       |       | 0.010     | 0.010     |       | 8     |           | 0.005     |
| 10    | 1     | 0.040     | 0.010     | 13    | 9     |           | 0.005     |
| 10    | 2     |           | 0.010     | 13    |       |           | 0.000     |
| 10    | 3     |           | 0.012     | 13    | 10    |           |           |
| 10    | 4     |           | 0.010     | 13    | 11    |           | 0.005     |
|       |       |           |           | 13    | 12    |           | 0.015     |
| 11    | 1     | 0.688     | 0.045     | 13    | 13    |           | 0.015     |
| 11    | 2     |           | 0.061     |       |       |           |           |
| 11    | 3     |           | 0.118     | 14    | 1     | 0.078     | 0.024     |
| 11    | 4     |           | 0.062     | 14    | 2     |           | 0.027     |
| 11    | 5     |           | 0.065     | 14    | 3     |           | 0.027     |
| 11    | ,     |           | 0.000     |       |       |           |           |



Table I.35. Weigh Station Inspection Cost-Responsibility for Trucks (1983)

|       |       |           |           | 47 - 1- | C I.  | *   | Ponno | nsibility |
|-------|-------|-----------|-----------|---------|-------|-----|-------|-----------|
| Veh   | Sub-  |           | sibility  | Veh     | Sub-  |     |       | Sub-Group |
| Class | Group | Veh Class | Sub-Group | Class   | Group | ven | CIASS | 3do-Group |
|       |       | 0         | 0         | 11      | 6     |     |       | 0.780     |
| 1     | 1     | 0.        | 0.        | 11      | 7     |     |       | 0.275     |
|       |       |           |           |         | 8     |     |       | 0.265     |
| 2     | 1     | 0.        | 0.        | 11      |       |     |       | 0.240     |
|       |       |           |           | 11      | 9     |     |       |           |
| 3     | 1     | 27.156    | 4.912     | 11      | 10    |     |       | 0.228     |
| 3     | 2     |           | 3.040     | 11      | 1.1   |     |       | 0.219     |
| 3     | 3     |           | 5.901     | 11      | 12    |     |       | 0.207     |
| 3     | 4     |           | 5.025     | 11      | 13    |     |       | 0.233     |
| 3     | 5     |           | 2.638     |         |       |     |       |           |
| 3     | 6     |           | 2.791     | 12      | 1     | 54  | .179  | 0.188     |
| 3     | 7     |           | 1.329     | 12      | 2     |     |       | 0.803     |
| 3     | 8     |           | 0.818     | 12      | 3     |     |       | 3.182     |
| 3     | 9     |           | 0.705     | 12      | 4     |     |       | 6.951     |
| 3     | 9     |           | 0.703     | 12      | 5     |     |       | 3.791     |
|       |       |           | 0         | 12      | 6     |     |       | 2.942     |
| 4     | 1     | 0.        | 0.        | 12      | 7     |     |       | 1.590     |
|       |       |           | _         | 12      | 8     |     |       | 1.776     |
| 5     | 1     | 0.        | 0.        |         | 9     |     |       | 1.970     |
|       |       |           |           | 12      |       |     |       | 1.883     |
| 6     | 1     | 6.212     | 2.049     | 12      | 10    |     |       |           |
| 6     | 2     |           | 1.134     | 12      | 11    |     |       | 1.477     |
| 6     | 3     |           | 0.932     | 12      | 12    |     |       | 1.362     |
| 6     | 4     |           | 0.824     | 12      | 13    |     |       | 1.371     |
| 6     | 5     |           | 0.224     | 12      | 14    |     |       | 1.610     |
| 6     | 6     |           | 0.191     | 12      | 15    |     |       | 1.446     |
| 6     | 7     |           | 0.217     | 12      | 16    |     |       | 2.351     |
|       | 8     |           | 0.200     | 12      | 17    |     |       | 1.924     |
| 6     |       |           | 0.441     | 12      | 18    |     |       | 2.601     |
| 6     | 9     |           | 0.441     | 12      | 19    |     |       | 1.912     |
|       |       |           |           | 12      | 20    |     |       | 2.573     |
| 7     | 1     | 2.826     | 0.398     |         |       |     |       | 4.064     |
| 7     | 2     |           | 0.265     | 12      | 21    |     |       | 3.531     |
| 7     | 3     |           | 0.291     | 12      | 22    |     |       | 2.055     |
| 7     | 4     |           | 0.319     | 12      | 23    |     |       |           |
| 7     | 5     |           | 0.305     | 12      | 24    |     |       | 0.580     |
| 7     | 6     |           | 0.277     | 12      | 25    |     |       | 0.107     |
| 7     | 7     |           | 0.388     | 12      | 26    |     |       | 0.154     |
| 7     | 8     |           | 0.305     |         |       |     |       |           |
| 7     | 9     |           | 0.277     | 13      | 1     | ]   | .675  | 0.367     |
| ·     | -     |           |           | 13      | 2     |     |       | 0.373     |
| 8     | 1     | 0.        | 0.        | 13      | 3     |     |       | 0.191     |
| · ·   | •     | •         | - •       | 13      | 4     |     |       | 0.151     |
| 9     | 1     | 0.929     | 0.163     | 13      | 5     |     |       | 0.097     |
| 9     | 2     | 0.727     | 0.767     | 13      | 6     |     |       | 0.054     |
| 9     | 2     |           | 0.707     | 13      | 7     |     |       | 0.082     |
|       |       | 0 101     | 0.110     | 13      | 8     |     |       | 0.038     |
| 10    | 1     | 0.486     | 0.118     | 13      | 9     |     |       | 0.038     |
| 10    | 2     |           | 0.118     |         |       |     |       | 0.067     |
| 10    | 3     |           | 0.131     | 13      | 10    |     |       | 0.038     |
| 10    | 4     |           | 0.118     | 13      | 11    |     |       |           |
|       |       |           |           | 13      | 12    |     |       | 0.090     |
| 11    | 1     | 5.744     | 0.440     | 13      | 13    |     |       | 0.090     |
| 11    | 2     |           | 0.624     |         |       |     |       |           |
| 11    | 3     |           | 1.079     | 14      | 1     | 1   | 0.792 | 0.253     |
| 11    | 4     |           | 0.625     | 14      | 2     |     |       | 0.269     |
| 11    | 5     |           | 0.529     | 14      | 3     |     |       | 0.269     |
| 1.1   | ,     |           | 0.55      |         |       |     |       |           |



Table 1.36. Cost-Responsibility for State Highways (1985-86)\*

| Veh   | Sub-   | 7 Respon  | nsibility | Veh   | Sub-  | 7    | Respor | nsibility  |
|-------|--------|-----------|-----------|-------|-------|------|--------|------------|
|       |        | Veh Class |           |       |       |      |        | Sub-Group  |
| Class | Group  | ven class | Sub-Group | CIASS | Group | 1011 | 01000  | 345 GE 345 |
| 1     | 1      | 12.439    | 12.439    | 11    | 6     |      |        | 0.249      |
| 1     | 1      | 12.437    | 120737    | 11    | 7     |      |        | 0.110      |
| 2     | 1      | 43.225    | 43.225    | 11    | 8     |      |        | 0.128      |
| 4-    | 1      | 40.225    | 77.225    | 11    | 9     |      |        | 0.126      |
| 3     | 1      | 3.564     | 0.317     | 11    | 10    |      |        | 0.149      |
| 3     | 2      | 3.304     | 0.212     | 11    | 11    |      |        | 0.168      |
| 3     | 3      |           | 0.505     | 11    | 12    |      |        | 0.180      |
|       | _      |           | 0.553     | 11    | 13    |      |        | 0.288      |
| 3     | 4<br>5 |           | 0.346     | 4.1   | 13    |      |        | 0.200      |
|       |        |           |           | 12    | 1     | 27   | .205   | 0.025      |
| 3     | 6      |           | 0.635     | 12    | 2     | 34   | . 203  | 0.113      |
| 3     | 7      |           | 0.453     |       | 3     |      |        |            |
| 3     | 8      |           | 0.237     | 12    |       |      |        | 0.442      |
| 3     | 9      |           | 0.308     | 12    | 4     |      |        | 1.228      |
|       |        |           |           | 12    | 5     |      |        | 0.779      |
| 4     | 1      | 0.214     | 0.214     | 12    | 6     |      |        | 0.635      |
|       |        |           |           | 12    | 7     |      |        | 0.381      |
| 5     | 1      | 0.475     | 0.475     | 12    | 8     |      |        | 0.448      |
|       |        |           |           | 12    | 9     |      |        | 0.576      |
| 6     | 1      | 0.986     | 0.181     | 12    | 10    |      |        | 0.612      |
| 6     | 2      |           | 0.117     | 12    | 11    |      |        | 0.454      |
| 6     | 3      |           | 0.101     | 12    | 12    |      |        | 0.512      |
| 6     | 4      |           | 0.118     | 12    | 13    |      |        | 0.599      |
| 6     | 5      |           | 0.046     | 12    | 14    |      |        | 0.735      |
| 6     | 6      |           | 0.047     | 12    | 15    |      |        | 0.787      |
| 6     | 7      |           | 0.057     | 12    | 16    |      |        | 1.209      |
| 6     | 8      |           | 0.074     | 12    | 17    |      |        | 1.297      |
| 6     | 9      |           | 0.245     | 12    | 18    |      |        | 2.563      |
|       |        |           |           | 12    | 19    |      |        | 1.938      |
| 7     | 1      | 0.991     | 0.038     | 12    | 20    |      |        | 3.285      |
| 7     | 2      |           | 0.038     | 12    | 21    |      |        | 5.478      |
| 7     | 3      |           | 0.055     | 12    | 22    |      |        | 4.995      |
| 7     | 4      |           | 0.078     | 12    | 23    |      |        | 3.652      |
| 7     | 5      |           | 0.086     | 12    | 24    |      |        | 1.050      |
| 7     | 6      |           | 0.131     | 12    | 25    |      |        | 0.151      |
| 7     | 7      |           | 0.171     | 12    | 26    |      |        | 0.261      |
| 7     | 8      |           | 0.185     |       |       |      |        |            |
| 7     | 9      |           | 0.209     | 13    | 1     | 0    | .837   | 0.098      |
|       |        |           |           | 13    | 2     |      |        | 0.120      |
| 8     | 1      | 0.118     | 0.118     | 13    | 3     |      |        | 0.105      |
|       |        |           |           | 13    | 4     |      |        | 0.082      |
| 9     | 1      | 0.489     | 0.025     | 13    | 5     |      |        | 0.063      |
| 9     | 2      |           | 0.464     | 13    | 6     |      |        | 0.032      |
|       |        |           |           | 13    | 7     |      |        | 0.051      |
| 10    | 1      | 0.110     | 0.021     | 13    | 8     |      |        | 0.023      |
| 10    | 2      |           | 0.024     | 13    | 9     |      |        | 0.026      |
| 10    | 3      |           | 0.031     | 13    | 10    |      |        | 0.046      |
| 10    | 4      |           | 0.035     | 13    | 11    |      |        | 0.029      |
| -     |        |           |           | 13    | 12    |      |        | 0.073      |
| 11    | 1      | 1.993     | 0.049     | 13    | 13    |      |        | 0.090      |
| 11    | 2      |           | 0.090     |       |       |      |        |            |
| 11    | 3      |           | 0.207     | 14    | 1     | 0    | .355   | 0.050      |
| 11    | 4      |           | 0.117     | 14    | 2     |      |        | 0.088      |
| 11    | 5      |           | 0.133     | 14    | 3     |      |        | 0.217      |
|       |        |           |           |       |       |      |        |            |

<sup>\*</sup>Costs do not include structure and enforcement costs



Table I.37. Cost-Responsibility for County Roads (1985-86)\*

| Veh   | Sub-  | % Respon  | nsibility | Veh   | Sub-  |           | nsibility |
|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Class | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
| Class | Group | Ven Oldbo | 000 01004 |       |       |           |           |
| 1     | 1     | 5.812     | 5.812     | 11    | 6     |           | 0.641     |
| 1     | 1     | 3.012     | 2 40 2 2  | 11    | 7     |           | 0.195     |
|       | 1     | 28.778    | 28.778    | 11    | 8     |           | 0.273     |
| 2     | 1     | 20.//0    | 20.770    | 11    | 9     |           | 0.181     |
|       |       |           | 0 (15     | 11    | 10    |           | 0.231     |
| 3     | 1     | 10.882    | 0.415     |       |       |           | 0.291     |
| 3     | 2     |           | 0.240     | 11    | 11    |           | 0.361     |
| 3     | 3     |           | 1.228     | 11    | 12    |           |           |
| 3     | 4     |           | 1.354     | 11    | 13    |           | 0.879     |
| 3     | 5     |           | 0.650     |       |       |           |           |
| 3     | 6     |           | 3.000     | 12    | 1     | 37.686    | 0.012     |
| 3     | 7     |           | 2.284     | 12    | 2     |           | 0.034     |
|       | 8     |           | 0.680     | 12    | 3     |           | 0.125     |
| 3     |       |           | 1.031     | 12    | 4     |           | 0.732     |
| 3     | 9     |           | 1.031     | 12    | 5     |           | 0.211     |
|       |       |           |           | 12    | 6     |           | 0.448     |
| 4     | 1     | 0.371     | 0.371     |       |       |           | 0.049     |
|       |       |           |           | 12    | 7     |           |           |
| 5     | 1     | 0.255     | 0.255     | 12    | 8     |           | 0.239     |
|       |       |           |           | 12    | 9     |           | 0.627     |
| 6     | 1     | 4.626     | 0.543     | 12    | 10    |           | 0.706     |
|       | 2     | 4.020     | 0.441     | 12    | 11    |           | 0.209     |
| 6     |       |           | 0.277     | 12    | 12    |           | 0.386     |
| 6     | 3     |           |           | 12    | 13    |           | 0.629     |
| 6     | 4     |           | 0.387     |       |       |           | 0.573     |
| 6     | 5     |           | 0.158     | 12    | 14    |           |           |
| 6     | 6     |           | 0.207     | 12    | 15    |           | 0.678     |
| 6     | 7     |           | 0.261     | 12    | 16    |           | 0.534     |
| 6     | 8     |           | 0.421     | 12    | 17    |           | 1.077     |
| 6     | 9     |           | 1.932     | 12    | 18    |           | 4.598     |
| O     | ,     |           | 1 0,552   | 12    | 19    |           | 2.480     |
| -     |       | 1 751     | 0.029     | 12    | 20    |           | 5.115     |
| 7     | 1     | 1.751     |           | 12    | 21    |           | 7.257     |
| 7     | 2     |           | 0.046     | 12    | 22    |           | 4.616     |
| 7     | 3     |           | 0.073     |       | 23    |           | 5.287     |
| 7     | 4     |           | 0.115     | 12    |       |           | 0.717     |
| 7     | 5     |           | 0.125     | 12    | 24    |           |           |
| 7     | 6     |           | 0.261     | 12    | 25    |           | 0.163     |
| 7     | 7     |           | 0.271     | 12    | 26    |           | 0.184     |
| 7     | 8     |           | 0.371     |       |       |           |           |
| 7     | 9     |           | 0.460     | 13    | 1     | 2.294     | 0.478     |
| ,     | ,     |           | 0.400     | 13    | 2     |           | 0.606     |
|       |       | 0.015     | 0.016     | 13    | 3     |           | 0.507     |
| 8     | 1     | 0.015     | 0.015     | 13    | 4     |           | 0.315     |
|       |       |           |           |       |       |           | 0.388     |
| 9     | 1     | 1.784     | 0.009     | 13    | 5     |           | 0.300     |
| 9     | 2     |           | 1.775     | 13    | 6     |           |           |
|       |       |           |           | 13    | 7     |           | 0.        |
| 10    | 1     | 0.109     | 0.017     | 13    | 8     |           | 0.        |
| 10    | 2     |           | 0.023     | 13    | 9     |           | 0.        |
|       | 3     |           | 0.028     | 13    | 10    |           | n.        |
| 10    |       |           |           | 13    | 11    |           | 0.        |
| 10    | 4     |           | 0.041     | 13    | 12    |           | 0.        |
|       |       |           |           |       |       |           | 0.        |
| 11    | 1     | 3.779     | 0.064     | 13    | 13    |           |           |
| 11    | 2     |           | 0.141     |       |       | 1 007     | 0.17/     |
| 11    | 3     |           | 0.265     | 14    | 1     | 1.857     | 0.174     |
| 11    | 4     |           | 0.157     | 14    | 2     |           | 0.404     |
| 11    | 5     |           | 0.101     | 14    | 3     |           | 1.280     |
| 1.1   |       |           |           |       |       |           |           |

<sup>\*</sup>Costs do not include structure and enforcement costs.



Table I.38. Cost-Responsibility for City Streets (1985-86)\*

|       |       |           |           |      |         | e .       |           |
|-------|-------|-----------|-----------|------|---------|-----------|-----------|
| Veh   | Sub-  |           | nsibility | Veh  | Sub-    |           | naibility |
| Class | Group | Veh Class | Sub-Group | Clas | s Group | Veh Class | Sub-Croup |
|       |       | 0.03/     | 9.934     | 11   | 6       |           | 0.401     |
| 1     | 1     | 9.934     | 9.934     | 11   | 7       |           | 0.120     |
|       |       |           |           |      | 8       |           | 0.165     |
| 2     | 1     | 39.843    | 39.843    | 11   | _       |           |           |
|       |       |           |           | 11   | 9       |           | 0.108     |
| 3     | 1     | 3.746     | 0.327     | 11   | 10      |           | 0.137     |
| 3     | 2     |           | 0.142     | 11   | 11      |           | 0.171     |
| 3     | 3     |           | 0.553     | 11   | 12      |           | 0.212     |
| 3     | 4     |           | 0.496     | 11   | 13      |           | 0.514     |
| 3     | 5     |           | 0.209     |      |         |           |           |
| 3     | 6     |           | 0.895     | 12   | 1       | 38.507    | 0.018     |
| 3     | 7     |           | 0.647     | 12   | 2       |           | 0.045     |
| 3     | 8     |           | 0.192     | 12   | 3       |           | 0.157     |
|       |       |           | 0.192     | 12   | 4       |           | 0.866     |
| 3     | 9     |           | 0.200     | 12   | 5       |           | 0.237     |
|       |       |           | 0 ( )     | 12   | 6       |           | 0.495     |
| 4     | 1     | 0.641     | 0.641     |      |         |           | 0.053     |
|       |       |           |           | 12   | 7       |           |           |
| 5     | 1     | 0.265     | 0.265     | 12   | 8       |           | 0.255     |
|       |       |           |           | 12   | 9       |           | 0.659     |
| 6     | 1     | 1.976     | 0.289     | 12   | 10      |           | 0.732     |
| 6     | 2     |           | 0.228     | 12   | 11      |           | 0.215     |
| 6     | 3     |           | 0.129     | 12   | 12      |           | 0.394     |
| 6     | 4     |           | 0.170     | 12   | 13      |           | 0.641     |
| 6     | 5     |           | 0.065     | 12   | 14      |           | 0.582     |
|       | 6     |           | 0.083     | 12   | 15      |           | 0.685     |
| 6     |       |           |           | 12   | 16      |           | 0.537     |
| 6     | 7     |           | 0.104     |      |         |           | 1.091     |
| 6     | 8     |           | 0.161     | 12   | 17      |           |           |
| 6     | 9     |           | 0.746     | 12   | 18      |           | 4.653     |
|       |       |           |           | 12   | 19      |           | 2.509     |
| 7     | 1     | 0.769     | 0.016     | 12   | 20      |           | 5.178     |
| 7     | 2     |           | 0.023     | 12   | 21      |           | 7.355     |
| 7     | 3     |           | 0.035     | 12   | 22      |           | 4.686     |
| 7     | 4     |           | 0.053     | 12   | 23      |           | 5.378     |
| 7     | 5     |           | 0.056     | 12   | 24      |           | 0.731     |
| 7     | 6     |           | 0.113     | 12   | 25      |           | 0.166     |
| 7     | 7     |           | 0.117     | 12   | 26      |           | 0.189     |
| 7     | 8     |           | 0.159     |      |         |           |           |
| 7     | 9     |           | 0.196     | 13   | 1       | 0.627     | 0.134     |
| /     | 9     |           | 0.190     | 13   | 2       | 0.00      | 0.167     |
|       |       | 0.010     | 0.010     | 13   | 3       |           | 0.138     |
| 8     | 1     | 0.010     | 0.010     | 13   | 4       |           | 0.085     |
|       |       |           |           |      |         |           | 0.103     |
| 9     | 1     | 0.774     | 0.005     | 13   | 5       |           |           |
| 9     | 2     |           | 0.769     | 13   | 6       |           | 0.        |
|       |       |           |           | 13   | 7       |           | 0.        |
| 10    | 1     | 0.164     | 0.027     | 13   | 8       |           | 0.        |
| 10    | 2     |           | 0.035     | 13   | 9       |           | 0.        |
| 10    | 3     |           | 0.042     | 13   | 10      |           | 0.        |
| 10    | 4     |           | 0.059     | 13   | 11      |           | 0.        |
| 10    | 7     |           |           | 13   | 12      |           | 0.        |
| 11    | 1     | 2.353     | 0.061     | 13   | 13      |           | 0.        |
|       |       | 2.333     | 0.105     | 13   |         |           |           |
| 11    | 2     |           |           | 14   | 1       | 0.391     | 0.039     |
| 11    | 3     |           | 0.184     |      |         | 0.391     | 0.037     |
| 11    | 4     |           | 0.107     | 14   | 2       |           | 0.265     |
| 11    | 5     |           | 0.067     | 14   | 3       |           | 0.203     |
|       |       |           |           |      |         |           |           |

<sup>\*</sup>Costs do not include structure and enforcement acts.



Table I.39. Cost-Responsibility for Bridges on State Eighways (1985-86)

|       |       |           |           | Veh   | Sub-     | -  | Respo | naibility |
|-------|-------|-----------|-----------|-------|----------|----|-------|-----------|
| Veh   | Sub-  | % Respon  | nsibility | Class |          |    |       | Sub-Group |
| Class | Group | Veh Class | Sub-Group | Class | 01000    |    | 02000 |           |
| 1     | 1     | 16.137    | 16.137    | 1.1   | 6        |    |       | 0.197     |
| 1     | ı     | 10 4137   | 10.13,    | 11    | 7        |    |       | 0.078     |
| _     |       | 55 (0)    | 55.606    | 11    | 8        |    |       | 0.076     |
| 2     | 1     | 55.606    | 33.000    | 11    | 9        |    |       | 0.062     |
|       |       |           |           | 11    | 10       |    |       | 0.060     |
| 3     | 1     | 4.344     | 0.626     | 11    | 11       |    |       | 0.063     |
| 3     | 2     |           | 0.345     |       |          |    |       | 0.060     |
| 3     | 3     |           | 0.901     | 11    | 12<br>13 |    |       | 0.103     |
| 3     | 4     |           | 0.690     | 11    | 13       |    |       | 0.103     |
| 3     | 5     |           | 0.450     |       |          |    | 005   | 0.031     |
| 3     | 6     |           | 0.607     | 12    | 1        | 15 | -895  | 0.031     |
| 3     | 7     |           | 0.370     | 12    | 2        |    |       | 0.120     |
| 3     | 8     |           | 0.171     | 12    | 3        |    |       | 0.457     |
| 3     | 9     |           | 0.184     | 12    | 4        |    |       | 1.444     |
| ,     | ,     |           |           | 12    | 5        |    |       | 0.695     |
| 4     | 1     | 0.236     | 0.236     | 12    | 6        |    |       | 0.642     |
| 4     | 1     | 0.230     | 0.230     | 12    | 7        |    |       | 0.286     |
|       |       | 0.5/5     | 0.545     | 12    | 8        |    |       | 0.355     |
| 5     | 1     | 0.545     | 0.343     | 12    | 9        |    |       | 0.555     |
|       |       |           | 0.075     | 12    | 10       |    |       | 0.519     |
| 6     | 1     | 1.051     | 0.275     |       | 11       |    |       | 0.331     |
| 6     | 2     |           | 0.161     | 12    |          |    |       | 0.332     |
| 6     | 3     |           | 0.124     | 12    | 12       |    |       | 0.394     |
| 6     | 4     |           | 0.111     | 12    | 13       |    |       |           |
| 6     | 5     |           | 0.040     | 12    | 14       |    |       | 0.416     |
| 6     | 6     |           | 0.048     | 12    | 15       |    |       | 0.400     |
| 6     | 7     |           | 0.053     | 12    | 16       |    |       | 0.572     |
| 6     | 8     |           | 0.054     | 12    | 17       |    |       | 0.584     |
| 6     | 9     |           | 0.185     | 12    | 18       |    |       | 1.066     |
| 0     | ,     |           | 0         | 12    | 19       |    |       | 0.701     |
| -     |       | 0.507     | 0.056     | 12    | 20       |    |       | 1.027     |
| 7     | 1     | 0.307     | 0.040     | 12    | 21       |    |       | 1.787     |
| 7     | 2     |           | 0.044     | 12    | 22       |    |       | 1.318     |
| 7     | 3     |           |           | 12    | 23       |    |       | 1.416     |
| 7     | 4     |           | 0.050     | 12    | 24       |    |       | 0.267     |
| 7     | 5     |           | 0.046     | 12    | 25       |    |       | 0.081     |
| 7     | 6     |           | 0.061     | 12    | 26       |    |       | 0.100     |
| 7     | 7     |           | 0.075     | 1.2   | 20       |    |       | 0.200     |
| 7     | 8     |           | 0.069     |       | ,        |    | .447  | 0.105     |
| 7     | 9     |           | 0.066     | 13    | 1        |    | 44/   | 0.105     |
|       |       |           |           | 13    | 2        |    |       | 0.061     |
| 8     | 1     | 0.213     | 0.213     | 13    | 3        |    |       |           |
|       |       |           |           | 13    | 4        |    |       | 0.040     |
| 9     | 1     | 1.739     | 0.033     | 13    | 5        |    |       | 0.030     |
| ģ     | 2     |           | 1.706     | 13    | 6        |    |       | 0.009     |
| ,     | _     |           |           | 13    | 7        |    |       | 0.020     |
| 10    | 1     | 0.126     | 0.031     | 13    | 8        |    |       | 0.009     |
| 10    |       | 0.120     | 0.031     | 13    | 9        |    |       | 0.009     |
| 10    | 2     |           | 0.033     | 13    | 10       |    |       | 0.014     |
| 10    | 3     |           |           | 13    | 11       |    |       | 0.009     |
| 10    | 4     |           | 0.031     | 13    | 12       |    |       | 0.018     |
|       |       |           | 0.077     | 13    | 13       |    |       | 0.018     |
| 11    | 1     | 1.350     | 0.077     | 13    | 13       |    |       |           |
| 11    | 2     |           | 0.102     | 1.1   | 1        |    | 1.828 | 0.078     |
| 11    | 3     |           | 0.234     | 14    | 1        |    | 020   | 0.312     |
| 11    | 4     |           | 0.130     | 14    | 2        |    |       | 1.438     |
| 11    | 5     |           | 0.109     | 14    | 3        |    |       | 1.430     |
|       |       |           |           |       |          |    |       |           |



Table I.40. Cost-Responsibility for Bridges on County Roads (1985-86)

| Veh         Sub-         X         Responsibility         Class         Group         Veh         Class         Group         Veh         Class         Class         Sub-Group           1         1         1         15.039         15.039         11         6         9.056           2         1         63.124         63.124         11         7         9.056           3         1         6.958         1.206         11         10         9.032           3         2         0.430         11         11         9         0.032           3         3         1.618         11         12         9.041           3         3         1.618         11         12         9.041           3         3         1.618         11         12         9.041           3         3         1.618         11         12         9.041           3         3         1.618         11         12         9.041           3         3         1.200         12         1         4.814         0.008           3         7         0.671         12         1         4.814         0.008 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th> 15111</th>  |         |      |           |           |       |       |          | 15111       |
|--|---------|------|-----------|-----------|-------|-------|----------|-------------|
| 1  | Veh S   | ub-  | % Respon  | nsibility | Veh   |       |          |             |
| 2 1 63.124 63.124 11 8 0.056 2 1 63.124 63.124 11 8 0.056 3 1 6.958 1.206 11 10 9.032 3 2 0.430 11 11 11 9.041 3 3 1.618 11 12 0.041 3 4 0.925 11 13 0.122 3 5 0.478 3 6 1.200 12 1 4.214 0.008 3 7 0.671 12 2 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.339 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.066 4 1 0.325 12 12 7 0.016 6 1 2.124 0.455 12 10 0.163 6 2 0.152 12 12 9 0.181 6 5 0.071 12 12 12 0.066 6 3 0.152 12 11 0.066 6 4 0.152 12 11 0.066 6 5 0.071 12 14 0.089 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 21 17 0.132 6 9 0.659 12 18 0.477 7 4 0.012 12 20 0.463 7 7 2 0.010 12 20 0.463 7 7 3 0.010 12 21 0.259 7 1 0.120 0.010 12 21 0.259 7 1 0.120 0.010 12 22 0.049 9 1 2.129 0. 13 5 0.259 7 6 0.010 12 22 0.0463 7 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0414 9 1 2.129 0. 13 5 0.099 9 2 0.13 3 7 0.281 10 1 0 0 0 13 3 9 0.016 11 1 0 0 0 13 3 9 0.016 11 1 1 0.987 0.068 13 11 0 0.016 11 1 1 0.987 0.068 13 11 0 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100   | Class G | roup | Veh Class | Sub-Group | Class | Group | Ven Llas | s Sub-Group |
| 2 1 63.124 63.124 11 8 0.056 2 1 63.124 63.124 11 8 0.056 3 1 6.958 1.206 11 10 9.032 3 2 0.430 11 11 11 9.041 3 3 1.618 11 12 0.041 3 4 0.925 11 13 0.122 3 5 0.478 3 6 1.200 12 1 4.214 0.008 3 7 0.671 12 2 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.339 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.066 4 1 0.325 12 12 7 0.016 6 1 2.124 0.455 12 10 0.163 6 2 0.152 12 12 9 0.181 6 5 0.071 12 12 12 0.066 6 3 0.152 12 11 0.066 6 4 0.152 12 11 0.066 6 5 0.071 12 14 0.089 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 21 17 0.132 6 9 0.659 12 18 0.477 7 4 0.012 12 20 0.463 7 7 2 0.010 12 20 0.463 7 7 3 0.010 12 21 0.259 7 1 0.120 0.010 12 21 0.259 7 1 0.120 0.010 12 22 0.049 9 1 2.129 0. 13 5 0.259 7 6 0.010 12 22 0.0463 7 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0463 7 9 0.010 12 22 0.0414 9 1 2.129 0. 13 5 0.099 9 2 0.13 3 7 0.281 10 1 0 0 0 13 3 9 0.016 11 1 0 0 0 13 3 9 0.016 11 1 1 0.987 0.068 13 11 0 0.016 11 1 1 0.987 0.068 13 11 0 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100 11 1 1 0.987 0.068 13 13 10 0.100   |         |      | 15 030    | 15 030    | 1.1   | 6     |          | 9.182       |
| 2 1 63.124 63.124 11 8 0.056 3 1 6.958 1.206 11 10 0.032 3 2 0.430 11 11 0.0031 3 3 1.618 11 12 0.041 3 3 4 0.925 11 13 0.122 3 5 0.478 3 3 6 1.200 12 1 4.214 0.008 3 7 0.671 12 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.065 6 2 0.325 12 11 0.066 6 3 0.152 12 11 0.066 6 3 0.152 12 11 0.066 6 4 0.152 12 11 0.066 6 5 0.071 12 14 0.086 6 6 0.052 12 12 10 0.066 6 7 0.099 12 16 0.066 6 8 0.112 12 17 0.116 6 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.136 6 9 0.659 12 18 10 0.067 7 1 0.120 0.010 12 21 18 0.477 7 1 0.120 0.010 12 22 0.464 7 4 0.012 12 12 10 0.259 7 5 0.009 12 16 0.067 7 7 0.010 12 20 0.463 7 7 2 0.010 12 22 0.414 7 4 0.012 12 12 18 0.477 7 5 0.009 12 24 0.069 7 6 0.010 12 22 0.4414 7 7 4 0.012 12 12 13 0.577 7 5 0.009 12 24 0.069 7 6 0.010 12 22 0.4414 7 7 4 0.012 12 22 0.4414 7 7 4 0.012 12 12 13 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 9 0.016 12 25 0.016 7 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 133 8 0 13 3 9 0.001 14 1 0. 0. 133 8 0 15 0.001 16 1 0. 0. 133 8 0 17 1 0.987 0.068 13 13 10 0. 11 1 1 0.987 0.068 11 3 13 10 0. 11 1 1 0.987 0.068 11 1 3 0.081 14 2 2.897 0.156 11 0.759   | 1       | 1    | 15.039    | 13.039    |       |       |          |             |
| 1  |         |      |           |           |       |       |          |             |
| 3         1         6.958         1.206         11         10         0.032           3         2         0.430         11         11         20.041           3         3         1.618         11         12         0.041           3         4         0.925         11         13         0.122           3         5         0.478         0.12         1         4.214         0.008           3         7         0.671         12         2         0.049           3         8         0.172         12         3         0.049           3         9         0.258         12         4         0.389           4         1         0.251         0.251         12         6         0.177           5         1         0.622         0.622         12         8         0.065           6         1         2.124         0.455         12         10         0.163           6         2         0.325         12         11         0.066           6         1         2.124         0.455         12         10         0.163           6         2   | 2       | 1    | 63.124    | 63.124    |       |       |          |             |
| 3 2 0.430 11 11 11 0.041 3 3 3 1.618 11 12 0.041 3 4 0.925 11 13 0.122 3 5 0.478 3 6 1.200 12 1 4.214 0.008 3 7 0.671 12 2 0.049 3 9 0.258 12 4 0.339 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.066 6 3 0.152 12 12 0.069 6 4 0.152 12 12 10 0.163 6 5 0.071 12 12 12 0.066 6 7 0.099 12 15 0.101 6 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 6 7 2 0.010 12 21 18 0.477 7 1 0.120 0.010 12 21 18 0.477 7 2 0.010 12 22 0.444 7 4 0.012 12 12 13 0.575 7 3 0.010 12 22 0.445 7 4 0.012 12 12 13 0.575 7 3 0.010 12 22 0.444 7 4 0.012 12 12 13 0.575 7 3 0.010 12 22 0.444 7 4 0.012 12 12 13 0.575 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 8 0.019 12 12 12 0.069 7 6 0.016 12 25 0.016 7 7 9 0.016 12 25 0.016 7 7 9 0.016 12 25 0.016 7 8 0.019 7 0.016 12 25 0.016 7 8 0.019 7 0.016 12 25 0.016 7 8 0.019 7 0.016 12 25 0.016 7 8 0.019 7 0.016 12 25 0.016 7 8 0.019 13 1 0.937 0.281 10 1 0 0 0 13 13 10 0.018 11 1 0.987 0.068 13 13 0.011 11 1 0.987 0.068 13 13 0.011 11 1 0.987 0.068 13 13 0.0754 11 1 1 0.987 0.068 13 13 0.0754 11 1 1 0.987 0.068 13 13 0.0754 11 1 1 0.987 0.068 13 13 0.0754 11 1 1 0.987 0.068 13 13 13 0.7554   |         |      |           |           |       |       |          |             |
| 3 2 0.430 11 11 11 0.041 3 3 4 0.925 11 13 0.041 3 4 0.925 11 13 0.012 3 5 0.478 3 6 1.200 12 1 4.814 0.008 3 7 0.671 12 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0 0.163 6 2 0.325 12 11 0 0.665 6 3 0.152 12 12 10 0.666 6 3 0.152 12 11 0 0.666 6 4 0.152 12 11 0 0.666 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.087 6 6 7 0.099 12 15 0.007 6 8 0.112 12 17 0.016 6 7 0.099 12 15 0.007 6 8 0.112 12 17 0.037 6 6 8 0.112 12 17 0.037 7 1 0.120 0.010 12 20 0.657 7 3 0.010 12 21 18 0.477 7 4 0.012 12 22 0.477 7 5 0.009 12 24 0.059 7 6 0.010 12 22 0.414 7 7 4 0.012 12 23 0.575 7 3 0.010 12 22 0.414 7 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.019 9 2 2.129 13 6 0.019 13 1 0.997 0.068 13 10 0.010 11 1 0. 0. 13 18 0.111 11 0.987 0.068 13 13 10 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111 11 1 0.987 0.068 13 13 13 0.111  | 3       | 1    | 6.958     | 1.206     |       |       |          |             |
| 3       3       1.618       11       12       0.041         3       4       0.925       11       13       0.122         3       5       0.478       1       1       1       0.008         3       7       0.671       12       2       0.016       0.016         3       8       0.172       12       3       0.049         3       9       0.258       12       4       0.389         4       1       0.251       0.251       12       6       0.177         5       1       0.622       0.622       12       8       0.065         6       1       2.124       0.455       12       10       0.016         6       2       0.325       12       11       0.046         6       2       0.152       12       12       0.069         6       4       0.152       12       13       0.016         6       5       0.071       12       14       0.087         6       6       0.071       12       14       0.087         6       7       0.099       12       16   | 3       | 2    |           | 0.430     | 11    | 11    |          |             |
| 3 4 0.925 11 13 0.122 3 5 0.478 3 6 1.200 12 1 2 0.008 3 7 0.671 12 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.066 6 3 0.152 12 12 0.0669 6 4 0.152 12 12 10 0.066 6 3 0.152 12 12 0.0669 6 4 0.099 12 15 0.087 6 6 6 0.099 12 15 0.007 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.477 7 3 0.010 12 20 0.463 7 2 0.010 12 20 0.463 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.416 7 7 4 0.012 12 23 0.416 7 7 0.016 12 25 0.069 7 6 0.019 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 26 0.016 7 7 0.016 12 26 0.016 7 7 0.016 12 26 0.016 7 7 0.019 13 1 0.937 0.281 8 1 0. 0. 13 8 0. 0. 13 3 0. 0. 10 1 0. 0. 13 13 0 0. 10 1 0. 0. 13 13 0 0. 11 1 0.987 0.068 13 15 0. 11 1 0.987 0.068 13 15 0.016 11 2 0.068 11 14 2 0.0754   |         |      |           | 1.618     | 11    | 12    |          | 0.041       |
| 3 5 0.478 1.200 12 1 4.814 0.008 3.7 7 0.671 12 2 3 0.016 3.8 8 0.172 12 3 0.049 3.8 9 0.258 12 4 0.251 0.251 12 5 0.086 6.2 12 8 0.065 12 9 0.181 6.2 0.325 12 11 0.066 6.3 0.152 12 12 10 0.016 6.3 0.152 12 12 10 0.046 6.5 0.071 12 14 0.087 6.6 6 0.071 12 14 0.087 6.6 6 0.099 12 15 0.101 6.7 7 0.099 12 16 0.067 6.8 0.112 12 17 0.0259 7.1 0.120 0.010 12 22 0.067 7.2 0.010 12 22 0.069 7.7 6 0.010 12 22 0.041 7.7 7.7 0.016 12 22 0.414 7.4 0.012 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 12 12 23 0.577 7.5 0.009 12 24 0.069 7.7 6 0.016 12 25 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 0.016 7.7 7.0 7.0 7.7 7.0 7.0 7.0 7.0 7.0 7.0   |         |      |           |           | 11    | 13    |          | 0.122       |
| 3 6 1.200 12 1 4.214 0.008 3 7 0.671 12 2 0.016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.046 6 3 0.152 12 11 0.046 6 3 0.152 12 11 0.046 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 6 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 21 17 0.132 6 9 0.659 12 18 0.477 7 2 0.010 12 22 0.463 7 2 0.010 12 22 0.463 7 2 0.010 12 22 0.463 7 3 0.010 12 22 0.463 7 7 0.010 12 22 0.463 7 7 0.010 12 22 0.444 7 4 0.012 12 23 0.575 7 5 0.009 12 24 0.066 7 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.094 9 1 2.129 0. 13 5 0.099 9 2 2.129 13 6 0.019 13 1 0.997 0.068 13 13 0.11 10 4 0. 13 10 0. 11 11 1 0.987 0.068 13 13 0. 11 11 1 0.987 0.068 13 13 13 0. 11   | 3       |      |           |           |       |       |          |             |
| 3 7 0.671 12 2 0.0016 3 8 0.172 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 12 7 0.016 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.046 6 3 0.152 12 12 10 0.163 6 4 0.152 12 12 10 0.069 6 4 0.152 12 12 10 0.069 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.116 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.132 6 9 0.659 12 18 0.477 7 0.059 12 18 0.477 7 1 0.120 0.010 12 12 17 0.132 6 9 0.010 12 22 0.414 7 4 0.012 12 12 13 0.575 7 3 0.010 12 22 0.414 7 4 0.012 12 12 12 0.069 7 6 0.016 12 25 0.016 7 7 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.937 0.281 13 2 0.281 13 3 0.094 9 1 2.129 0. 13 5 0.099 9 2 2.129 13 6 0.009 13 1 0.937 0.281 10 1 0. 0. 13 10 0. 113 10 0. 110 10 1 0. 0. 13 10 0. 113 10 0. 110 11 1 0.9987 0.068 13 13 13 0. 111 11 1 0.9987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111 11 1 0.987 0.068 13 13 13 0. 111  |         |      |           |           | 1.2   | 1     | 4.214    | 0.008       |
| 3 8 0.1772 12 3 0.049 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 6 0.177 5 1 0.622 0.622 12 8 0.065 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.046 6 3 0.152 12 12 10 0.068 6 4 0.152 12 12 13 0.116 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 15 0.101 6 7 0.099 12 16 0.067 7 1 0.120 0.010 12 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 21 0.755 7 3 0.010 12 22 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.755 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.016 7 8 0.019 9 1 2.129 0. 13 5 0.016 9 1 2.129 0. 13 5 0.016 10 2 0.094 9 1 0.120 0.13 3 0.016 11 1 0. 0. 13 13 0.0 11 1 0. 0. 13 10 0.1 10 1 0. 0. 13 10 0.1 11 1 0.987 0.068 13 13 10 0.1 11 1 0.987 0.068 13 13 10 0.1 11 1 0.987 0.068 13 13 10 0.1 11 1 0.987 0.068 13 13 13 0.1 11 1 0.987 0.068 13 13 13 0.1 11 1 0.081 14 2 2 0.754   | 3       |      |           |           |       |       |          |             |
| 3 9 0.258 12 4 0.389 4 1 0.251 0.251 12 5 0.086 4 1 0.622 0.622 12 8 0.016 5 1 0.622 0.622 12 8 0.065 12 9 0.181 6 1 2.124 0.455 12 10 0.163 6 2 0.325 12 11 0.046 6 3 0.152 12 12 10 0.066 6 4 0.152 12 12 13 0.116 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 15 0.101 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.887 9 2 2.129 13 6 0. 13 3 0.094 9 1 2.129 0. 13 5 0.016 10 2 0.01 13 10 0. 10 10 1 0. 0. 13 10 0. 11 1 0.987 0.068 13 11 0. 11 1 0.987 0.068 13 12 11 0.754 11 2 0.068  | 3       |      |           |           |       |       |          |             |
| 1  |         |      |           |           |       |       |          |             |
| 4       1       0.251       0.251       12       6       0.177         5       1       0.622       0.622       12       8       0.065         6       1       2.124       0.455       12       10       0.163         6       2       0.325       12       11       0.046         6       3       0.152       12       11       0.046         6       3       0.152       12       12       0.069         6       4       0.152       12       13       0.116         6       5       0.071       12       14       0.087         6       6       0.099       12       15       0.101         6       7       0.099       12       16       0.067         6       8       0.112       12       17       0.132         6       9       0.120       0.010       12       17       0.132         7       1       0.120       0.010       12       20       0.463         7       2       0.010       12       21       0.755         7       3       0.010       12       23 <th>3</th> <td>9</td> <td></td> <td>0.258</td> <td></td> <td></td> <td></td> <td></td>   | 3       | 9    |           | 0.258     |       |       |          |             |
| 5         1         0.622         0.622         12         8         0.065           6         1         2.124         0.455         12         10         0.181           6         2         0.325         12         11         0.046           6         3         0.152         12         12         0.069           6         4         0.152         12         13         0.116           6         5         0.071         12         14         0.087           6         6         0.099         12         15         0.101           6         7         0.099         12         16         0.067           6         8         0.112         12         17         0.132           6         9         0.659         12         18         0.477           7         1         0.120         0.010         12         20         0.463           7         2         0.010         12         21         19         0.259           7         1         0.120         0.010         12         22         0.414           7         2         0.010  |         |      |           |           |       |       |          |             |
| 5         1         0.622         0.622         12         8         0.065           6         1         2.124         0.455         12         10         0.163           6         2         0.325         12         11         0.046           6         3         0.152         12         12         0.069           6         4         0.152         12         13         0.116           6         5         0.071         12         14         0.087           6         6         0.099         12         15         0.101           6         7         0.099         12         16         0.067           6         8         0.112         12         17         0.132           6         9         0.659         12         18         0.477           7         1         0.120         0.010         12         20         0.463           7         2         0.010         12         20         0.463           7         3         0.010         12         22         0.414           7         4         0.012         12         23   | 4       | 1    | 0.251     | 0.251     | 12    |       |          |             |
| 1  |         |      |           |           | 12    | 7     |          | 0.016       |
| 12    9  | 5       | 1    | 0.622     | 0.622     | 12    | 8     |          | 0.065       |
| 6 1 2.124 0.455 12 10 0.463 6 2 0.325 12 11 0.046 6 3 0.152 12 12 0.069 6 4 0.152 12 13 0.416 6 5 0.071 12 14 0.087 6 6 6 0.0999 12 15 0.101 6 7 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.463 7 7 6 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.094 9 1 2.129 0. 13 5 0.094 9 1 0.019 13 1 0.937 0.281 10 3 0. 13 10 0.018 10 2 0. 13 13 0.018 11 1 0.987 0.068 13 13 10 0.111 11 1 0.987 0.068 11 1 3 0.161 14 1 2.597 0.156 11 1 4 0.081 14 2   | ,       | 1    | 0.022     | 0 1022    | 12    | 9     |          | 0.181       |
| 6 2 0.325 12 11 0.046 6 3 0.152 12 12 0.069 6 4 0.152 12 13 0.116 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 19 0.259 7 1 0.120 0.010 12 21 0.755 7 3 0.010 12 21 0.755 7 4 0.012 12 22 0.446 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.066 7 7 7 0.016 12 25 0.016 7 7 8 0.019 12 24 0.0669 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 8 1 0. 0. 13 3 0.009 9 1 2.129 0. 13 5 0.281 9 1 2.129 0. 13 6 0.094 9 1 0.094 0.019 13 1 0.937 0.281 10 1 0. 0. 13 18 0.161 10 2 0. 13 19 0. 10 1 0. 0. 13 11 0. 11 1 0.987 0.068 11 1 3 0.068 11 1 3 0.068 11 1 3 0.161 14 1 2.897 0.156 11 1 4 0.081 14 2  | ,       | ,    | 2 126     | 0 455     |       |       |          |             |
| 6 3 0.152 12 12 0.069 6 4 0.152 12 13 0.116 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.463 7 4 0.012 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.067 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 7 0.016 12 26 0.016 7 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 8 1 0. 0. 13 3 0.093 9 2 2.129 13 6 0.094 9 1 2.129 0. 13 5 0.094 9 1 0.094 0.019 13 1 0.001 13 1 0.001 13 1 0.001 14 0.001 15 0.001 16 0.001 17 0.001 18 0.001 19 0.001 10 1 0. 0. 13 10 0.001 11 1 0. 0. 13 10 0.001 11 1 0. 0. 13 10 0.001 11 1 0.0068 11 1 0.987 0.068 11 1 0.0081 14 1 2.897 0.156 11 1 0.0081  |         |      | 2.124     |           |       |       |          |             |
| 6 4 0.152 12 13 0.116 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 5 0.094 9 1 0.094 10 1 0. 0. 13 8 0.187 10 1 0. 0. 13 8 0.187 10 1 0. 0. 13 10 0. 10 2 0. 13 10 0. 11 1 0. 0. 13 11 0. 11 1 0.987 0.068 13 11 0. 11 1 0.987 0.068 11 1 0.0081  |         |      |           |           |       |       |          |             |
| 6 5 0.071 12 14 0.087 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.094 10 1 0. 0. 13 18 0.094 10 2 0. 13 9 0.187 10 1 0. 0. 13 10 0.019 11 1 0. 0. 13 10 0.111 11 0.987 0.068 13 13 0.111 11 1 0.987 0.068 11 2 0.068 11 2 0.068 11 2 0.068 11 3 0.016 14 2 0.754 11 1 0.081 14 1 2.897 0.156 11 0.0994   |         |      |           |           |       |       |          |             |
| 6 6 6 0.099 12 15 0.101 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 12 19 0.259 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.093 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 5 0.094 9 1 0.01 13 5 0.094 9 1 0.01 13 5 0.099 10 1 1 0. 0. 13 8 0.099 10 2 13 9 0.019 11 1 0. 0. 13 10 0. 10 1 0. 0. 13 10 0. 11 1 0.987 0.068 13 10 0. 11 1 0.987 0.068 11 14 1 2.897 0.156 11 2 0.068 11 2 0.068 11 2 0.068 11 2 0.068 11 2 0.068  | 6       | 4    |           |           |       |       |          |             |
| 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 19 0.259 7 1 0.120 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.187 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 1 0. 0. 13 10 0. 11 1 0. 0. 13 11 0. 11 2 0.987 0.068 13 13 10 0. 11 1 0.987 0.068 13 13 10 0. 11 1 0.987 0.068 11 14 1 2.897 0.156 11 1 4 0.081 14 1 2.897 0.156   | 6       | 5    |           | 0.071     |       |       |          |             |
| 6 7 0.099 12 16 0.067 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 12 19 0.259 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 25 0.016 7 7 0.016 12 26 0.016 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 6 0.094 9 2 2.129 13 6 0. 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 10 0. 11 1 0.987 0.068 13 13 10 0. 11 1 0.987 0.068 13 13 10 0. 11 1 1 0.987 0.068 13 13 10 0. 11 1 2 0.068 11 14 1 2.897 0.156 11 1 4 0.081 14 2 1.088   | 6       | 6    |           | 0.099     |       |       |          |             |
| 6 8 0.112 12 17 0.132 6 9 0.659 12 18 0.477 7 1 0.120 0.010 12 20 0.463 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 7 0.016 12 25 0.016 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.161 10 1 0. 0. 13 8 0.187 10 1 0. 0. 13 9 0.094 11 1 0. 0. 13 10 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 12 0. 11 1 0.987 0.068 13 13 10 0. 11 1 1 0.987 0.068 13 13 10 0. 11 1 1 0.068 11 14 1 2.897 0.156 11 1 4 0.081 14 2 0.754  |         |      |           | 0.099     | 12    | 16    |          |             |
| 6       9       0.659       12       18       0.477         7       1       0.120       0.010       12       20       0.463         7       2       0.010       12       21       0.755         7       3       0.010       12       22       0.414         7       4       0.012       12       23       0.577         7       5       0.009       12       24       0.069         7       6       0.016       12       25       0.016         7       7       0.016       12       26       0.016         7       8       0.019       13       1       0.937       0.281         8       1       0.       0.       13       3       0.187         9       1       2.129       0.       13       5       0.093         9       2       2.129       13       6       0.093         10       1       0.       0.       13       9       0.         10       2       0.       13       10       0.         10       3       0.       13       11       0. </th <th></th> <td></td> <td></td> <td></td> <td>12</td> <td>17</td> <td></td> <td>0.132</td>  |         |      |           |           | 12    | 17    |          | 0.132       |
| 7       1       0.120       0.010       12       20       0.463         7       2       0.010       12       21       0.755         7       3       0.010       12       21       0.755         7       3       0.012       12       22       0.414         7       4       0.012       12       23       0.577         7       5       0.009       12       24       0.069         7       6       0.016       12       25       0.016         7       7       0.016       12       26       0.016         7       8       0.019       13       1       0.937       0.281         8       1       0.       0.       13       3       0.281         8       1       0.       0.       13       3       0.187         9       1       2.129       0.       13       6       0.093         9       2       2.129       13       6       0.093         10       1       0.       0.       13       8       0.         10       2       0.       13       9  |         |      |           |           | 12    | 18    |          | 0.477       |
| 7       1       0.120       0.010       12       20       0.463         7       2       0.010       12       21       0.755         7       3       0.010       12       22       0.414         7       4       0.012       12       23       0.577         7       5       0.009       12       24       0.069         7       6       0.016       12       25       0.016         7       7       0.016       12       26       0.016         7       8       0.019       13       1       0.937       0.281         8       1       0.       0.       13       2       0.281         8       1       0.       0.       13       3       0.187       0.281         8       1       0.       0.       13       3       0.187       0.281         8       1       0.       0.       13       5       0.093       0.281         8       1       0.       0.       13       5       0.094       0.094         9       1       2.129       0.       13       6       0.094 <th>U</th> <td>,</td> <td></td> <td>0.037</td> <td></td> <td></td> <td></td> <td>0.259</td>  | U       | ,    |           | 0.037     |       |       |          | 0.259       |
| 7 2 0.010 12 21 0.755 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 26 0.016 7 7 8 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.094 10 1 0. 0. 13 8 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.111 0.1 | 7       |      | 0 120     | 0.010     |       |       |          | 0.463       |
| 7 3 0.010 12 22 0.414 7 4 0.012 12 23 0.577 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 0.016 12 26 0.016 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.093 9 2 2.129 13 6 0.093 10 1 0. 0. 13 18 0.0094 10 2 0. 13 9 0.100 10 2 0. 13 9 0.100 10 3 0. 13 10 0.100 10 4 0. 13 11 0.100 11 1 0.987 0.068 13 13 10 0.110 11 1 0.987 0.068 13 13 10 0.111 11 1 0.987 0.068 13 13 10 0.111 11 2 0.068 11 3 0.068 11 3 0.0161 14 1 2.897 0.156 11 4 0.081 14 2  |         |      | 0.120     |           |       |       |          | 0.755       |
| 7  |         |      |           |           |       |       |          |             |
| 7 5 0.009 12 24 0.069 7 6 0.016 12 25 0.016 7 7 7 0.016 12 26 0.016 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.093 9 2 2.129 13 6 0.093 10 1 0. 0. 13 8 0. 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 13 10 0. 11 1 0.987 0.068 13 13 0. 11 1 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754   |         |      |           |           |       |       |          |             |
| 7 6 0.016 12 25 0.016 7 7 7 0.016 12 26 0.016 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.093 9 2 2.129 13 6 0.093 13 7 0.093 10 1 0. 0. 13 8 0. 13 7 0.101 10 2 0. 13 8 0. 13 9 0. 13 10 0. 13 10 0. 13 11 | 7       |      |           |           |       |       |          |             |
| 7 7 0.016 12 26 0.016 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.093 9 2 2.129 13 6 0.093 9 2 2.129 13 6 0.13 7 0.093 10 1 0. 0. 13 8 0. 13 7 0.101 10 2 0. 13 8 0. 13 9 0. 10 13 10 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 13 11 0. 11 1 0. 11 1 1 0.987 0.068 13 13 13 10 0. 11 1 2 0.068 11 1 1 0.987 0.068 13 13 13 0. 156 11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754   | 7       | 5    |           |           |       |       |          |             |
| 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0. 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 13 12 0. 11 1 0.987 0.068 13 13 10 0. 11 2 0.068 11 3 0. 11 2 0.068 11 3 0. 11 4 0.081 14 2 0.754 11 0.0754   | 7       |      |           |           |       |       |          |             |
| 7 8 0.019 7 9 0.019 13 1 0.937 0.281 8 1 0. 0. 13 3 0.281 8 1 0. 0. 13 3 0.187 9 1 2.129 0. 13 5 0.094 9 2 2.129 13 6 0. 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 12 0. 11 1 0.987 0.068 13 13 0. 11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754   | 7       | 7    |           | 0.016     | 12    | 26    |          | 0.016       |
| 7 9 0.019 13 1 0.937 0.281 0.281 8 1 0. 0. 0. 13 3 0.187 0.187 0.187 9 1 2.129 0. 13 5 0.094 0.094 9 2 2.129 13 6 0. 13 7 0. 13 7 0. 13 7 0. 13 7 0. 13 7 0. 13 13 0 0. 13 10 0. 13 10 0. 13 11 0. 0. 13 11 0. 0. 13 12 0. 13 12 0. 13 12 0. 13 12 0. 13 12 0. 13 13 12 0. 11 1 1 0.987 0.068 13 13 13 0. 11 2 0.068 11 3 0.068 11 3 0.068 11 3 0.068 11 4 2 0.081 14 2 0.754 11 4 0.081   |         | 8    |           | 0.019     |       |       |          |             |
| 8     1     0.     0.     13     2     0.281       9     1     2.129     0.     13     3     0.094       9     2     2.129     13     6     0.093       10     1     0.     0.     13     7     0.       10     2     0.     13     9     0.       10     3     0.     13     10     0.       10     4     0.     13     11     0.       11     1     0.987     0.068     13     13     13       11     2     0.068     13     13     13       11     3     0.161     14     1     2.897     0.156       11     4     0.081     14     2     2.897     0.156   | 7       | 9    |           | 0.019     | 13    | 1     | 0.937    |             |
| 9  |         |      |           |           | 13    | 2     |          |             |
| 9 I 2.129 0. 13 5 0.094 9 2 2.129 13 6 0.093 10 1 0. 0. 13 8 0. 13 9 0. 13 10 0. 13 11 0. 13 12 0. 13 12 0. 11 1 0.987 0.068 13 13 13 0. 11 1 2 0.068 11 2 0.068 13 13 10 0. 11 1 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754  | 8       | 1    | Λ.        | 0.        | 13    | 3     |          | 0.187       |
| 9 1 2.129 0. 13 5 0.093 9 2 2.129 13 6 0. 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 13 10 0. 11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754   | o       | •    | •         | • •       | 13    | 4     |          | 0.094       |
| 9 2 2.129 13 6 0.  10 1 0. 0. 13 8 0.  10 2 0. 13 9 0.  10 3 0. 13 10 0.  10 4 0. 13 11 0.  11 1 0.987 0.068 13 13 12 0.  11 2 0.068 11 3 0.  11 3 0.161 14 1 2.897 0.156  11 4 0.081 14 2 0.754   | 0       | ,    | 2 120     | 0         | 13    | 5     |          | 0.093       |
| 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 13 0. 11 2 0.068 13 13 13 0. 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2  |         |      | 2.129     |           |       |       |          | 0.          |
| 10 1 0. 0. 13 8 0. 10 2 0. 13 9 0. 10 3 0. 13 10 0. 10 4 0. 13 11 0. 11 1 0.987 0.068 13 13 0. 11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2  | 9       | 2    |           | 2.129     |       |       |          |             |
| 10 1 0 0 0 13 9 0 0 13 10 0 10 10 4 0 0 13 11 0 0 11 1 1 1 0 1 1 1 1 1 1 1   |         |      |           |           |       |       |          |             |
| 10 2 0. 13 10 0. 13 10 0. 13 11 0. 0. 13 12 0. 13 12 0. 13 12 0. 13 12 0. 13 12 0. 13 13 12 13 13 13 13 13 13 13 14 14 1 2.897 0.156 11 4 0.081 14 2 0.754   |         |      | 0.        |           |       |       |          |             |
| 10 4 0. 13 11 0.  11 1 0.987 0.068 13 13 0.  11 2 0.068  11 3 0.161 14 1 2.897 0.156  11 4 0.081 14 2 0.754  | 10      | 2    |           |           |       |       |          |             |
| 11 1 0.987 0.068 13 13 0.  11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2  | 10      | 3    |           | 0.        |       |       |          |             |
| 13 12 0.00.  11 1 0.987 0.068 13 13 0.  11 2 0.068 11 3 0.161 14 1 2.897 0.156 11 4 0.081 14 2 0.754   | 10      | 4    |           | 0.        |       |       |          |             |
| 11 2 0.068<br>11 3 0.161 14 1 2.897 0.156<br>11 4 0.081 14 2   |         |      |           |           | 13    | 12    |          |             |
| 11 2 0.068<br>11 3 0.161 14 1 2.897 0.156<br>11 4 0.081 14 2 0.754   | 11      | 1    | 0.987     | 0.068     | 13    | 13    |          | 0.          |
| 11 3 0.161 14 1 2.897 0.156<br>11 4 0.081 14 2 0.754   |         |      | 0.,0.     |           |       |       |          |             |
| 11 4 0.081 14 2 0.754  |         |      |           |           | 14    | 1     | 2.897    | 0.156       |
| 11 4 0.001   |         |      |           |           |       |       |          |             |
| 11 ) 0.040   |         |      |           |           |       |       |          |             |
|  | 11      | )    |           | 0.040     | 1.4   | ,     |          |             |



Table L41. Cost-Responsibility for Bridges on City Streets (1985-86)

|       |       |           |           |    | ,    | C.L   | 7 Panna   | nsibility |
|-------|-------|-----------|-----------|----|------|-------|-----------|-----------|
| Veh   | Sub-  | % Respo   | nsibility | V. | eh   | Sub-  |           | Sub-Group |
| Class | Group | Veh Class | Sub-Group | C  | Lass | Group | ven Class | 3ub-Group |
|       |       |           |           |    |      | 6     |           | 0.225     |
| 1     | 1     | 15.935    | 15.935    |    | 11   | 7     |           | 0.067     |
|       |       |           |           |    | 11   |       |           | 0.067     |
| 2     | 1     | 60.972    | 60.972    |    | 11   | 8     |           |           |
|       |       |           |           |    | 11   | 9     |           | 0.037     |
| 3     | 1     | 3.486     | 0.666     |    | 11   | 10    |           | 0.037     |
| 3     | 2     |           | 0.238     |    | 11   | 11    |           | 0.044     |
| 3     | 3     |           | 0.881     |    | 11   | 12    |           | 0.044     |
|       |       |           | 0.504     |    | 11   | 13    |           | 0.116     |
| 3     | 4     |           |           |    |      |       |           |           |
| 3     | 5     |           | 0.214     |    | 12   | I     | 11.507    | 0.028     |
| 3     | 6     |           | 0.539     |    |      | 2     | 11.50     | 0.057     |
| 3     | 7     |           | 0.278     |    | 12   |       |           |           |
| 3     | 8     |           | 0.071     |    | 12   | 3     |           | 0.168     |
| 3     | 9     |           | 0.096     |    | 12   | 4     |           | 1.180     |
| _     | -     |           |           |    | 12   | 5     |           | 0.262     |
| 4     | :     | 0.829     | 0.829     |    | 12   | 6     |           | 0.516     |
| 4     | -     | 0.029     | 17.027    |    | 12   | 7     |           | 0.048     |
|       |       | 0.111     | 0.166     |    | 12   | 8     |           | 0.190     |
| 5     | :     | 0.466     | 0.466     |    | 12   | 9     |           | 0.509     |
|       |       |           |           |    |      |       |           | 0.456     |
| 6     | 1     | 1.467     | 0.374     |    | 12   | 10    |           | 0.124     |
| 6     | 2     |           | 0.267     |    | 12   | 11    |           |           |
| 6     | 3     |           | 0.118     |    | 12   | 12    |           | 0.186     |
| 6     | 4     |           | 0.118     |    | 12   | 13    |           | 0.290     |
| 6     | 5     |           | 0.048     |    | 12   | 14    |           | 0.218     |
|       |       |           | 0.062     |    | 12   | 15    |           | 0.239     |
| 6     | 6     |           |           |    | 12   | 16    |           | 0.159     |
| 6     | 7     |           | 0.062     |    |      | 17    |           | 0.294     |
| 6     | 8     |           | 0.068     |    | 12   |       |           | 1.064     |
| 6     | 9     |           | 0.350     |    | 12   | 18    |           |           |
|       |       |           |           |    | 12   | 19    |           | 0.544     |
| 7     | 1     | 0.124     | 0.012     |    | 12   | 20    |           | 0.972     |
| 7     | 2     | 0.12      | 0.012     |    | 12   | 21    |           | 1.517     |
|       | 3     |           | 0.012     |    | 12   | 22    |           | 0.832     |
| 7     |       |           |           |    | 12   | 23    |           | 1.395     |
| 7     | 4     |           | 0.013     |    | 12   | 24    |           | 0.167     |
| 7     | 5     |           | 0.010     |    |      |       |           | 0.046     |
| 7     | 6     |           | 0.016     |    | 12   | 25    |           |           |
| 7     | 7     |           | 0.016     |    | 12   | 26    |           | 0.046     |
| 7     | 8     |           | 0.017     |    |      |       |           |           |
| 7     | 9     |           | 0.017     |    | 13   | 1     | 0.363     | 0.109     |
| •     | -     |           |           |    | 13   | 2     |           | 0.109     |
| 8     | 1     | 0.        | 0.        |    | 13   | 3     |           | 0.073     |
| 0     | 1     | 0.        | ٠.        |    | 13   | 4     |           | 0.036     |
| ^     |       | 2 200     | 0.        |    | 13   | 5     |           | 0.036     |
| 9     | 1     | 2.286     |           |    | 13   | 6     |           | 0.        |
| 9     | 2     |           | 2.286     |    |      | 7     |           | 0.        |
|       |       |           |           |    | 13   |       |           | 0.        |
| 10    | 1     | 0.129     | 0.032     |    | 13   | 8     |           | 0.        |
| 10    | 2     |           | 0.032     |    | 13   | 9     |           |           |
| 10    | 3     |           | 0.032     |    | 13   | 10    |           | 0.        |
| 10    | 4     |           | 0.032     |    | 13   | 11    |           | 0.        |
|       |       |           |           |    | 13   | 12    |           | 0.        |
| 1.1   | 1     | 1.205     | 0.100     |    | 13   | 13    |           | 0.        |
| 11    |       | 1.203     | 0.100     |    | -    |       |           |           |
| 11    | 2     |           |           |    | 14   | 1     | 1.420     | 0.040     |
| 11    | 3     |           | 0.208     |    | 14   | 2     | 20,50     | 0.204     |
| 11    | 4     |           | 0.104     |    |      | 3     |           | 1.176     |
| 11    | 5     |           | 0.057     |    | 14   | 3     |           | 1.10      |
|       |       |           |           |    |      |       |           |           |

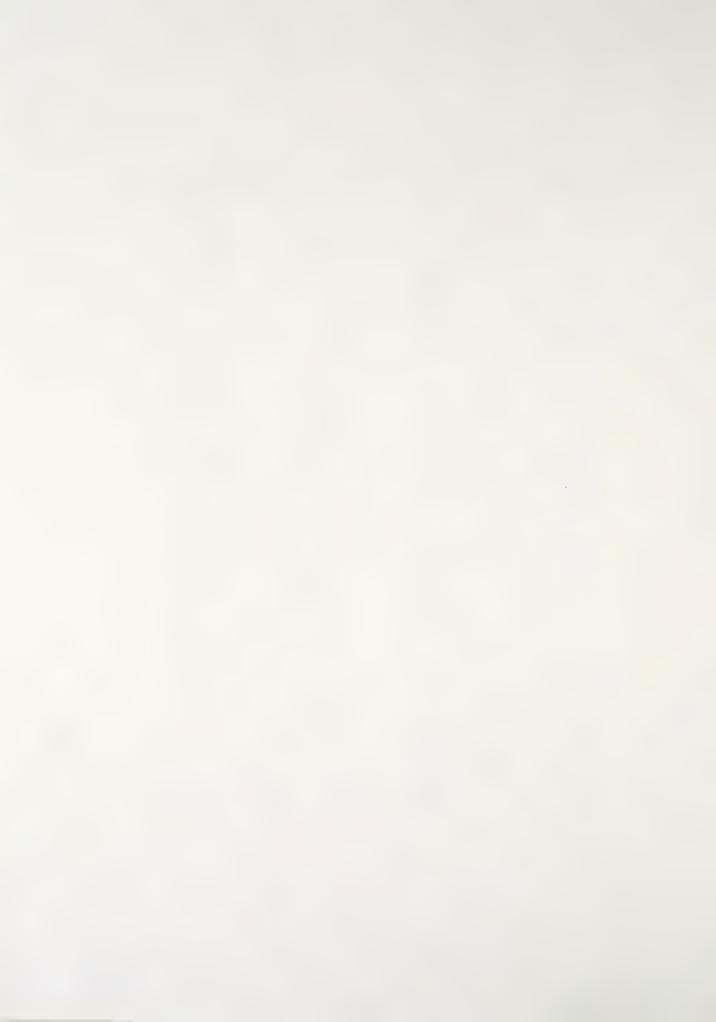


Table I.46. Overall Cost-Responsibility for County Road System (1983)

|       |       |           |           | 11 - h | Sub-  | 7 Peese    | naibility  |
|-------|-------|-----------|-----------|--------|-------|------------|------------|
| Veh   | Sub-  | % Кевроі  | nsibility | Veh    |       |            | Sub-Group  |
| Class | Group | Veh Class | Sub-Group | Class  | oroup | AGII CIANO | 300 01.300 |
|       |       | 5 001     | 5.901     | 11     | 6     |            | 0.728      |
| 1     | 1     | 5.901     | 2.901     | 11     | 7     |            | 0.226      |
|       |       |           |           |        | 8     |            | 0.314      |
| 2     | 1     | 30.713    | 30.713    | 11     |       |            |            |
|       |       |           |           | 11     | 9     |            | 0.202      |
| 3     | 1     | 15.075    | 0.481     | 11     | 10    |            | 0.258      |
| 3     | 2     |           | 0.948     | 11     | 1.1   |            | 0.327      |
| 3     | 3     |           | 1.542     | 11     | 12    |            | 0.352      |
| 3     | 4     |           | 1.745     | 11     | 13    |            | 0.861      |
| 3     | 5     |           | 0.866     |        |       |            |            |
|       |       |           | 4.027     | 12     | 1     | 27.483     | 0.008      |
| 3     | 6     |           |           | 12     | 2     | 2, 0, 00   | 0.025      |
| 3     | 7     |           | 3.082     |        | 3     |            | 0.089      |
| 3     | 8     |           | 0.928     | 12     |       |            | 0.533      |
| 3     | 9     |           | 1.456     | 12     | 4     |            |            |
|       |       |           |           | 12     | 5     |            | 0.150      |
| 4     | 1     | 0.607     | 0.607     | 12     | 6     |            | 0.324      |
|       |       |           |           | 12     | 7     |            | 0.034      |
| 5     | 1     | 0.285     | 0.285     | 12     | 8     |            | 0.170      |
| ,     |       | 0.205     | 0.203     | 12     | 9     |            | 0.449      |
| ,     |       | ( (()     | 0.790     | 12     | 10    |            | 0.499      |
| 6     | 1     | 6.662     |           | 12     | 11    |            | 0.151      |
| 6     | 2     |           | 0.603     | 12     | 12    |            | 0.274      |
| 6     | 3     |           | 0.388     |        |       |            | 0.450      |
| 6     | 4     |           | 0.567     | 12     | 13    |            |            |
| 6     | 5     |           | 0.224     | 12     | 14    |            | 0.386      |
| 6     | 6     |           | 0.298     | 12     | 15    |            | 0.499      |
| 6     | 7     |           | 0.376     | 12     | 16    |            | 0.385      |
| 6     | 8     |           | 0.604     | 12     | 17    |            | 0.766      |
| 6     | 9     |           | 2.811     | 12     | 18    |            | 3.308      |
| U     | ,     |           | 2.02.2    | 12     | 19    |            | 1.792      |
| 7     | 1     | 0.999     | 0.016     | 12     | 20    |            | 3.729      |
| 7     |       | 0.777     | 0.017     | 12     | 21    |            | 5.345      |
| 7     | 2     |           |           | 12     | 22    |            | 3.409      |
| 7     | 3     |           | 0.041     | 12     | 23    |            | 3.926      |
| 7     | 4     |           | 0.063     |        |       |            | 0.540      |
| 7     | 5     |           | 0.077     | 12     | 24    |            | 0.123      |
| 7     | 6     |           | 0.151     | 12     | 25    |            |            |
| 7     | 7     |           | 0.156     | 12     | 26    |            | 0.120      |
| 7     | 8     |           | 0.210     |        |       |            |            |
| 7     | 9     |           | 0.259     | 13     | 1     | 3.334      | 0.724      |
| ,     |       |           |           | 13     | 2     |            | 0.892      |
| 8     | 1     | 0.        | 0.        | 13     | 3     |            | 0.730      |
| 0     | 1     | 0.        | 0.        | 13     | 4     |            | 0.446      |
|       |       | 2.364     | 0.016     | 13     | 5     |            | 0.541      |
| 9     | 1     | 2.364     |           | 13     | 6     |            | 0.         |
| 9     | 2     |           | 2.348     |        | 7     |            | 0.         |
|       |       |           | _         | 13     |       |            | 0.         |
| 10    | 1     | 0.        | 0.        | 13     | 8     |            |            |
| 10    | 2     |           | 0.        | 13     | 9     |            | 0.         |
| 10    | 3     |           | 0.        | 13     | 10    |            | 0.         |
| 10    | 4     |           | 0.        | 13     | 11    |            | 0.         |
|       |       |           |           | 13     | 12    |            | 0.         |
| 11    | 1     | 4.038     | 0.061     | 13     | 13    |            | 0.         |
| 11    | 2     | 4.030     | 0.134     |        |       |            |            |
|       | 3     |           | 0.285     | 14     | 1     | 2.539      | 0.231      |
| 11    |       |           |           | 14     | 2     |            | 0.599      |
| 11    | 4     |           | 0.174     | 14     | 3     |            | 1.709      |
| 11    | 5     |           | 0.116     | 14     | ٥     |            |            |
|       |       |           |           |        |       |            |            |



Table I.47. Overall Cost-Responsibility for City Street System (1983)

| Veh   | Sub-   | 7 Respo    | nsibility | Veh | Sub-  | % Respo   | nsibility |
|-------|--------|------------|-----------|-----|-------|-----------|-----------|
|       |        |            | Sub-Group |     | Group | Veh Class | Sub-Group |
| 01443 | or out | VCI. 01000 | 040 0400  |     | ·     |           |           |
| 1     | 1      | 10.434     | 10.434    | 11  | 6     |           | 0.415     |
| -     |        |            |           | 11  | 7     |           | 0.128     |
| 2     | I      | 41.798     | 41.798    | 11  | 8     |           | 0.173     |
| _     | _      |            |           | 11  | 9     |           | 0.108     |
| 3     | 1      | 3.649      | 0.352     | 11  | 10    |           | 0.137     |
| 3     | 2      |            | 0.318     | 11  | 11    |           | 0.172     |
| 3     | 3      |            | 0.541     | 1.1 | 12    |           | 0.174     |
| 3     | 4      |            | 0.456     | 11  | 13    |           | 0.423     |
| 3     | 5      |            | 0.191     |     |       |           |           |
| 3     | 6      |            | 0.792     | 12  | 1     | 36.011    | 0.017     |
| 3     | 7      |            | 0.567     | 12  | 2     |           | 0.046     |
| 3     | 8      |            | 0.170     | 12  | 3     |           | 0.154     |
| 3     | 9      |            | 0.263     | 12  | 4     |           | 0.875     |
| ٥     | 7      |            | 0.203     | 12  | 5     |           | 0.233     |
| 4     | 1      | 1.074      | 1.074     | 12  | 6     |           | 0.491     |
| 4     | 1      | 1.074      | 1.074     | 12  | 7     |           | 0.051     |
| _     | ,      | 0 202      | 0 202     | 12  | 8     |           | 0.244     |
| 5     | 1      | 0.282      | 0.282     | 12  | 9     |           | 0.641     |
| ,     |        | 0 120      | 0.330     | 12  | 10    |           | 0.695     |
| 6     | 1      | 2.139      | 0.328     | 12  | 11    |           | 0.209     |
| 6     | 2      |            | 0.246     | 12  | 12    |           | 0.371     |
| 6     | 3      |            | 0.138     | 12  | 13    |           | 0.608     |
| 6     | 4      |            | 0.188     | 12  | 14    |           | 0.514     |
| 6     | 5      |            | 0.068     | 12  | 15    |           | 0.665     |
| 6     | 6      |            | 0.090     | 12  | 16    |           | 0.506     |
| 6     | 7      |            | 0.111     |     |       |           | 0.998     |
| 6     | 8      |            | 0.170     | 12  | 17    |           | 4.290     |
| 6     | 9      |            | 0.801     | 12  | 18    |           |           |
|       |        |            |           | 12  | 19    |           | 2.313     |
| 7     | 1      | 0.398      | 0.009     | 12  | 20    |           | 4.799     |
| 7     | 2      |            | 0.014     | 12  | 21    |           | 6.886     |
| 7     | 3      |            | 0.019     | 12  | 22    |           | 4.375     |
| 7     | 4      |            | 0.027     | 12  | 23    |           | 5.034     |
| 7     | 5      |            | 0.033     | 12  | 24    |           | 0.691     |
| 7     | 6      |            | 0.059     | 12  | 25    |           | 0.158     |
| 7     | 7      |            | 0.061     | 12  | 26    |           | 0.148     |
| 7     | 8      |            | 0.080     |     |       |           |           |
| 7     | 9      |            | 0.097     | 13  | 1     | 0.617     | 0.141     |
|       |        |            |           | 13  | 2     |           | 0.168     |
| 8     | 1      | 0.         | 0.        | 13  | 3     |           | 0.134     |
|       |        |            |           | 13  | 4     |           | 0.080     |
| 9     | 1      | 0.838      | 0.006     | 13  | 5     |           | 0.095     |
| 9     | 2      |            | 0.832     | 13  | 6     |           | 0.        |
|       |        |            |           | 13  | 7     |           | 0.        |
| 10    | 1      | 0.144      | 0.027     | 13  | 8     |           | 0.        |
| 10    | 2      |            | 0.033     | 13  | 9     |           | 0.        |
| 10    | 3      |            | 0.036     | 13  | 10    |           | 0.        |
| 10    | 4      |            | 0.048     | 13  | 11    |           | 0.        |
|       |        |            |           | 13  | 12    |           | 0.        |
| 11    | I      | 2.248      | 0.059     | 13  | 13    |           | 0.        |
| 11    | 2      |            | 0.093     |     |       |           |           |
| 11    | 3      |            | 0.185     | 14  | 1     | 0.386     | 0.032     |
| 11    | 4      |            | 0.110     | 14  | 2     |           | 0.084     |
| 11    | 5      |            | 0.070     | 14  | 3     |           | 0.270     |
|       |        |            |           |     |       |           |           |



Table I.48. Overall Cost-Responsibility for State Highway System (1985-86)

|       |       |           |           |       | C . L | 7 Pospor  | achiliry  |
|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh   | Sub-  | % Respon  | nsibility | Veh   | Sub-  | A Kespoi  | nsibility |
| Class | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
|       |       |           |           |       | ,     |           | 0.236     |
| 1     | 1     | 13.321    | 13.321    | 11    | 6     |           | 0.102     |
|       |       |           |           | 1 i   | 7     |           |           |
| 2     | 1     | 46.179    | 46.179    | 11    | 8     |           | 0.115     |
| -     | •     |           |           | 11    | 9     |           | 0.111     |
| 3     | 1     | 3.750     | 0.391     | 11    | 10    |           | 0.128     |
|       |       | 3.730     | 0.244     | 11    | 11    |           | 0.143     |
| 3     | 2     |           |           | 11    | 12    |           | 0.151     |
| 3     | 3     |           | 0.599     | 11    | 13    |           | 0.244     |
| 3     | 4     |           | 0.585     | 11    | 13    |           |           |
| 3     | 5     |           | 0.370     |       | ,     | 20 026    | 0.026     |
| 3     | 6     |           | 0.628     | 12    | 1     | 29.836    |           |
| 3     | 7     |           | 0.433     | 12    | 2     |           | 0.115     |
| 3     | 8     |           | 0.221     | 12    | 3     |           | 0.445     |
| 3     | 9     |           | 0.278     | 12    | 4     |           | 1.280     |
| 2     | 7     |           | 0.210     | 12    | 5     |           | 0.759     |
|       |       | 0 220     | 0.220     | 12    | 6     |           | 0.637     |
| 4     | 1     | 0.220     | 0.220     | 12    | 7     |           | 0.359     |
|       |       |           |           | 12    | 8     |           | 0.426     |
| 5     | 1     | 0.491     | 0.491     | _     | 9     |           | 0.571     |
|       |       |           |           | 12    |       |           | 0.590     |
| 6     | 1     | 1.001     | 0.204     | 12    | 10    |           |           |
| 6     | 2     |           | 0.127     | 12    | 11    |           | 0.425     |
| 6     | 3     |           | 0.106     | 12    | 12    |           | 0.469     |
| 6     | 4     |           | 0.116     | 12    | 13    |           | 0.550     |
|       |       |           | 0.045     | 12    | 14    |           | 0.658     |
| 6     | 5     |           |           | 12    | 15    |           | 0.694     |
| 6     | 6     |           | 0.047     | 12    | 16    |           | 1.057     |
| 6     | 7     |           | 0.056     |       | 17    |           | 1.127     |
| 6     | 8     |           | 0.069     | 12    |       |           | 2.206     |
| 6     | 9     |           | 0.230     | 12    | 18    |           | 1.643     |
|       |       |           |           | 12    | 19    |           |           |
| 7     | 1     | 0.876     | 0.042     | 12    | 20    |           | 2.746     |
| 7     | 2     |           | 0.039     | 12    | 21    |           | 4.597     |
| 7     | 3     |           | 0.052     | 12    | 22    |           | 4.118     |
| 7     | 4     |           | 0.071     | 12    | 23    |           | 3.119     |
|       |       |           | 0.076     | 12    | 24    |           | 0.863     |
| 7     | 5     |           | 0.115     | 12    | 25    |           | 0.134     |
| 7     | 6     |           |           | 12    | 26    |           | 0.223     |
| 7     | 7     |           | 0.148     | 14    | 40    |           |           |
| 7     | 8     |           | 0.157     |       | ,     | 0.744     | 0.100     |
| 7     | 9     |           | 0.175     | 13    | 1     | 0.744     | 0.116     |
|       |       |           |           | 13    | 2     |           | 0.095     |
| 8     | 1     | 0.141     | 0.141     | 13    | 3     |           |           |
|       |       |           |           | 13    | 4     |           | 0.072     |
| 9     | 1     | 0.787     | 0.027     | 13    | 5     |           | 0.055     |
|       |       | (/,/0/    | 0.760     | 13    | 6     |           | 0.026     |
| 9     | 2     |           | 0.700     | 13    | 7     |           | 0.044     |
|       |       |           | 0.000     | 13    | 8     |           | 0.020     |
| 10    | 1     | 0.114     | 0.023     |       |       |           | 0.022     |
| 10    | 2     |           | 0.026     | 13    | 9     |           | 0.038     |
| 10    | 3     |           | 0.031     | 13    | 10    |           |           |
| 10    | 4     |           | 0.034     | 13    | 11    |           | 0.024     |
|       |       |           |           | 13    | 12    |           | 0.060     |
| 1.1   | 1     | 1.840     | 0.056     | 13    | 13    |           | 0.073     |
| 11    |       | 1.040     | 0.093     | •     |       |           |           |
| 11    | 2     |           | 0.213     | 14    | 1     | 0.707     | 0.057     |
| 11    | 3     |           |           | 14    | 2     |           | 0.142     |
| 11    | 4     |           | 0.120     | 14    | 3     |           | 0.509     |
| 11    | 5     |           | 0.127     | [4    | ,     |           |           |



Table I.49. Overall Cost-Responsibility for County Road System (1985-86)

|       |       |           |           |       |       | # D       |           |
|-------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh   | Sub-  | % Respon  | nsibility | Veh   | Sub-  |           | sibility  |
| Class | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
|       |       |           |           |       |       |           | 0 (50     |
| 1     | 1     | 6.412     | 6.412     | 11    | 6     |           | 0.659     |
| -     | -     |           |           | 11    | 7     |           | 0.201     |
| 2     | 1     | 32.501    | 32.501    | 11    | 8     |           | 0.282     |
| 2     |       | 32.301    | 32        | 11    | 9     |           | 0.187     |
| 2     | 1     | 13.836    | 0.495     | 11    | 10    |           | 0.239     |
| 3     | 1     | 13.030    | 0.291     | 11    | 11    |           | 0.303     |
| 3     | 2     |           | 1.538     | 11    | 12    |           | 0.377     |
| 3     | 3     |           |           | 11    | 13    |           | 0.925     |
| 3     | 4     |           | 1.698     | * *   |       |           |           |
| 3     | 5     |           | 0.834     | 12    | 1     | 27.004    | 0.009     |
| 3     | 6     |           | 3.835     |       | 2     | 27.004    | 0.024     |
| 3     | 7     |           | 2.941     | 12    |       |           | 0.088     |
| 3     | 8     |           | 0.872     | 12    | 3     |           | 0.520     |
| 3     | 9     |           | 1.331     | 12    | 4     |           |           |
|       |       |           |           | 12    | 5     |           | 0.148     |
| 4     | 1     | 0.438     | 0.438     | 12    | 6     |           | 0.314     |
|       |       |           |           | 12    | 7     |           | 0.034     |
| 5     | 1     | 0.299     | 0.299     | 12    | 8     |           | 0.166     |
| ,     | •     | 0.277     |           | 12    | 9     |           | 0.435     |
| 6     | 1     | 6.211     | 0.717     | 12    | 10    |           | 0.489     |
|       |       | 0.211     | 0.580     | 12    | 11    |           | 0.145     |
| 6     | 2     |           |           | 12    | 12    |           | 0.267     |
| 6     | 3     |           | 0.368     | 12    | 13    |           | 0.438     |
| 6     | 4     |           | 0.513     |       |       |           | 0.399     |
| 6     | 5     |           | 0.213     | 12    | 14    |           | 0.473     |
| 6     | 6     |           | 0.281     | 12    | 15    |           |           |
| 6     | 7     |           | 0.352     | 12    | 16    |           | 0.373     |
| 6     | 8     |           | 0.570     | 12    | 17    |           | 0.762     |
| 6     | 9     |           | 2.617     | 12    | 18    |           | 3.264     |
| · ·   |       |           |           | 12    | 19    |           | 1.770     |
| 7     | 1     | 0.999     | 0.017     | 12    | 20    |           | 3.665     |
| 7     | 2     | 0.777     | 0.026     | 12    | 21    |           | 5.235     |
| 7     | 3     |           | 0.020     | 12    | 22    |           | 3.345     |
| /     | 4     |           | 0.064     | 12    | 23    |           | 3.859     |
| 7     |       |           | 0.070     | 12    | 24    |           | 0.526     |
| 7     | 5     |           | 0.149     | 12    | 25    |           | 0.120     |
| 7     | 6     |           |           | 12    | 26    |           | 0.136     |
| 7     | 7     |           | 0.154     | 12    | 20    |           |           |
| 7     | 8     |           | 0.213     | 13    | 1     | 3.224     | 0.673     |
| 7     | 9     |           | 0.265     |       | 2     | 3.224     | 0.852     |
|       |       |           |           | 13    | 3     |           | 0.712     |
| 8     | 1     | 0.        | 0.        | 13    |       |           | 0.442     |
|       |       |           |           | 13    | 4     |           |           |
| 9     | 1     | 2.543     | 0.011     | 13    | 5     |           | 0.544     |
| 9     | 2     |           | 2.531     | 13    | 6     |           | 0.        |
|       | _     |           |           | 13    | 7     |           | 0.        |
| 10    | 1     | 0.        | 0.        | 13    | 8     |           | 0.        |
|       | 2     | 0.        | 0.        | 13    | 9     |           | 0.        |
| 10    |       |           | 0.        | 13    | 10    |           | 0.        |
| 10    | 3     |           |           | 13    | 11    |           | 0.        |
| 10    | 4     |           | 0.        | 13    | 12    |           | 0.        |
|       |       |           | 0.073     |       | 13    |           | 0.        |
| 11    | 1     | 3.924     | 0.067     | 13    | 13    |           | •         |
| 11    | 2     |           | 0.145     |       | ,     | 2 610     | 0.234     |
| 11    | 3     |           | 0.275     | 14    | 1     | 2.610     | 0.234     |
| 11    | 4     |           | 0.162     | 14    | 2     |           |           |
| 11    | 5     |           | 0.105     | 14    | 3     |           | 1.804     |
|       |       |           |           |       |       |           |           |



Table I.50. Overall Cost-Responsibility for City Street System (1985-86)

|          |       |           |           |       | 6.1   | 9 Bacano  | neibility |
|----------|-------|-----------|-----------|-------|-------|-----------|-----------|
| Veh      | Sub-  | % Respon  | rsibility | Veh   | Sub-  |           |           |
| Class    | Group | Veh Class | Sub-Group | Class | Group | Veh Class | Sub-Group |
|          |       |           |           |       | ,     |           | 0.385     |
| 1        | 1     | 10.327    | 10.327    | 11    | 6     |           | 0.116     |
|          |       |           |           | 11    | 7     |           |           |
| 2        | 1     | 41.349    | 41.349    | 11    | 8     |           | 0.158     |
| -        | •     |           |           | 11    | 9     |           | 0.103     |
| 2        | ,     | 3.440     | 0.340     | 11    | 10    |           | 0.130     |
| 3        | 1     | 3.440     |           | 11    | 11    |           | 0.163     |
| 3        | 2     |           | 0.142     | 11    | 12    |           | 0.202     |
| 3        | 3     |           | 0.540     |       | 13    |           | 0.492     |
| 3        | 4     |           | 0.456     | 11    | 13    |           | 0.472     |
| 3        | 5     |           | 0.190     |       |       | 0.6 0.50  | 0.019     |
| 3        | 6     |           | 0.789     | 12    | 1     | 36.958    |           |
| 3        | 7     |           | 0.567     | 12    | 2     |           | 0.045     |
| 3        | 8     |           | 0.167     | 12    | 3     |           | 0.156     |
| 3        | 9     |           | 0.249     | 12    | 4     |           | 0.877     |
| 3        | 7     |           | 0 4 2 7 7 | 12    | 5     |           | 0.236     |
|          |       | 0.760     | 0.769     | 12    | 6     |           | 0.490     |
| 4        | 1     | 0.769     | 0.709     | 12    | 7     |           | 0.052     |
| •        |       |           |           | 12    | 8     |           | 0.247     |
| 5        | 1     | 0.279     | 0.279     |       | 9     |           | 0.641     |
|          |       |           |           | 12    |       |           | 0.706     |
| 6        | 1     | 2.060     | 0.307     | 12    | 10    |           |           |
| 6        | 2     |           | 0.241     | 12    | 11    |           | 0.206     |
| 6        | 3     |           | 0.134     | 12    | 12    |           | 0.377     |
| 6        | 4     |           | 0.175     | 12    | 13    |           | 0.613     |
|          | 5     |           | 0.068     | 12    | 14    |           | 0.554     |
| 6        |       |           | 0.087     | 12    | 15    |           | 0.652     |
| 6        | 6     |           |           | 12    | 16    |           | 0.510     |
| 6        | 7     |           | 0.108     |       | 17    |           | 1.040     |
| 6        | 8     |           | 0.167     | 12    |       |           | 4.431     |
| 6        | 9     |           | 0.772     | 12    | 18    |           | 2.393     |
|          |       |           |           | 12    | 19    |           |           |
| 7        | 1     | 0.420     | 0.010     | 12    | 20    |           | 4.939     |
| 7        | 2     | 00.00     | 0.014     | 12    | 21    |           | 7.042     |
| 7        | 3     |           | 0.020     | 12    | 22    |           | 4.488     |
| <u>'</u> |       |           | 0.029     | 12    | 23    |           | 5.192     |
| 7        | 4     |           |           | 12    | 24    |           | 0.706     |
| 7        | 5     |           | 0.030     | 12    | 25    |           | 0.162     |
| 7        | 6     |           | 0.061     | _     | 26    |           | 0.183     |
| 7        | 7     |           | 0.063     | 12    | 20    |           | 0.103     |
| 7        | 8     |           | 0.086     |       |       |           | 0.125     |
| 7        | 9     |           | 0.106     | 13    | 1     | 0.621     | 0.135     |
|          |       |           |           | 13    | 2     |           | 0.166     |
| 8        | 1     | 0.        | 0.        | 13    | 3     |           | 0.136     |
| 0        | •     | •         | • • •     | 13    | 4     |           | 0.083     |
|          |       | 0.960     | 0.005     | 13    | 5     |           | 0.101     |
| 9        | 1     | 0.960     |           | 13    | 6     |           | 0.        |
| 9        | 2     |           | 0.956     | 13    | 7     |           | 0.        |
|          |       |           | 0.036     | 13    | 8     |           | 0.        |
| 10       | I     | 0.152     | 0.026     |       | 9     |           | 0.        |
| 10       | 2     |           | 0.033     | 13    |       |           | 0.        |
| 10       | 3     |           | 0.039     | 13    | 10    |           | 0.        |
| 10       | 4     |           | 0.054     | 13    | 11    |           |           |
|          |       |           |           | 13    | 12    |           | 0.        |
| 11       | 1     | 2.267     | 0.063     | 13    | 13    |           | 0.        |
| 11       | 2     | _+201     | 0.103     |       |       |           |           |
|          | 3     |           | 0.183     | 14    | 1     | 0.411     | 0.034     |
| 11       |       |           | 0.105     | 14    | 2     |           | 0.083     |
| 11       | 4     |           |           | 14    | 3     |           | 0.295     |
| 11       | 5     |           | 0.065     | 14    | ,     |           |           |



#### APPENDIX J

# PROBLEMS OF USING CENTS PER VEHICLE-MILES OF TRAVEL AS AN INDEX FOR EXPRESSING COST-ALLOCATION RESULTS

The index cents/VMT was used in a number of cost-allocation studies to asses whether individual vehicle types were paying their fair share of cost responsibilities. This index is not adopted in this study to compare cost-responsibilities of vehicle classes and their revenue contribution because of a number of problems involved in its use.

Firstly, it is recognized that the index cents/VMT does not have a sound meaning in cost-allocation analysis. This is because not all expenditure items are functions of vehicle-miles of travel. For instance, a large portion of bridge related costs cannot be meaningfully related to vehicle-miles of travel. Consider two vehicle classes with identical percentage cost-responsibility of bridge construction cost based on individual vehicular loading consideration. When expressed in terms of cents/VMT, the vehicle class with a higher VMT would have a lower cents/VMT value. This appears to suggest that one vehicle class has a lower 'unit cost' than the other, which is actually not true. This clearly indicates that cents/VMT is a poor unit cost-responsibility measure in cost-allocation study where many expenditure items could not be allocated in direct proportion to vehicle class VMT. One must therefore be refrained from making comparison on the relative cost-responsibility of vehicle classes based on their cents/VMT values.

Secondly, since all user revenues can not be related to vehicle-miles of travel, the use of cents/VMT to measure vehicle class revenue contribution is a misrepresentation.



Lastly, the term cents/VMT, as it is being used in cost-allocation, is not uniquely defined. There are a few possible ways of computing cents/VMT cost-responsibility for vehicle classes in cost-allocation study, and each produces a different set of cents/VMT values. A simple hypothetical example is presented below to illustrate this point.

Consider a cost-allocation problem involving two highway classes and two vehicle classes. The total expenditures on highway classes 1 and 2 are \$90,000 and \$ 10,000 respectively, and the results of cost-allocation analysis are summarized in Table J.1.

The results in Table J.1 indicate that vehicle class A underpays by \$8,000 or 13.33%, and vehicle class B overpays by \$8,000 or 20.00%. A fair revenue collection scheme would require vehicle class A to increase its contribution by 13.33%, and vehicle class B to decrease by 20.00%.

Table J.2 shows four differents ways by which the same cost-allocation results may be expressed in terms of cents/VMT. Method (a) produces the same conclusion as that in Table J.1 regarding cost-responsibility. However, the resultant cents/VMT values are illogical and misleading in the sense that vehicle class A is lower in cents/VMT value than vehicle class B for both highway classes 1 and 2, yet the computed resultant cents/VMT values indicate the opposite.

Methods (b), (c) and (d) compute weighted average values of cents/VMT using different parameters as weighting factors. Method (b) concludes that both vehicle classes A and B are overpaying, whereas method (c) indicates that both are underpaying. The last method, method (d), leads to yet another conclusion: vehicle class A overpays and vehicle class B underpays.



# Table J.1 Cost-Allocation analysis of Example Problem

### (a) Problem data

Highway Class 1 - Total Expenditure \$90,000 Total Mileage 10,000 miles Total VMT  $10 \times 10^6$ 

Vehicle Class A VMT 8 x  $10^6$ Vehicle Class B VMT 2 x  $10^6$ 

Highway Class 2 - Total Expenditure \$10,000

Total Mileage 20,000
Total VMT 10 x 10<sup>6</sup>

Vehicle Class A VMT  $5 \times 10^6$ Vehicle Class B VMT  $5 \times 10^6$ 

Revenue Contribution - Vehicle Class A \$60,000

Vehicle Class B \$40,000

\$40,000

\$32,000

## (b) Cost-Allocation Results

\$26,000

Vehicle Class B

|                 | Highway Class 1     | Highway Class 2     | Total Cost-    | Total Revenue |
|-----------------|---------------------|---------------------|----------------|---------------|
|                 | Cost-Responsibility | Cost-Responsibility | Responsibility | Contribution  |
| Vehicle Class A | \$64,000            | \$4,000             | \$68,000       | \$60,000      |

\$6,000



The example above shows that, depending on the computational procedure adopted, the final cost-responsibility values expressed in cents/VMT can vary over a relatively wide range. Conclusions drawn from different versions of cents/VMT values also can be very different. The problem of these conflicting results is further complicated by the fact that none of the four procedures presented in Table J.2 can be claimed to be perfect, and none can be said to be completely wrong.

Based on the discussion above, it is clear that a fair and sound comparison between vehicle classes' cost-responsibilities and their revenue contribution cannot be made by expressing cost-responsibilities or revenue contribution or both in cents/VMT. It was therefore decided that the results of the present study would not be expressed in terms of cents/VMT.



Tible J.2 Cost Allocation of Fxamule Problem Expressed in Cents/VMT

| Revenue in<br>cents/WHT                    | 0.46  |  | :                  | -               |                   |                |  |
|--|---|--|--------------------|-----------------|-------------------|----------------|--|
| Overall<br>Cost in<br>ty Cents/V:IT        | 0.52  | Revenue in cents/viiT 0.46 0.57 0.57 0.46 0.57 0.46 0.46   | Research In        | CONC. VAIL      | 00                |                |  |
| Ove<br>Cost-<br>Responsibility             | \$68,000  | Overall 0.32 0.51 0.51 0.73 1.18   |                    | 0001311         | 0.44              | 0.71           |  |
| VHT  | 13 × 10 <sup>6</sup> 7 × 10 <sup>6</sup>  | 0  | <u>.</u>           |                 |                   |                |  |
| Cost in<br>Cents/WIT                       | 0.08 1  | Costs in cents/VMT Highway Class 2 0.08 0.12 . 0.6667 . 0.6667 Costs in cents/VMT Highway Class 2 0.08 0.12 0.10   | Costs in cents/Wif | Highway Class 2 | 0.08              | 0.12           | 0.50   |
| Highway Class 2<br>Cost-<br>Responsibility | \$4,000   | č  | ้อ                 | 4411 1          |                   |                |  |
| Try  | 5 × 10 <sup>6</sup> 5 × 10 <sup>6</sup>   | Highway Class 1<br>0.60<br>1.30<br>0.3333<br>Highway Class 1<br>0.80<br>1.30<br>0.90   |                    | Highway Clann 1 | 0.50              | 1.30           | 0.50   |
| Cost in<br>Cents/VMT                       | 0.80  | Class Mile:  |                    |                 |                   |                |  |
| Highway Class 1<br>Cost-<br>Responsibility | \$64,000  | d based on Expend  |                    |                 |                   |                |  |
| () Total Sum Method                        | Vehicle Class A 8 $\times$ 10 <sup>6</sup> Vehicle Class B 2 $\times$ 10 <sup>6</sup> | (b) Weighted Average Method based on Highway Class Mileages Vehicle Class B Weighting Factor (c) Weighted Average Method based on Expenditures (d) Weighted Average Method based on Highway Class B Weighted Class B Weighted Class B Weighted Average Method based on Highway Class WHT |                    |                 | V late a Tlassa A | Wester Class B | The first of the state of the s |



## REFERENCES

- American Association of State Highway and Transportation Officials, A Policy on Geometric Design of Highway and Streets, 1984.
- American Association of State Highway and Transportation Officials, AASHTO Interim Guide for Design of Pavement Structures, 1981.
- American Association of State Highway and Transportation Officials, Standard Specifications for Highway Bridges, 12th edition, 1977.
- 4. Black, J. E. and J. G. Pigman, "Allocation of Transportation Costs to Users," Kentucky Transportation Research Program, University of Kentucky, May, 1982.
- Census of Transportation U.S., "Summary: Truck Inventory and Use Survey", 1977.
- Colucci-Rios B., and E. J. Yoder, "Effects of Raising Load Limits on Pavements and Bridges in Indiana," JHRP-79-23, Purdue University, 1979.
- 7. Congressional Budget Office, "Guidelines for a Study of Highway Cost Allocation," U.S. Congress, February, 1979.
- 8. Connecticut Department of Transportation, "Highway User Costs in Connecticut," Office of Research, Report No. 85051-F-82-1, February, 1982.
- 9. Federal Highway Administration, "Final Report on the Federal Highway Cost Allocation Study," May, 1982.
- 10. Federal Highway Administration, <u>Incremental Analysis of Structural Construction Costs</u>, Report FHWA/p1/81/008, April, 1981.
- 11. Florida Department of Transportation, "Florida Highway cost Allocation Study," December, 1979.
- 12. Fwa, T. F. and K. C. Sinha, "Thickness Incremental Method for Allocating Pavement Construction Costs in Highway Cost-Allocation Study," to be presented at the 1985 Annual Meeting of Transportation Research Board, Washington, D.C.
- 13. Fwa, T.F. and K.C. Sinha, "A Performance-Based Approach for Determining Cost-Responsibilities of Load-Related and Non-Load-Related Factors in Highway Pavement Rehabilitation and Maintenance Cost Allocation," to be presented at the 1985 Annual Meeting of Transportation Research Board, Washington, D.C.
- 14. Georgia Department of Transportation, "Georgia Highway Cost Allocation Study," March, 1979.
- 15. Highway Research Board Special Report 61E, "The AASHTO Road Test, Report 5, Pavement Research," 1962.



- 16. Highway Research Board Special Report 87, Highway Capacity Manual, 1965.
- Huff, T.S. and F.H. Scrivner, "Simplified Climbing-Lane Design Theory and Road Test Results," <u>Highway Research Board Bulletin</u> 104, 1955.
- Indiana Department of Highways, Contract Proposals Section, Catolog of U.P.A. Prices for Roads, Bridges and Traffic Items, 1983.
- 19. Indiana Department of Highways, Division of Maintenance, Field Operations Handbook for Foremen 1982 1983.
- 20. Indiana Transportation Coodinating Board, <u>Indiana Transportation Fact</u> Book, June 1982.
- 21. Iowa Department of Transportation, "Final Report of the Iowa Highway Cost Allocation Study," 1982.
- 22. Joint Legislative Audit and Review Commission, State of Virginia, "Vehicle Cost Responsibility in Virginia," January, 1982.
- 23. Kent, P. M. and M. T. Robey, 1975-1979 National Truck Characteristic Report, U.S. Department of Transportation, FHWA, June 1981.
- 24. Kiley, E.V., "Concept of Cost Functions and Incremental Solutions of Vehicle-Tax Allocation Problem," <u>HRB Bulletin 121</u>, Highway Research Board, 1956.
- 25. Lewis, D. and R. A. Barnhart, Road <u>User and Property Taxes</u>, <u>On Selected Motor Vehicles</u>, U. S. Department of Transportation, FHWA, 1982.
- 26. MacTavish, Douglas and Neumann, Donald L., <u>Vehicle Classification Case</u>
  Study for the <u>Highway Performance Monitoring System</u>, Federal Highway
  Administration, August, 1982.
- 27. Maine Department of Transportation, "Final Report of the Maine Highway Cost Allocation Study," December, 1982.
- 28. Maine Department of Transportation, "Main Highway Cost Allocation," Working Paper No. 3, 1982.
- 29. Mannering, Fred L. and K. C. Sinha, "Methodology for Evaluating Impacts of Energy, National Economy, and Public Policies on Highway Financing and Performance," Transportation Research Record 742, Transportation Research Board, 1980, pp. 20-27.
- 30. Metwali, S., "Framework for a Pavement Evaluation System," JHRP-81-7, Purdue University, 1981.
- 31. Mohan, S., "Development of a System for the Evaluation of Pavements in Indiana," Interim Report, JHRP-78-21, Purdue University, 1978.
- 32. North Carolina Department of Transportation, "North Carolina Highway Cost Allocation Study," Final Report, March, 1983.



- 33. Oregon Department of Transportation, "1980 Motor Vehicle Cost Responsibility Study," March, 1981.
- 34. Rauhut, J. B., R. L. Lytton and M. I. Darter "Pavement Damage Functions for Cost Allocation: Vol. I. Damage Functions and Load Equipment Factors," FHWA, DOT FH61-80-c-00175, Draft Final Report, July, 1982.
- 35. Reno, Arlee, T., B. J. Ritchey, and J. R. Morris, <u>Transportation System Descriptors Used in Forecasting Federal Highway Revenues</u>, U.S. Department of Transportation, FHWA, June 1981.
- 36. Sharaf, Essam A., K. C. Sinha and E. J. Yoder, "Energy Conservation and Cost Saving Related to Highway routine Maintenance: Data Collection and analysis of Fuel Consumption," JHRP-82-83, Interim Report, Joint Highway Research Project, School of Civil Engineering, Purdue University, December, 1982.
- 37. Sharaf, E. A. and K. C. Sinha, "Estimation of Pavement Routine Maintenance Costs," Joint Highway Research Project, School of Civil Engineering, Purdue University, October, 1983.
- 38. Sinha, K.C. et al., "Indiana State Highway Reciprocity Study: Final Report", JHRP-83-15, Joint Highway Research Project, School of Civil Engineering, Purdue University, October, 1983.
- 39. Sinha, K.C. et al., "Indiana Highway Cost-Allocation Study: A Report on Methodology", FHWA/IN/JHRP 84/4, Joint Highway Research Project, March, 1984.
- 40. Taragin, A., "Effect of Length of Grade on Speed of Motor Vehicles," Highway Research Proceedings, 1945.
- 41. Transportation Development Associates, Inc., "Washington State Highway Cost Allocation Study," January, 1977.
- 42. University of Maryland, "Maryland Cost Allocation Study," February, 1983.
- 43. U.S. Department of Transportation, FHWA, Highway Statistics, 1979, 1980, 1981, 1982.
- 44. U.S. Department of Transportation, FHWA, <u>Highway Taxes and Fees</u>, <u>How They</u> are <u>Collected and Distributed</u>, 1982.
- 45. Wilbur Smith and Associates, "Highway User Fee Study," prepared for the Joint Transportation and Highways Interim Committee, Wyoming State Legislature, February, 1981.
- 46. Willey, W.E., "Uphill Speeds of Trucks on Maintenance Grades," <u>Highway</u> Research Board Proceedings, 1949.
- 47. Winfrey, R., Economic Analysis for Highways, International Textbook Company, 1968.



- 48. Wisconsin Department of Transportation, "Highway Cost Allocation Study," Final Report, December, 1982.
- 49. Yoder, E.J. and M.W. Witczak, <u>Principles of Pavement Design</u>, 2nd Edition, John Wiley & Sons, 1975.
- 50. Yoder, S. R., Chief, Division of Design, "Indiana Pavement Design Procedure," Memo dated October 3, 1978, Revised November 3, 1983, Indiana Department of Highways.

The later of the control of the cont



